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Course Description

Part 3: Special Welding Applications and Field Fixes

July 13, 2017

This session covers atypical welding applications for buildings. The session presents practical, straightforward solutions to challenging situations including: extending anchor bolts, welding on coated steels, welding AESS, welding on existing structures, welding heavy sections, welding under high restraint, field welding and heat shrinking.



Learning Objectives

- Name four weldability concerns with extending anchor rods.
- Describe tolerance issues that may affect welded connections in AESS structures.
- Identify welded HSS connections where member configurations could prevent proper welding, inspection or assembly.
- Identify situations where rolled heavy shapes in welded connections may perform poorly.



There's always a solution in steel.

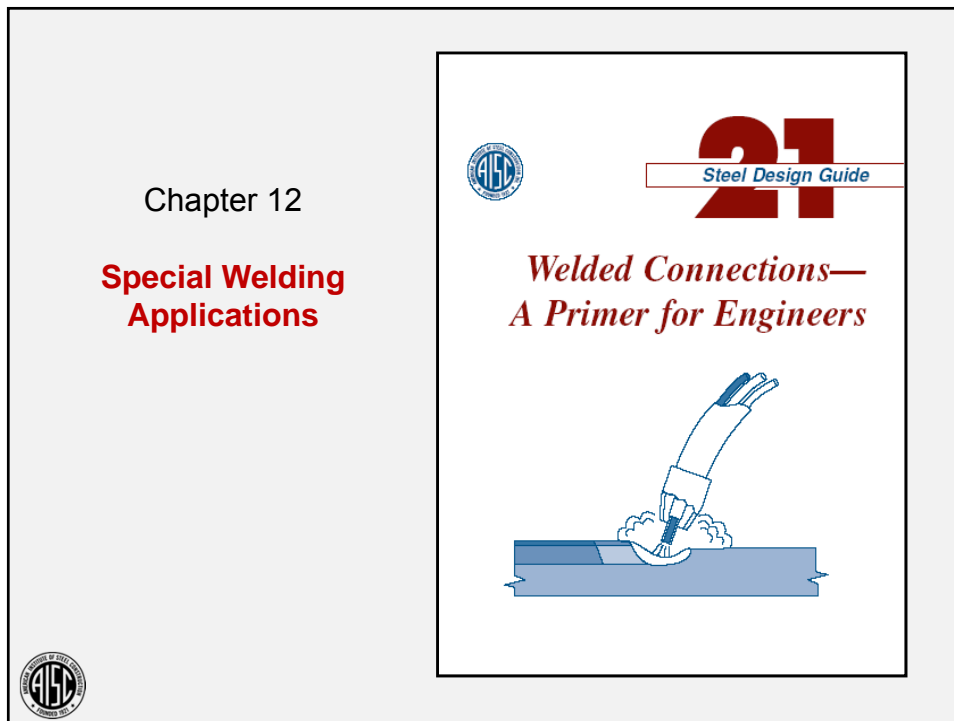
Welded Connections

Part 3: Special Welding Applications and Field Fixes
July 13, 2017



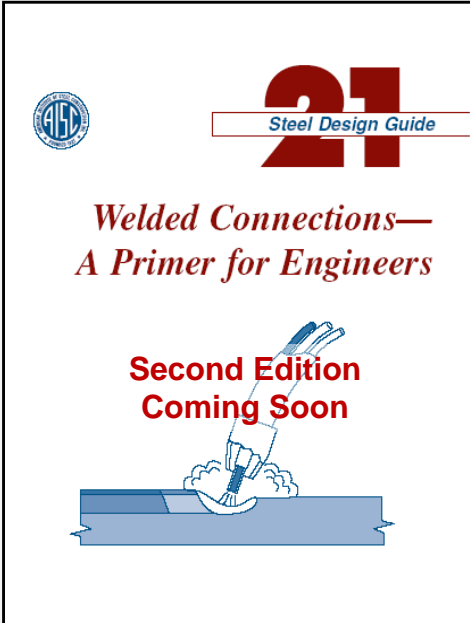
Presented by
Duane Miller, Sc.D., P.E.
Manager of Engineering Services and Welding
Design Consultant at The Lincoln Electric Company
Cleveland, OH





Chapter 14
Special Welding Applications


Chapter 15
Problems and Fixes




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Steel Design Guide

*Welded Connections—
A Primer for Engineers*

**Second Edition
Coming Soon**



14. SPECIAL WELDING APPLICATIONS

- 14.1 Welding of Steel Headed Stud Anchors
 - 14.2 Welding on Galvanized Steels
 - 14.3 Welding on Primed And Painted Steel
 - 14.4 Welding on Heavy Sections
 - 14.5 Welding on Highly Restrained Members
 - 14.6 Welding HSS
 - 14.7 Welding AESS
 - 14.8 Shop vs. Field Welding
 - 14.9 Welding on Existing Structures
 - 14.10 Welds and Mechanical Fasteners
 - 14.11 Welding on Members to be Hot-dip Galvanized
 - 14.12 Cold Temperature Applications
 - 14.13 Deck Welding
 - 14.14 Welding on In-place Embed Plates
 - 14.15 Heat Shrinking
 - 14.16 Buttering
- 




15 PROBLEMS AND FIXES

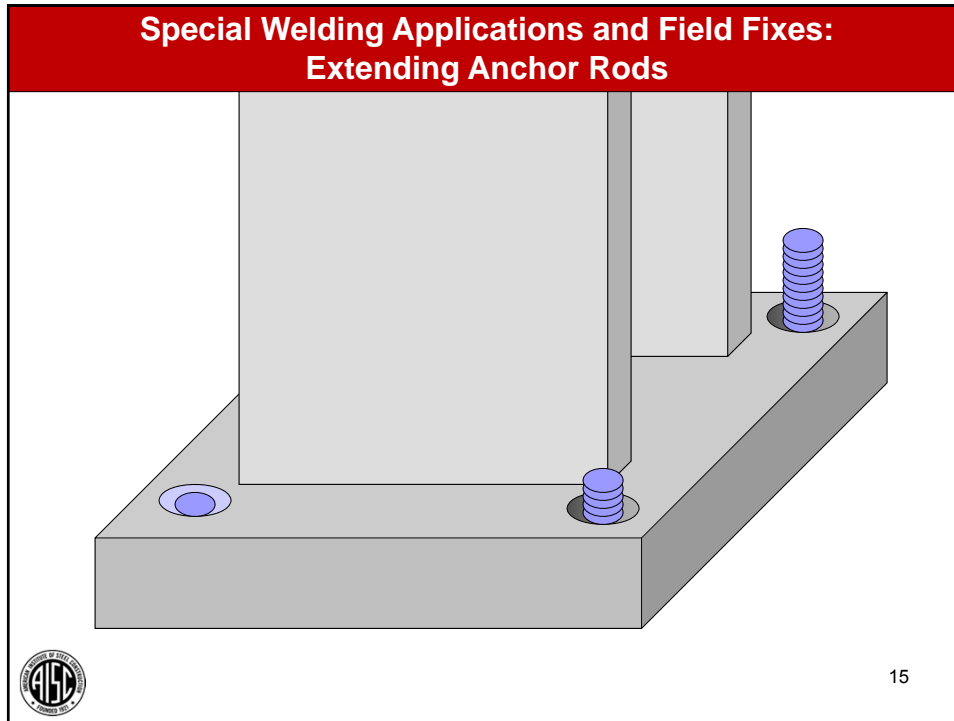
- 15.1 Repairs to Base Metal
- 15.2 Repairs to Cut Edges
- 15.3 Butt Joint Alignment
- 15.4 Out-of-tolerance Weld Joints
- 15.5 Fixing Members That Are Cut Short
- 15.6 Repair of Mislocated Holes
- 15.7 Use of Plug Welds In Lieu Of Bolts
- 15.8 Repairs to Welds
- 15.9 Heat Shrinking of Q&T Steel
- 15.10 Unspecified Welds
- 15.11 Welds Made Without Inspection
- 15.12 Welding on Anchor Rods
- 15.13 Welding Anchor Rod to Base Plates
- 15.14 Removing and Reinstalling Column Base Plates
- 15.15 Repairing Lamellar Tears



Special Welding Applications and Field Fixes

-  • Welding on Anchor Rods
- Welding on Heavy Sections (“Jumbo Shapes”)
- Welding HSS
- Welding AECS
- Field Welding
- Welding on Existing Structures
- Combining Welds and Bolts





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Design Guide 21: Welded Connections

12. Special Welding Applications

12.1 WELDING ON ANCHOR RODS

12.1.1 General

Before any welding on anchor rods is considered, the rod's composition must be considered, as addressed in detail in Section 4.3.4 of this Guide. This point cannot be overstated; material with unknown or poor weldability simply should not be welded upon until appropriate testing and analysis has been performed.

12.1.2 Extending Anchor Rods

When an anchor rod is set too deep, there may be an inadequate length of thread available for proper engagement of the nut. In extreme conditions, the end of the anchor rod may be below the top surface of the base plate. Possible solutions that involve welding are often offered, but such approaches must be carefully evaluated.

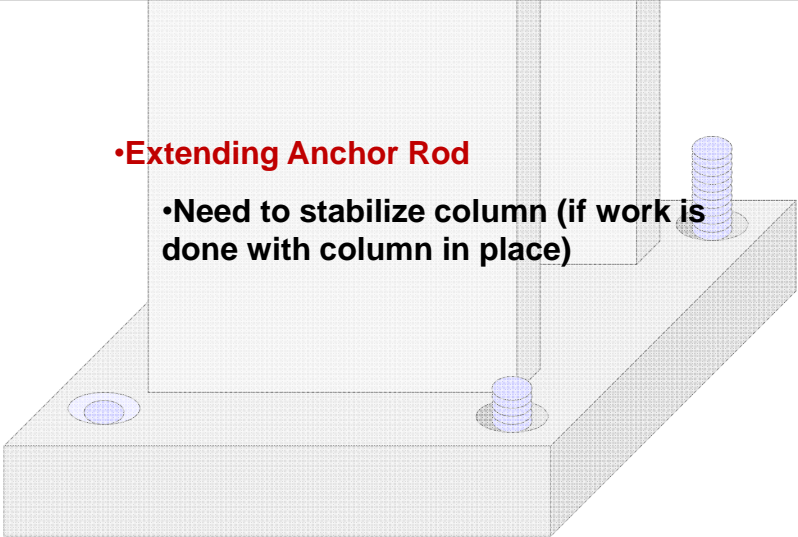
Even when a weldable anchor rod is involved, several commonly proposed corrective concepts are problematic. For example, if the rod is very short, some may be tempted to use a plug weld in the base plate to weld on to the end of the

A connection detail has been developed to address some of the problematic aspects associated with anchor rod extension (Fisher and Kloiber, 2006). The weld joint involved is a double-sided horizontal bevel groove weld. The extension rod is prepared by applying two bevels that form a chisel-like configuration (not a pencil point) as shown in Figure 12-1. A ring or washer is made from steel with a known weldability, and of a thickness great enough that welds will not melt through it. The top surface of the ring is positioned so that it is flush with the too-short rod. The ring acts as a weld tab, allowing the arc starts and stops to be placed outside of the width of the anchor rod. As with prequalified double-sided welds, the root region of the first weld pass should be back-gouged before the second side is welded. When the welding is complete, the ring can be removed by grinding or other methods and finally, the weld can be ground flush around the perimeter.


Welding is typically performed with SMAW using electrodes with low-hydrogen coatings. The strength of the electrode must be selected to match the strength of the anchor rod used. Depending on the rod composition, preheat may



**Special Welding Applications and Field Fixes:
Extending Anchor Rods**

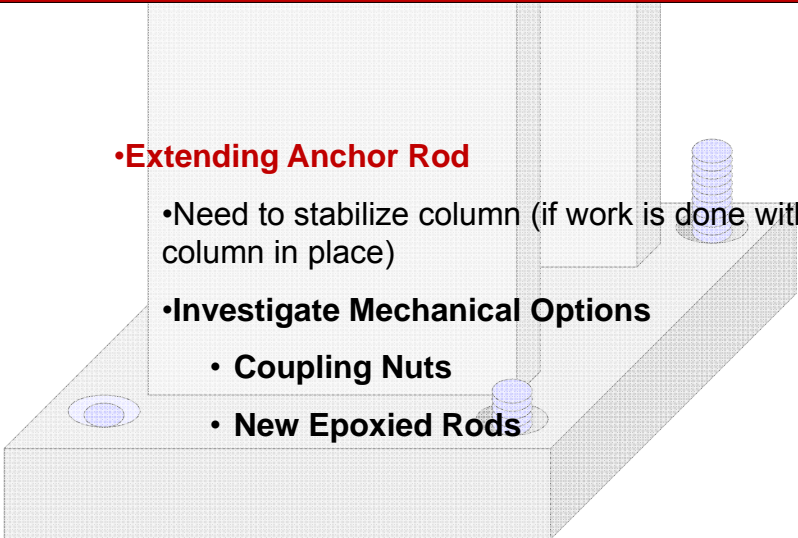


- **Extending Anchor Rod**
- **Need to stabilize column (if work is done with column in place)**




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**Special Welding Applications and Field Fixes:
Extending Anchor Rods**

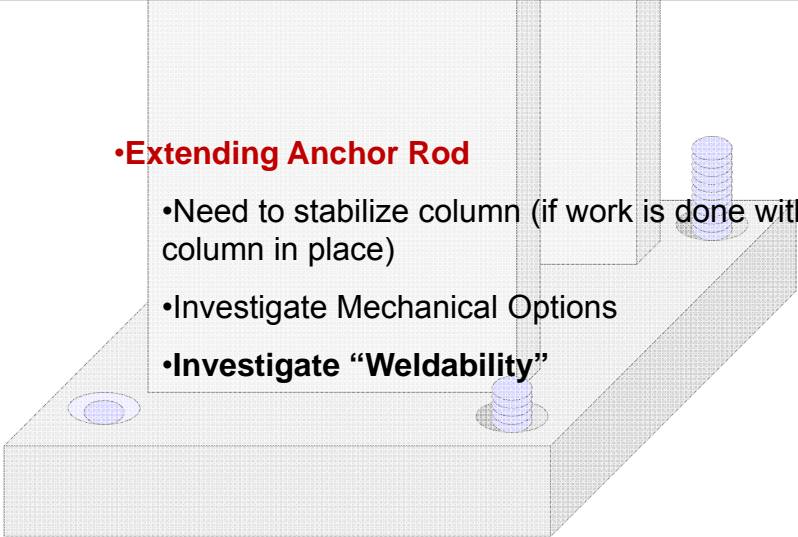


- **Extending Anchor Rod**
- **Need to stabilize column (if work is done with column in place)**
- **Investigate Mechanical Options**
 - **Coupling Nuts**
 - **New Epoxied Rods**




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Special Welding Applications and Field Fixes: Extending Anchor Rods



- **Extending Anchor Rod**
 - Need to stabilize column (if work is done with column in place)
 - Investigate Mechanical Options
 - Investigate **“Weldability”**




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Weldability

- Based on composition
- Driven by carbon content
- Compounded by alloy content
- Related to “hardenability”
- “Hot cracking” concerns as well (S, P, others)

Weldability: How easily can the material be welded

NOT can the material be welded




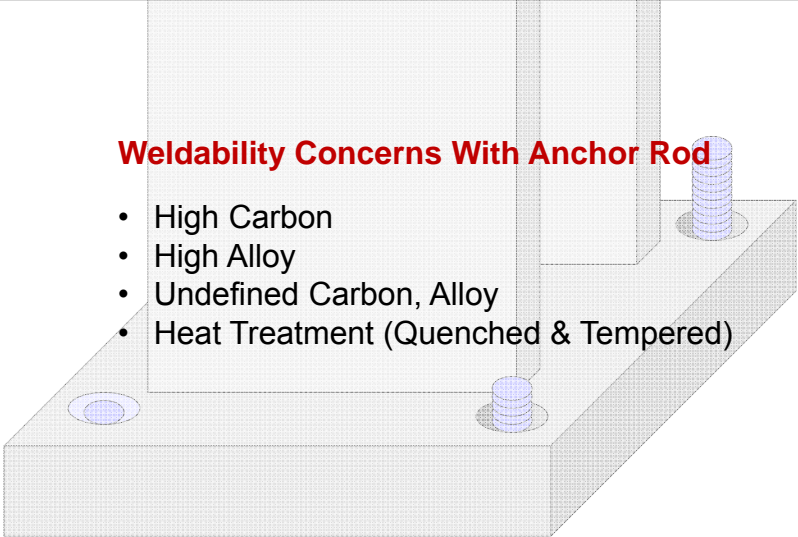
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**Special Welding Applications and Field Fixes:
Extending Anchor Rods**

Weldability Concerns With Anchor Rod

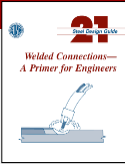
- High Carbon
- High Alloy
- Undefined Carbon, Alloy
- Heat Treatment (Quenched & Tempered)



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Design Guide 21: Welded Connections


Metallurgical Issues



4.5 Welding Nonstructural Steels

4.5.1 Anchor Rods

- ASTM A307
- ASTM A325
- ASTM A354
- ASTM A449
- ASTM A675
- ➔ ASTM F1554




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ASTM A1554-07a

Standard Specification for
Anchor Bolts, Steel, 36,
55, and 105-ksi Yield
Strength



Designation: F 1554 – 07a

**Standard Specification for
Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength¹**

This standard is issued under the fixed designation F 1554; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last approval. A superscript letter (X) indicates an editorial change since the last revision or approval.

1. Scope²

1.1 This specification covers straight and bent, headed and headless, carbon, carbon-manganese, alloy, or high-strength low-alloy steel anchor bolts (also known as anchor rods). The anchor bolts are furnished in three strength grades, two thread classes, and in the sizes specified in Section 4.

1.2 The anchor bolts are intended for anchoring structural supports to concrete foundations. Such structural supports include building columns, column supports for highway signs, street lighting and traffic signals, steel bearing plates, and similar applications.

1.3 Supplementary requirements are included to provide for Grade 55 weldable steel, permanent manufacturer and grade identification, and impact properties for Grades 55 and 105.

1.4 Zinc coating requirements are included in Section 7 for applications requiring corrosion protection.

1.5 The recommended grade and style of nut and washer are included in 6.6 and 6.7 for each grade.

1.6 This specification does not cover the requirements for mechanical expansion anchors, powder-actuated nails, or studs, or anchor bolts (extracted from deformed bar).

1.7 The values stated in inch-pound units are to be regarded as the standard. The values given in parentheses are for information only.

2. Referenced Documents

2.1 *ASTM Standards:*³

A 1063/A 1063M Specification for Carbon and Alloy Steel Nuts for Bolts for High Pressure or High Temperature Service, or Both

A 130 Test Methods and Definitions for Mechanical Testing of Steel Products

A 363 Specification for Carbon and Alloy Steel Nuts

A 673/A 673M Specification for Sampling Procedure for Impact Testing of Structural Steel

3. Terminology

3.1 *Definitions of Terms Specific to This Standard:*

3.1.1 *anchor bolt*—steel rod or bar, one end of which is intended to be cast in concrete, while the opposite end is threaded and projects from the concrete, for anchoring other material to the concrete. The end cast in concrete may be either straight or provided with an anchor nut as a forged head, forged head, or a laprod or welded attachment to resist forces imposed on the anchor bolt, as required.

3.1.2 *manufacturer*—manufacturer of the anchor bolt; the party that performs the cutting, bending, and threading operations.


3.1.3 *producer*—manufacturer of the steel rods or bars.

3.1.4 *purchaser*—purchaser of the finished anchor bolt, or his designated agent.

¹Available from Research Council on Structural Connections, c/o Industrial Engineering Institute, 1175 Lee Street, Cleveland, OH 44116.
²Available from American Society of Mechanical Engineers (ASME), ASME International Headquarters, Three Park Ave., New York, NY 10016-5900, http://www.asme.org.
³A Summary of Changes section appears at the end of this standard.
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ASTM A1554-07a

Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength



Three Grades

4. Classification

4.1 The anchor bolts are furnished in three grades denoting minimum yield strength and two classes denoting thread class as follows:


Grade	Tensile Strength, ksi (MPa)	Description Yield Strength, min, ksi (MPa)	Size Range, in. (mm)
36 ^A	58–80 (400–558)	36 (248)	1/4–4 (6.4–102)
55	75–95 (517–655)	55 (380)	1/4–4 (6.4–102)
105	125–150 (862–1034)	105 (724)	1/4–3 (6.4–76)

Class

1A anchor bolts with Class 1A threads

2A anchor bolts with Class 2A threads

^A When Grade 36 is specified, a weldable Grade 55 may be furnished at the supplier's option.



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ASTM A1554-07a
Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

4.2 Weldable steel for Grade 55 is provided for in Supplementary Requirement SI.

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Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

Substitution option: weldable Grade 55 for Grade 36

4. Classification

4.1 The anchor bolts are furnished in three grades denoting minimum yield strength and two classes denoting thread class as follows:

Grade	Tensile Strength, ksi (MPa)	Description Yield Strength, min, ksi (MPa)	Size Range, in. (mm)
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55	75–95 (517–655)	55 (380)	¼ –4 (6.4–102)
105	125–150 (862–1034)	105 (724)	¼ –3 (6.4–76)

Class

1A anchor bolts with Class 1A threads

2A anchor bolts with Class 2A threads


^A When Grade 36 is specified, a weldable Grade 55 may be furnished at the supplier's option.

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ASTM A1554-07a
Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

Permitted Options	
Ordered	Delivered
Grade 36	Grade 36
	Grade 55 S1
Grade 55	Grade 55
	Grade 55 S1
Grade 55 S1	Grade 55 S1
Grade 105	Grade 105




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ASTM A1554-07a
Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

Permitted Options	
Ordered	Delivered
Grade 36	Grade 36
	Grade 55 S1
Grade 55	Grade 55
	Grade 55 S1
Grade 55 S1	Grade 55 S1
Grade 105	Grade 105

Four Types to be Considered



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ASTM A1554-07a
Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

TABLE 1 Chemical Requirements for Grade 36

Element	Diameter, in. (mm)		
	To ¾ (20), incl	Over ¾ to 1½ (20 to 40), incl	Over 1½ to 4 (40 to 100), incl
Carbon, max, %			
Heat	0.26	0.27	0.28
Product	0.29	0.30	0.31
Manganese, %			
Heat	^A	0.60–0.90	0.60–0.90
Product		0.54–0.98	0.54–0.98
Phosphorus, max, %			
Heat		0.04	0.04
Product		0.05	0.05
Sulfur, max, %			
Heat	0.05	0.05	0.05
Product	0.06	0.06	0.06
Copper, min, % (when specified)			
Heat	0.20	0.20	0.20
Product	0.18	0.18	0.18

^A Optional with the manufacturer but shall be compatible with weldable steel.

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Similar to A36

Grade 36

ASTM A1554-07a
Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

TABLE 2 Chemical Requirements for Grades 55 and 105

Element	Composition, %	
	Heat Analysis	Product Analysis
Phosphorous, max	0.040	0.048
Sulfur, max	0.050	0.058
Copper, min (when Cu is specified)	0.20	0.18

No controls on carbon
or alloy content

Grade 55

Grade 105

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ASTM A1554-07a
 Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

Grade 55 S1

S1. Grade 55 Bars and Anchor Bolts

S1.1 The material described in this section is intended for welding. This supplemental section, by chemical composition restrictions and by a carbon equivalent formula, provides assurance of weldability.

S1.2 Welding technique is of fundamental importance when bolts produced to this supplementary section are welded. It is assumed that suitable welding procedures for the steel being welded and the intended service will be selected.

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 Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

Grade 55 S1

S1.5 *Chemical Composition:*

S1.5.1 Steel shall conform to the following limitations:

	Heat Analysis	Product Analysis
→ Carbon, max, %	0.30	0.33
→ Manganese, max, %	1.35	1.41
← Phosphorus, max, %	0.040	0.048
← Sulfur, max, %	0.050	0.058
→ Silicon, max, %	0.50	0.55

**Cold
Cracking
Controls**

**Hot
Cracking
Controls**

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ASTM A1554-97a
 Standard Specification for Anchor Bolts, Steel, 36, 55, and 105-ksi Yield Strength

Grade 55 S1

S1.5.2 *Carbon Equivalent*—In addition to the requirements specified in S1.5.1, the analysis shall be such as to provide a carbon equivalent (CE) meeting the following requirements:

S1.5.2.1 For alloy or low-alloy steel, the carbon equivalent shall not exceed 0.45 % when calculated as follows:

$$CE = \% C + \frac{\% Mn}{6} + \frac{\% Cu}{40} + \frac{\% Ni}{20} + \frac{\% Cr}{10} + \frac{\% Mo}{50} + \frac{\% V}{10}$$

S1.5.2.2 For carbon steel, the carbon equivalent shall not exceed 0.40 % when calculated as follows:

$$CE = \% C + \frac{\% Mn}{4}$$

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Grade 36

- Chemistry is similar to that of ASTM A36
- Deviation on Mn permitted only for smaller rods
- If Grade 55 is substituted, only weldable (S1) material may be used

Weldability should be good.

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Grade 55

- The only chemistry control is on S, P (and Cu, when Cu is specified)
- No weldability promises

Weldability should be investigated on a case-by-case basis.

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Grade 55 S1

- Chemistry is similar to that of ASTM A36
- Carbon equivalency limits
- “The material described in this section is intended for welding.”
- “This supplemental section...provides assurance of weldability.”

Weldability should be good.

36



Grade 105

- The only chemistry control is on S, P (and Cu, when Cu is specified)
- No weldability promises
- High strength (105 ksi yield)
- May be quenched and tempered

Weldability is likely to be poor.

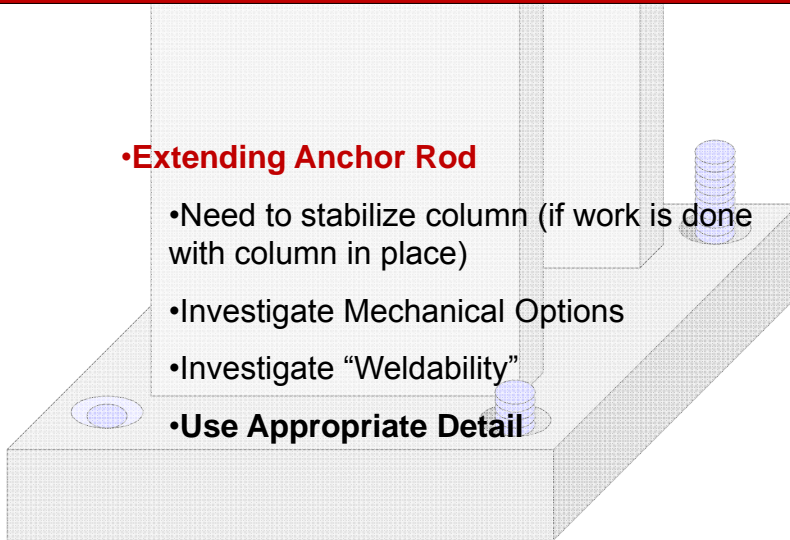
Caveat: poor weldability does not mean unweldable.

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Special Welding Applications and Field Fixes: Extending Anchor Rods

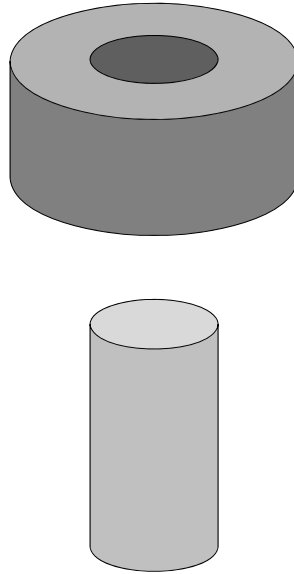
•Extending Anchor Rod

- Need to stabilize column (if work is done with column in place)
- Investigate Mechanical Options
- Investigate “Weldability”
- Use Appropriate Detail



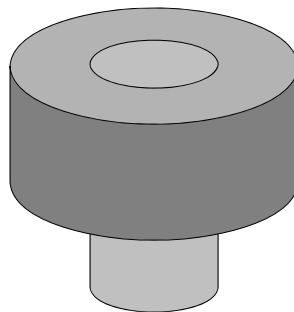
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Cut “donut” from weldable steel—same ID as OD of rod.

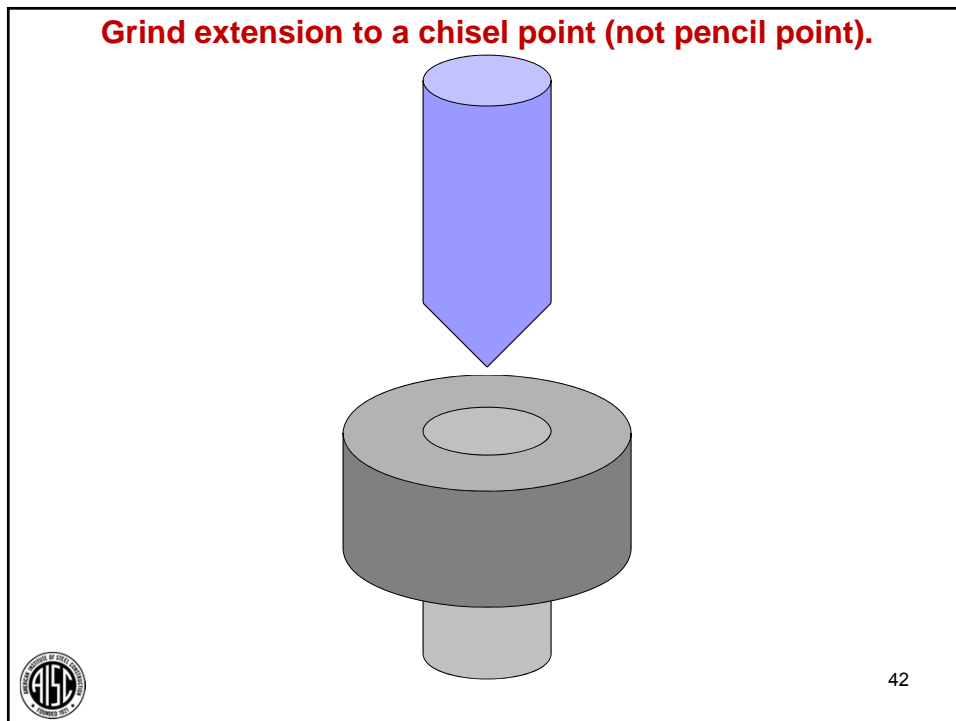
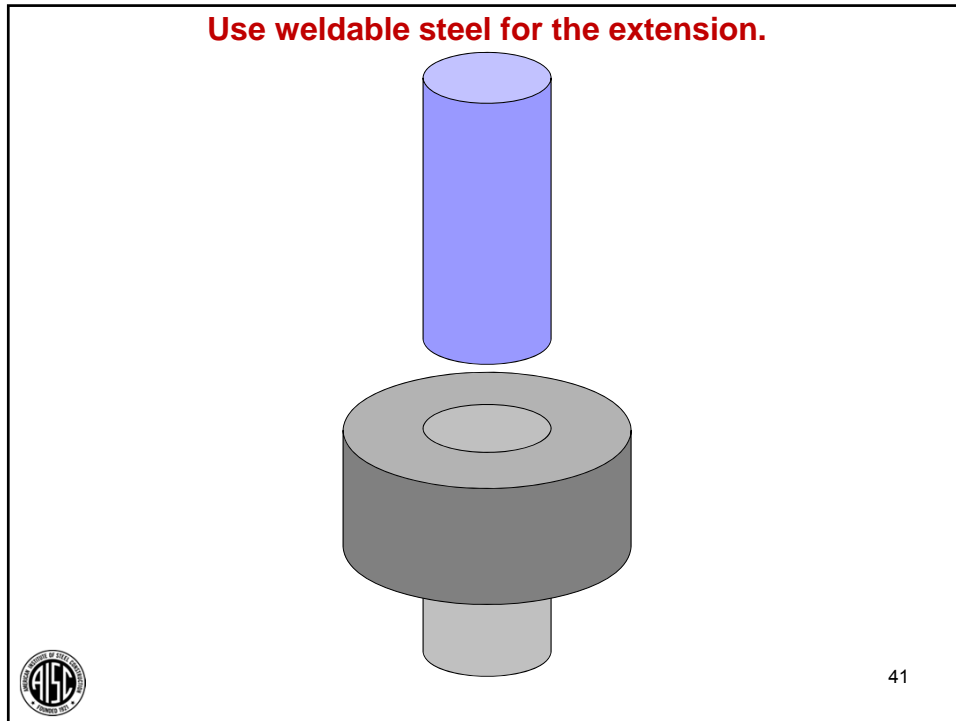


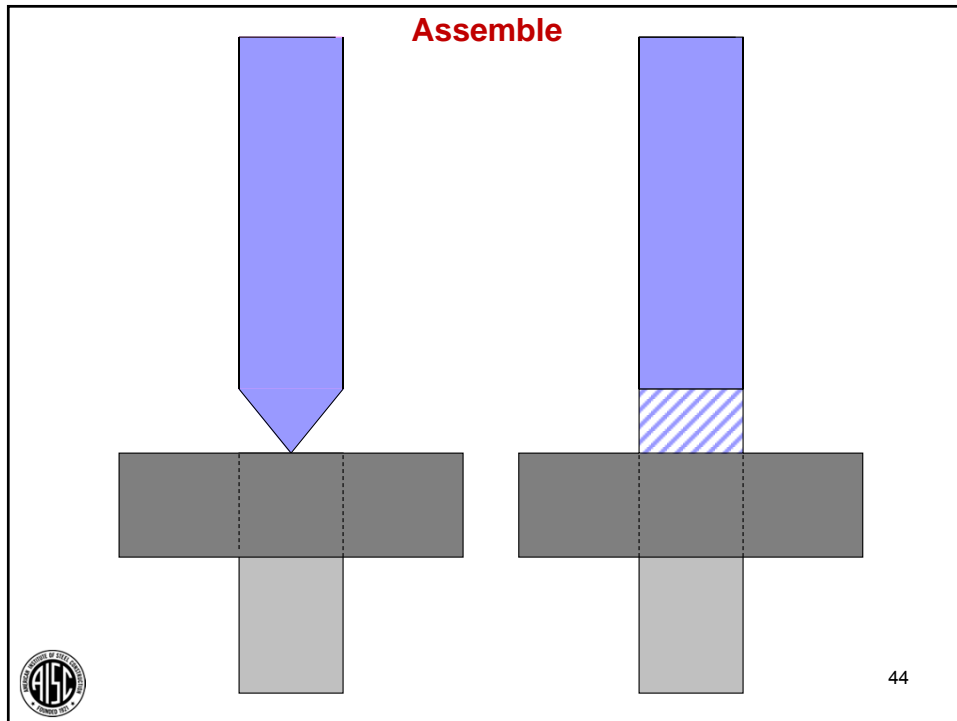
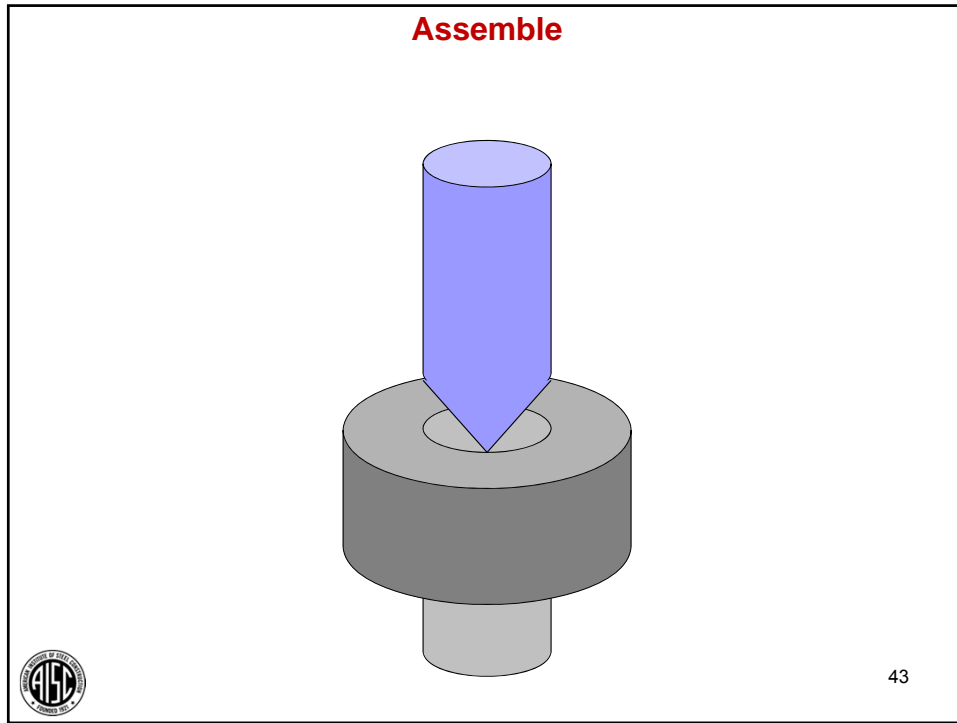
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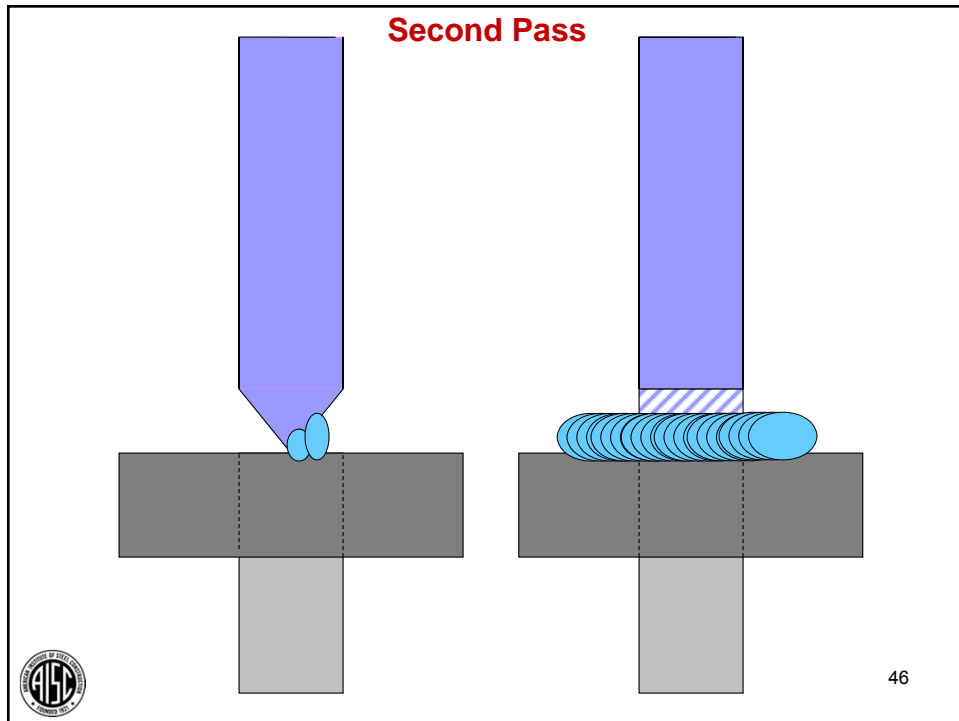
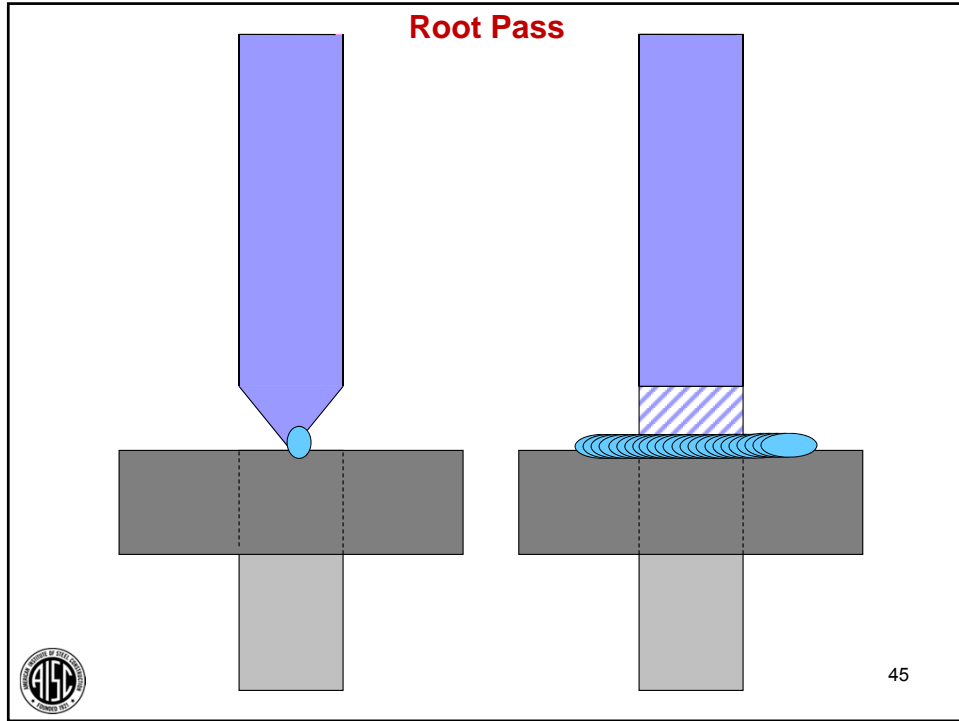
“Donut” acts as weld tab and shelf bar.

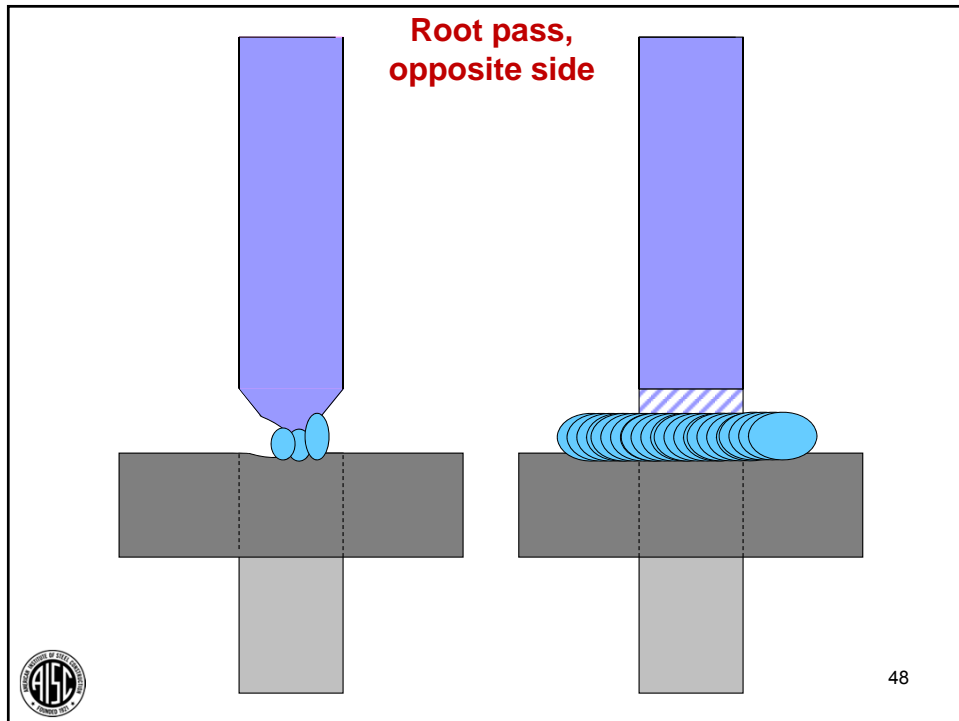
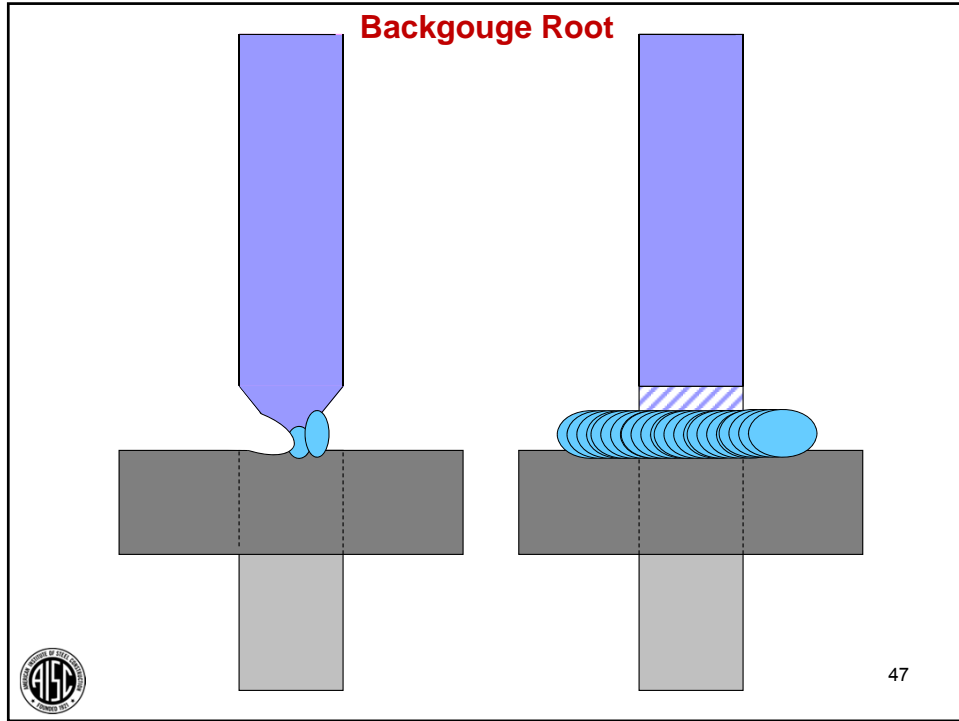


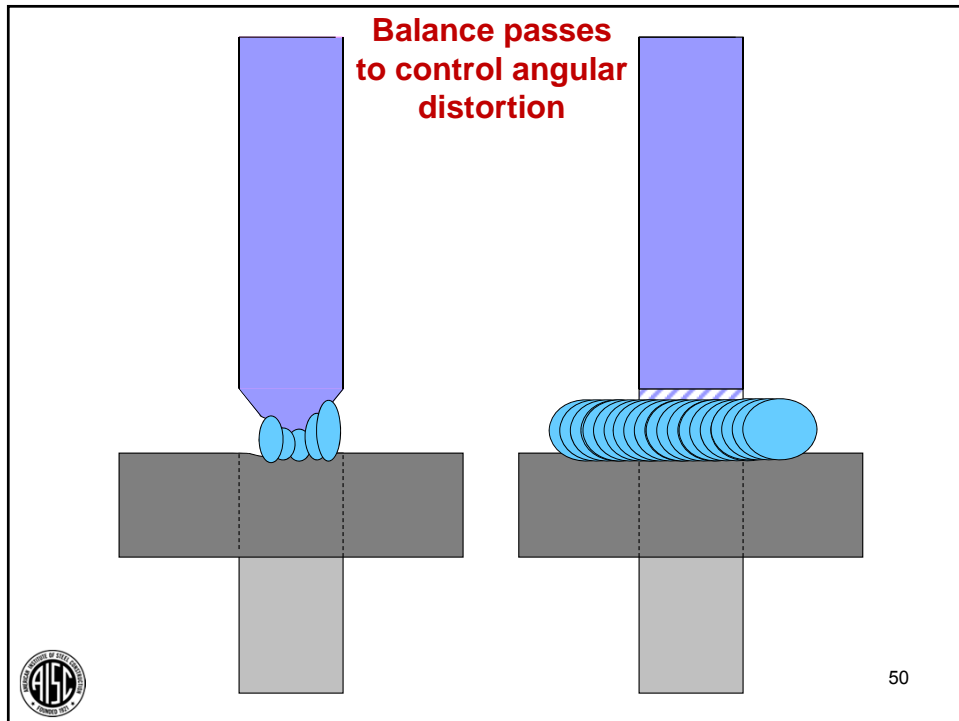
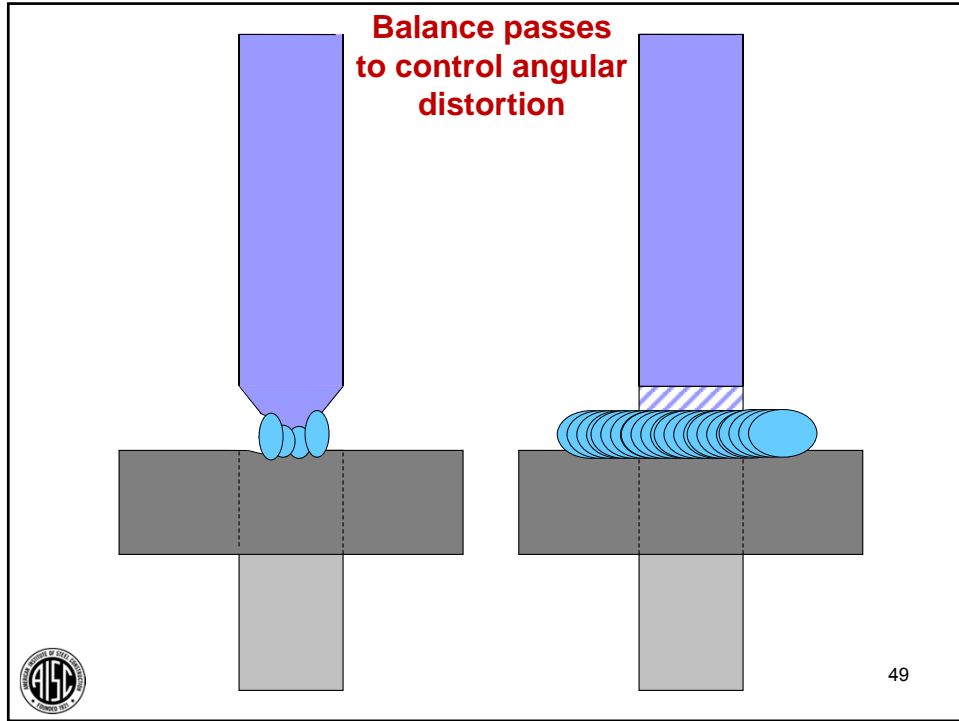
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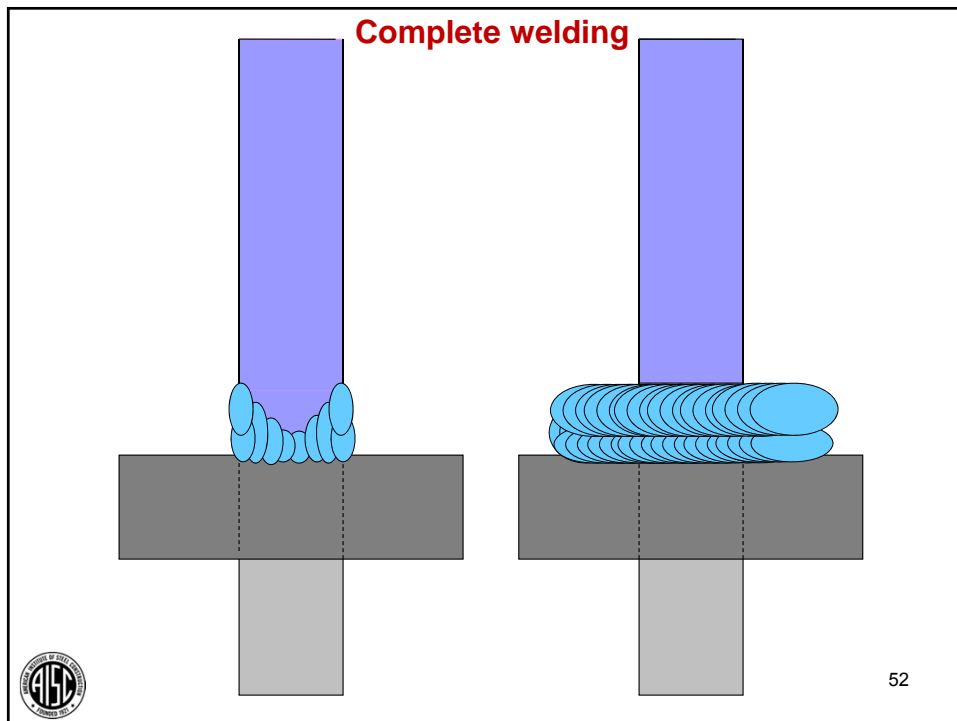
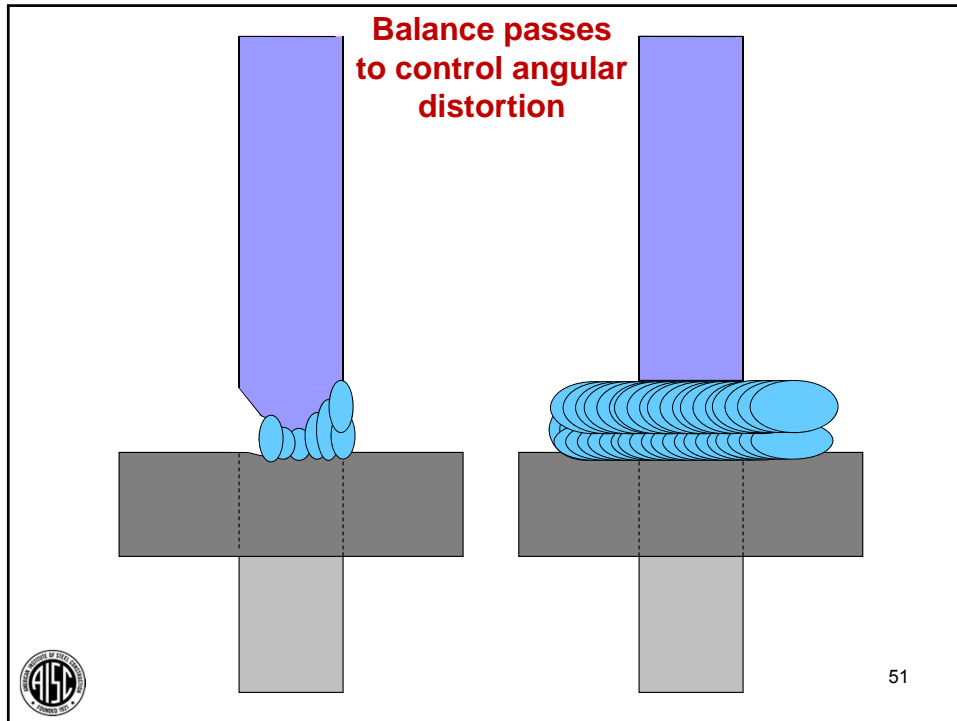


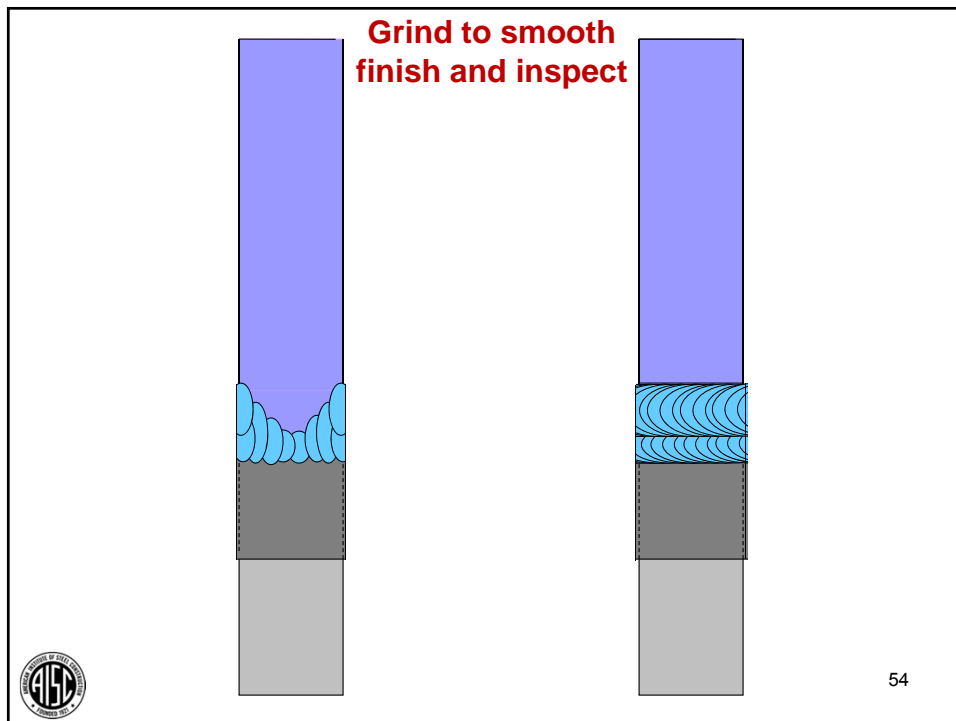
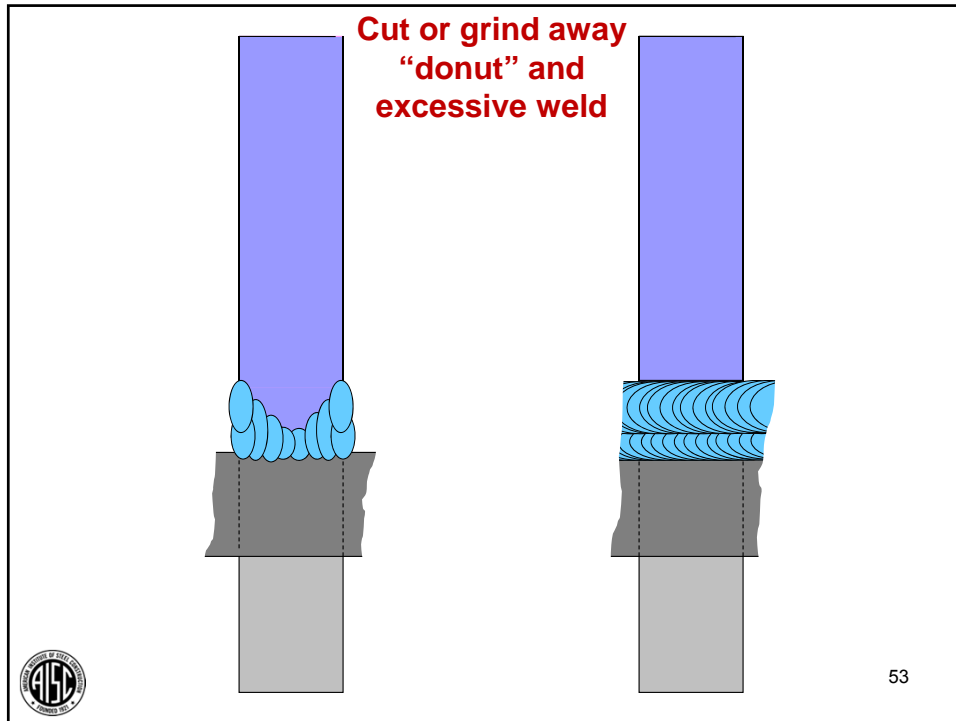


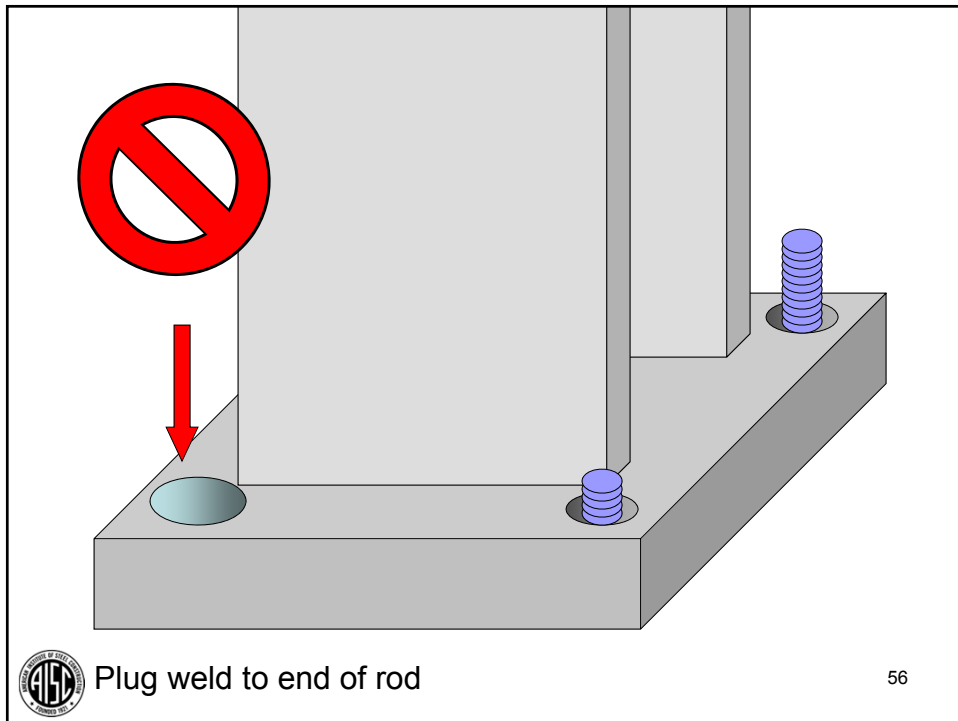
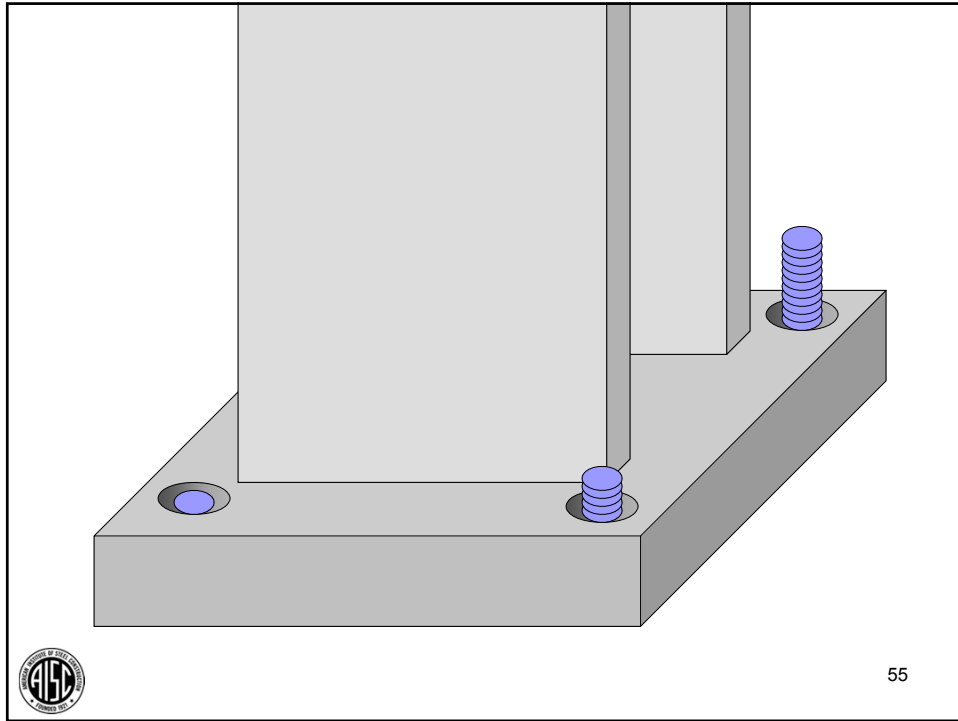


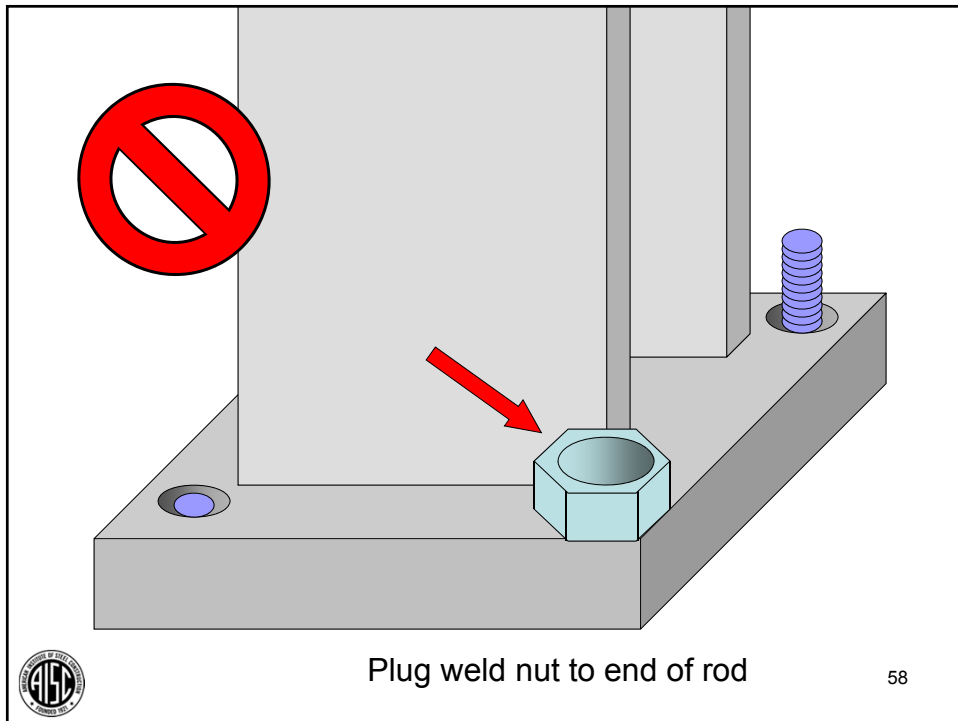
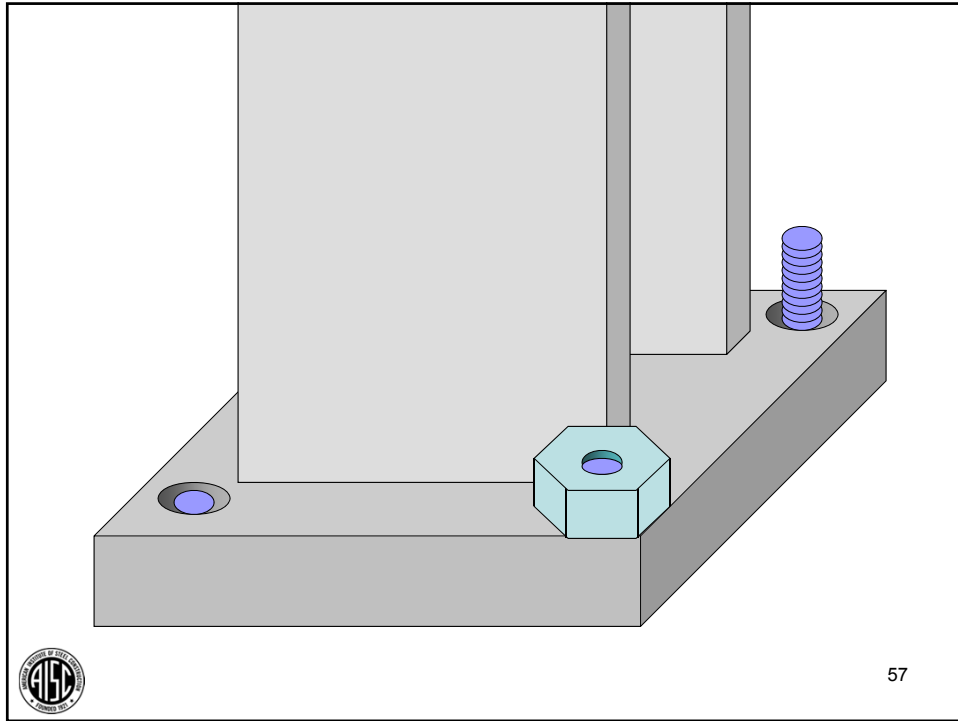












Special Welding Applications and Field Fixes

- Welding on Anchor Rods
- ➔ • Welding on Heavy Sections (“Jumbo Shapes”)
- Welding HSS
- Welding AESS
- Field Welding
- Welding on Existing Structures
- Combining Welds and Bolts



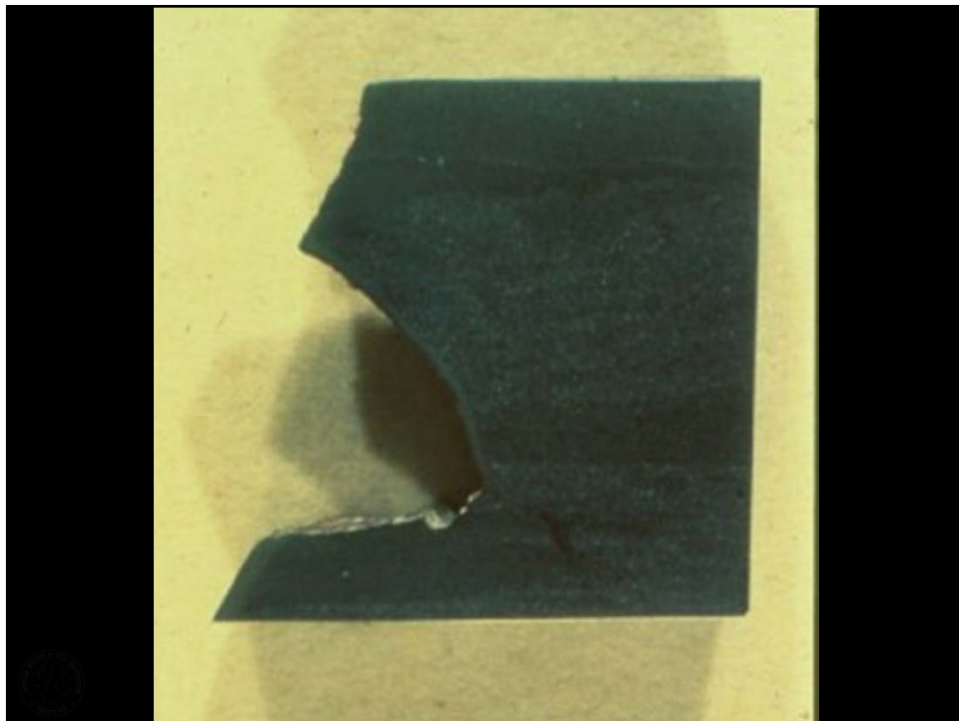
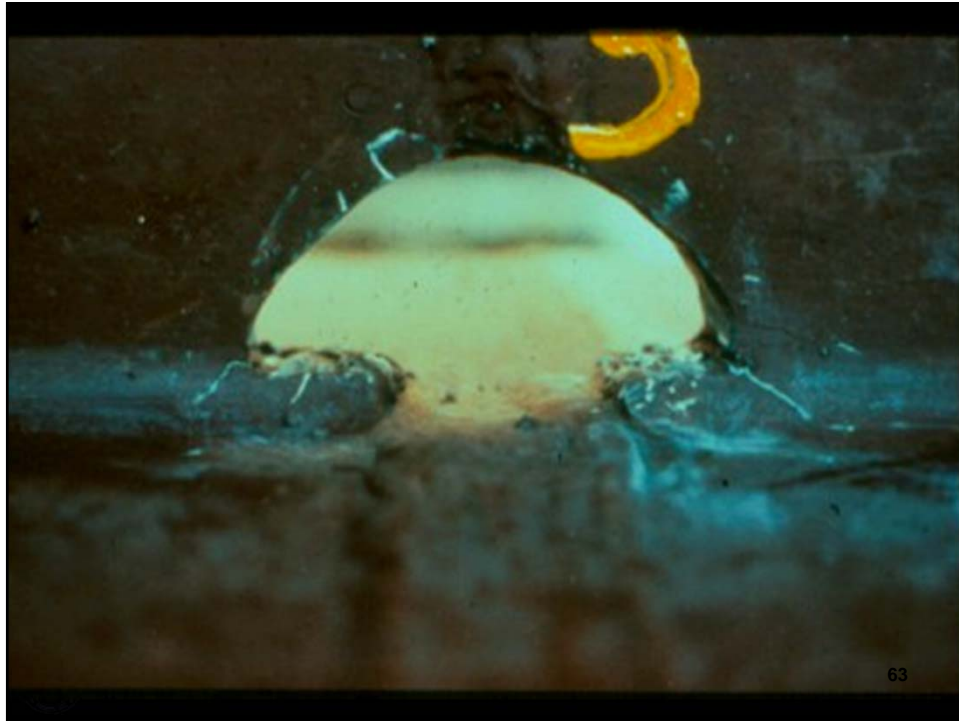
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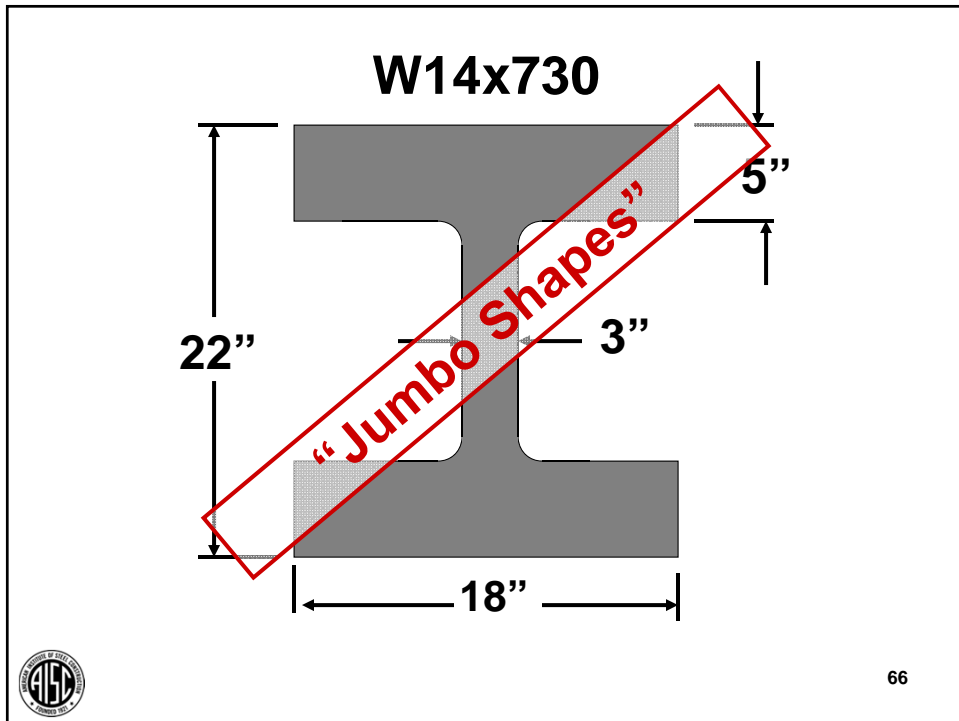
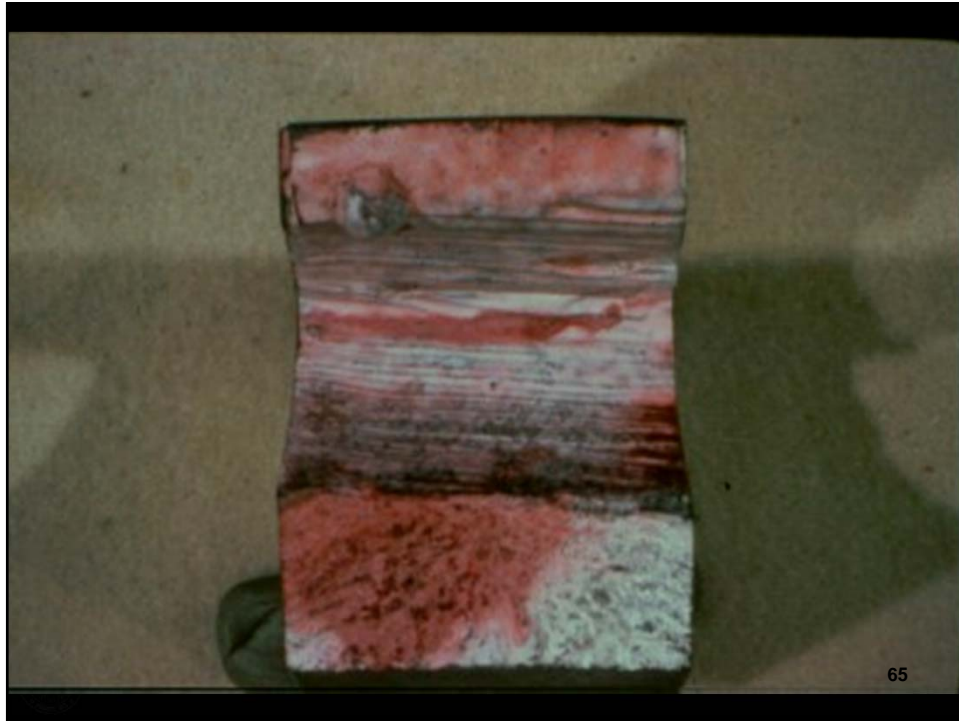


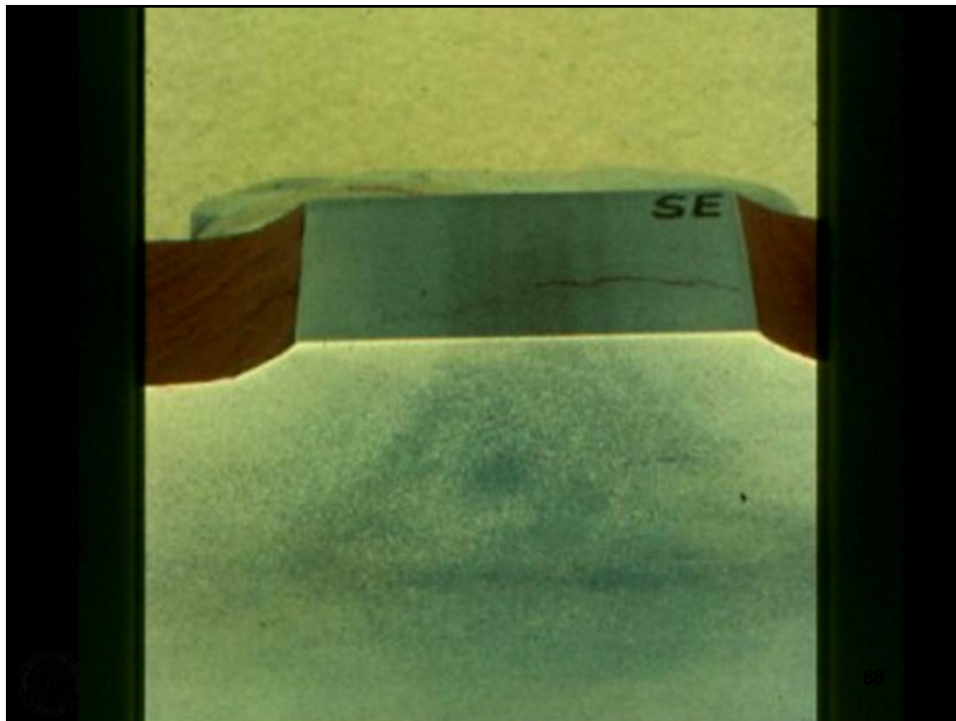
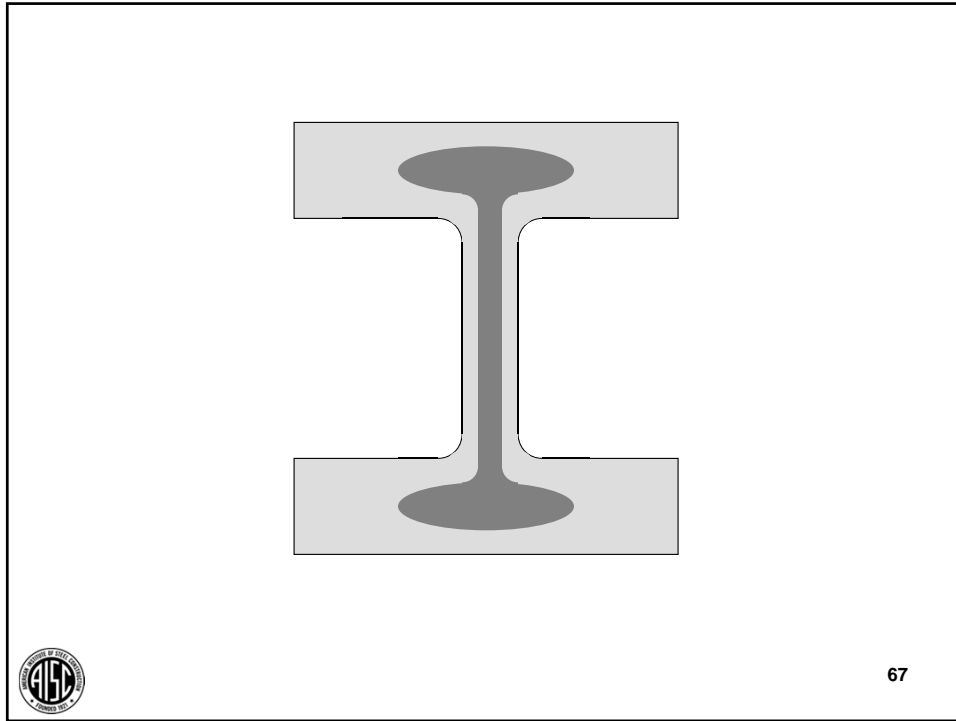
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AISC 360-10 SPECIFICATION

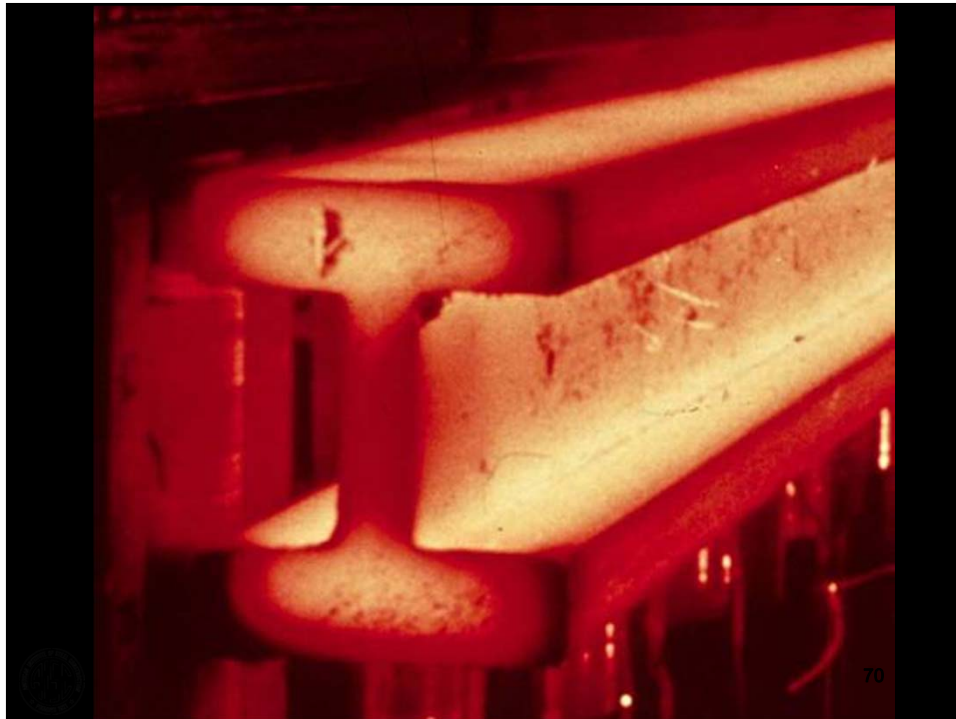


Commentary A3.1c
Rolled Heavy Shapes

The web-to-flange intersection and the web center of heavy hot-rolled shapes, as well as the interior portions of heavy plates, may contain a more coarse grain structure and/or lower notch toughness material than other areas of these products.

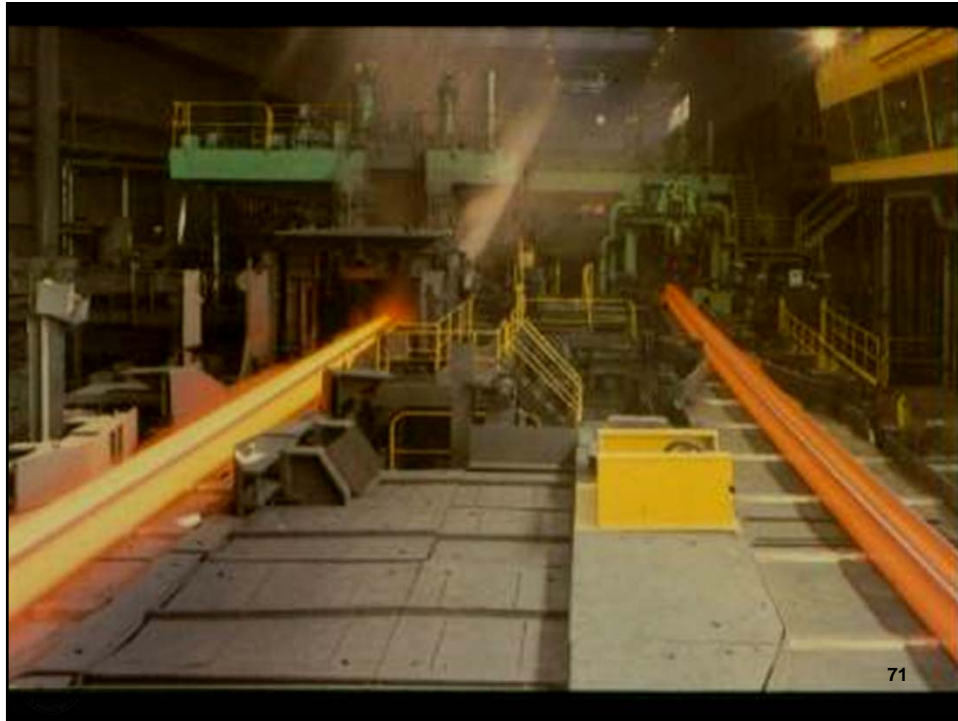


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AISC 360-10 SPECIFICATION



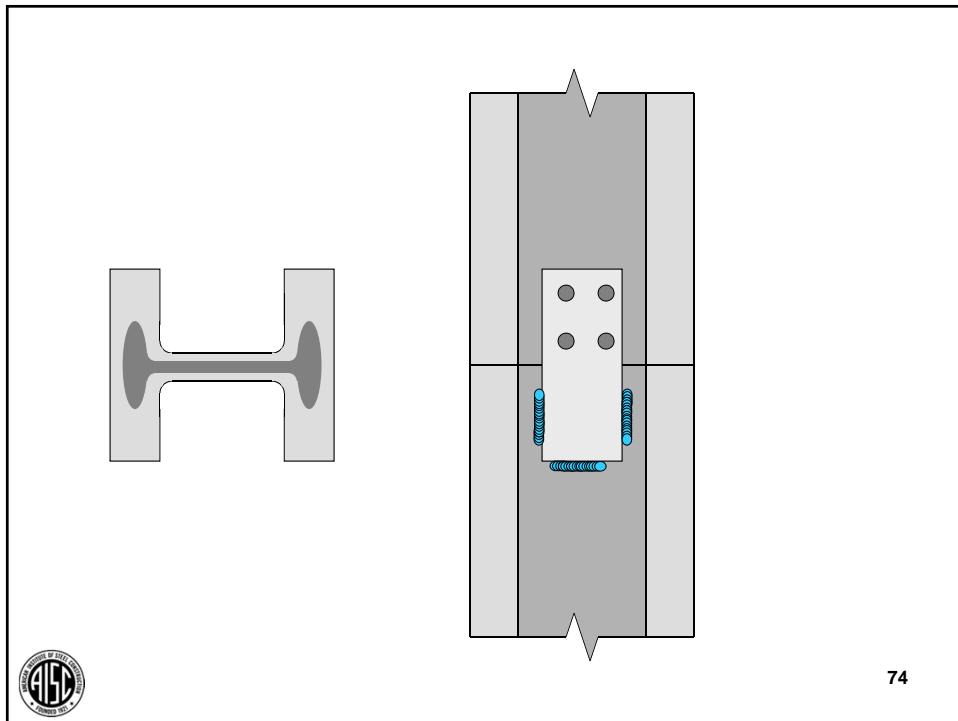
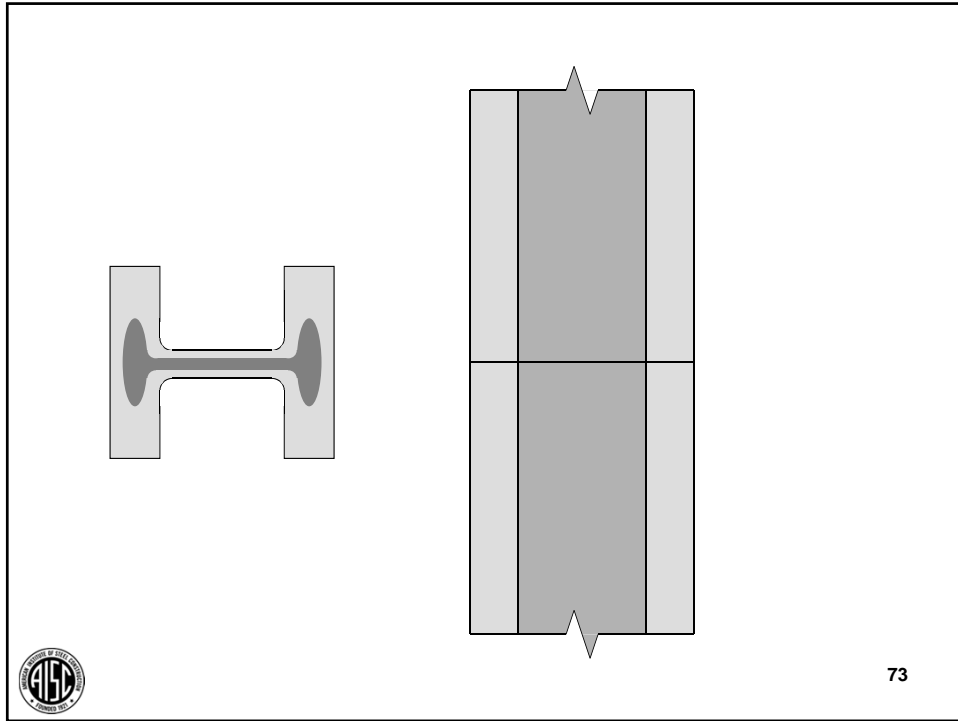
Commentary A3.1c

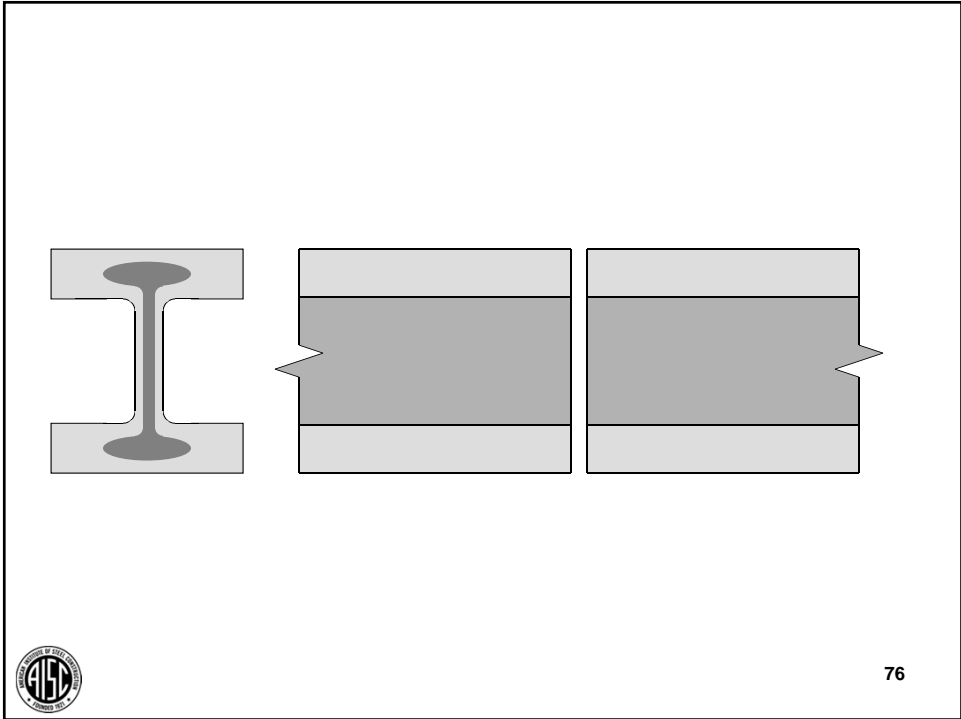
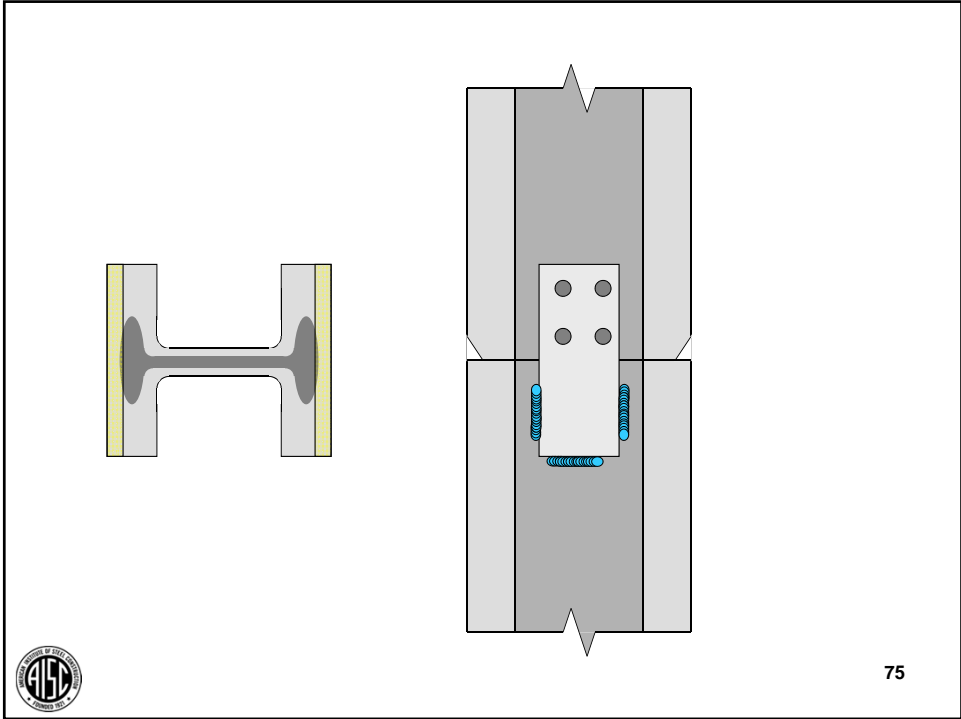
This characteristic is not detrimental to suitability for compression members or for nonwelded members. However, when heavy cross sections are joined by splices or connections using complete –joint-penetration (groove) welds that extend through the coarser and/or low notch-tough interior portions, tensile strains induced by welding may result in cracking.

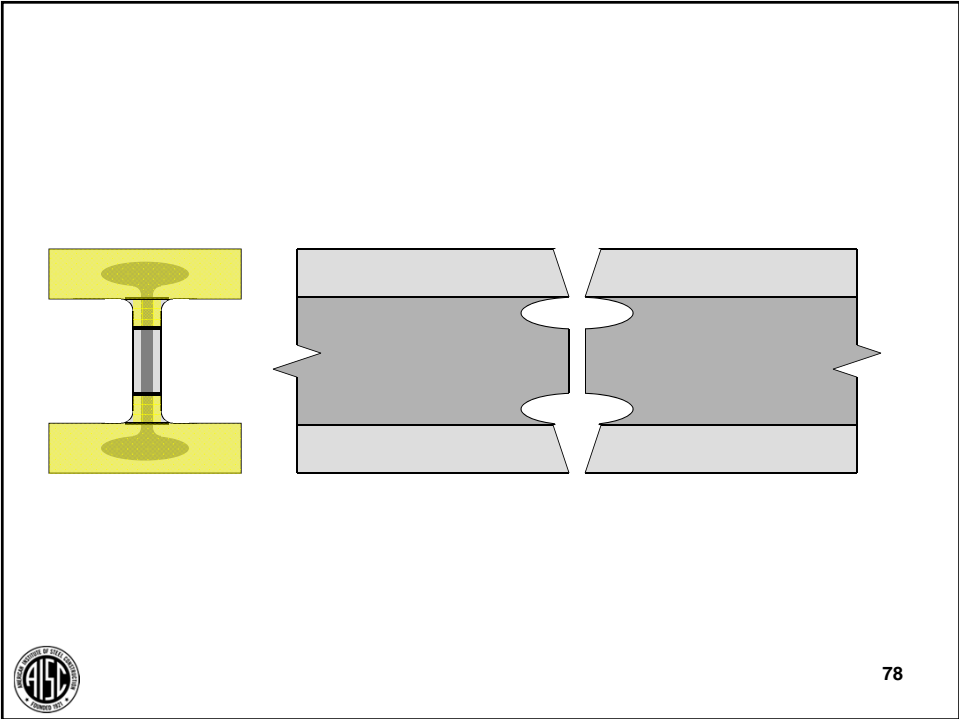
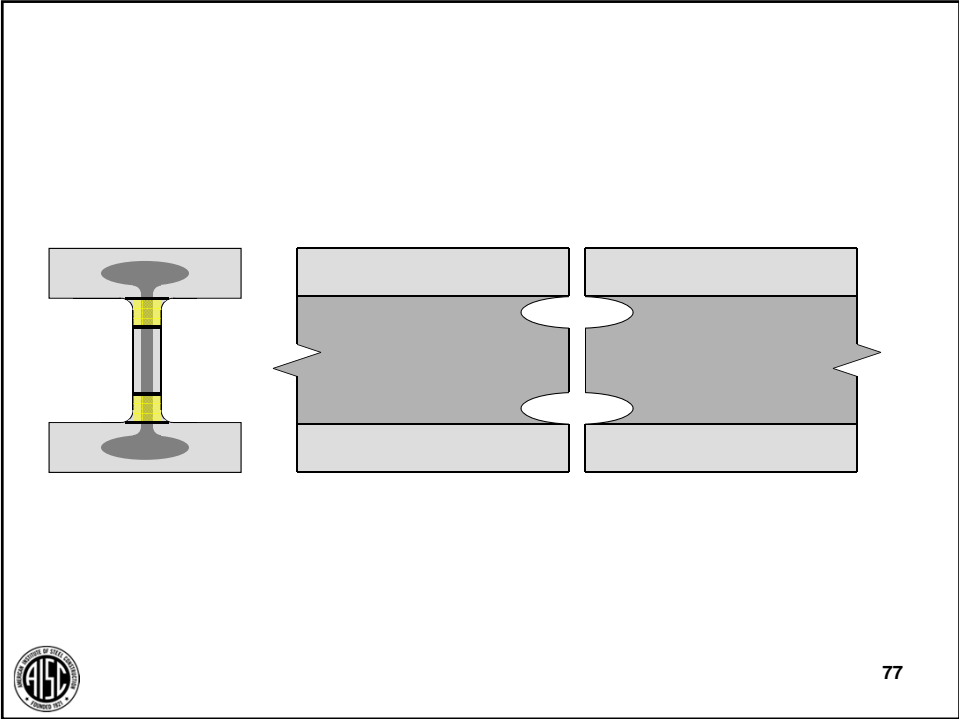


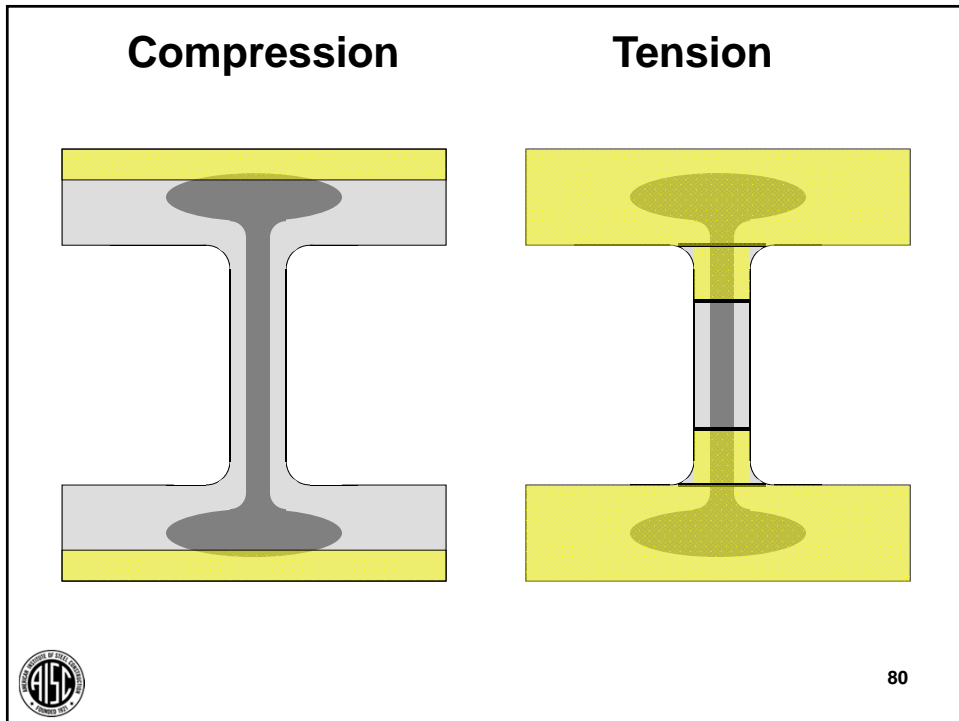
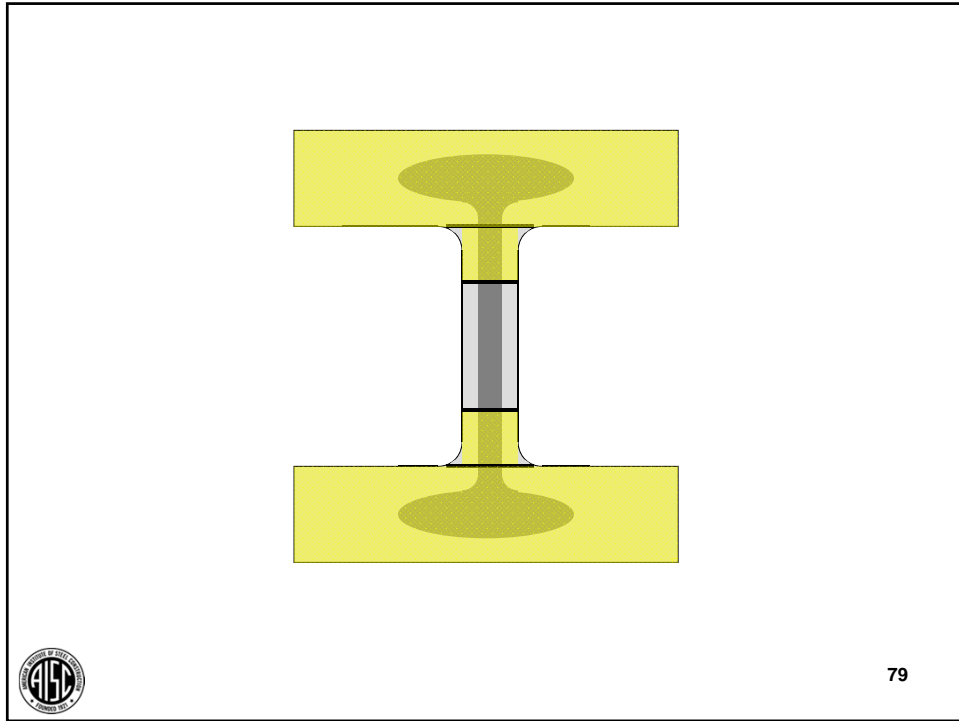
72











AISC 360-10 SPECIFICATION



Commentary A3.1c
Rolled Heavy Shapes

The web-to-flange intersection and the web center of heavy hot-rolled shapes, as well as the interior portions of heavy plates, may contain a more coarse grain structure and/or lower notch toughness material than other areas of these products.

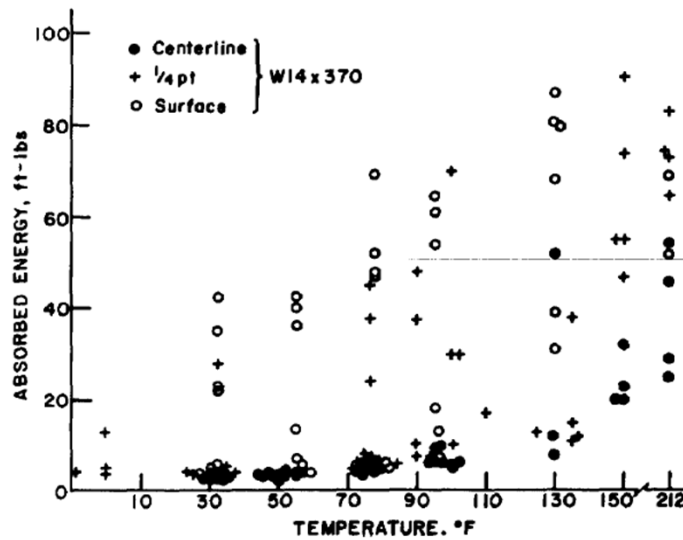


Fig. 15. Charpy V-Notch test results for W14 × 370 section—
 Supplier A



AISC 360-10 SPECIFICATION

ASTM A6, Supplementary Requirement S30 *Charpy V-Notch Impact Tests for Structural Shapes—Alternate Core Location*


**20 ft-lbs (27J) @ +70 °F
(+21 °C)**

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AISC 360-10 SPECIFICATION

ASTM A6, Supplementary Requirement S5 Charpy V-Notch Impact Test



20 ft-lbs (27J) @ +70 °F (+21 °C)





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AISC 360-10 SPECIFICATION

J2.6 Filler Metal Requirements

20 ft-lbs (27J) @ +40 °F (+4 °C)



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AISC 360-10 SPECIFICATION



Commentary A3.1c

To minimize the potential for fracture, the notch toughness requirement of Section A3.1c must be used in conjunction with good design and fabrication procedures.



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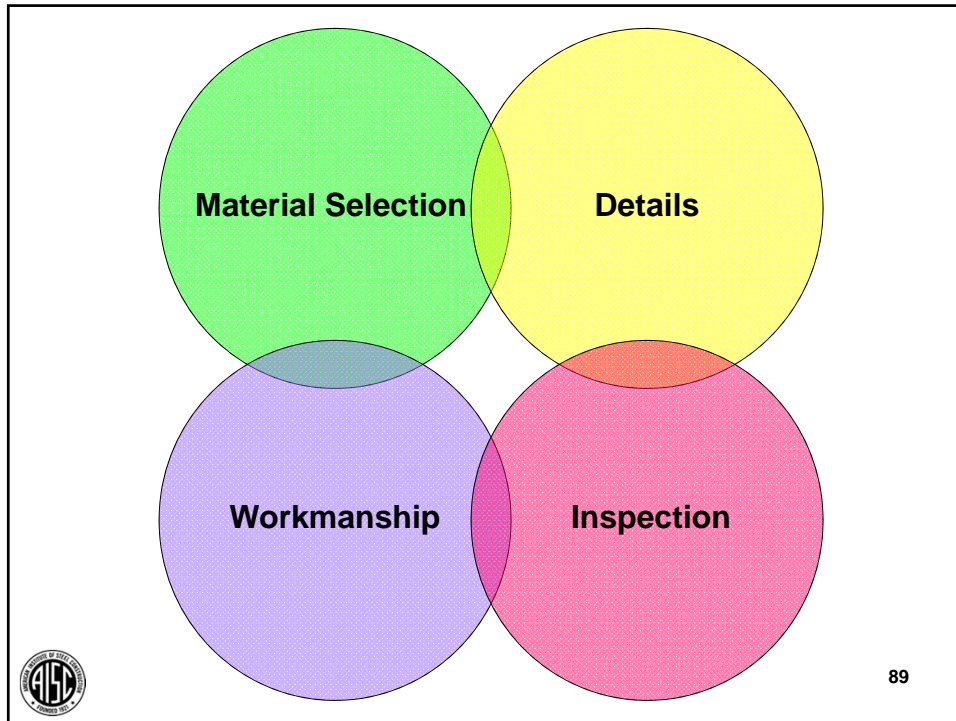
Commentary A3.1a
ASTM Designations

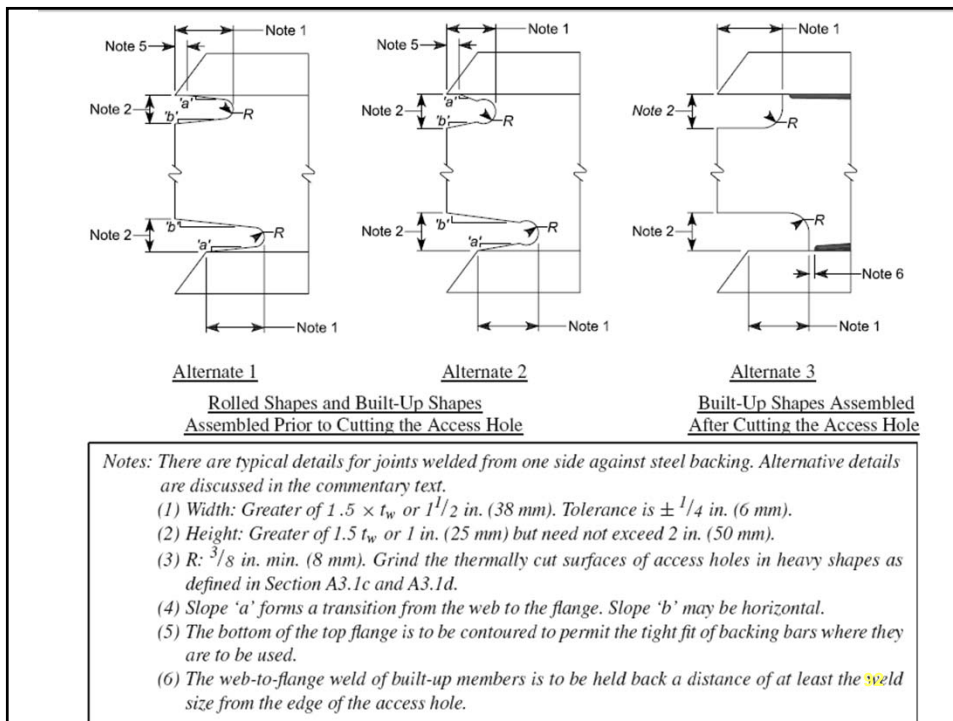
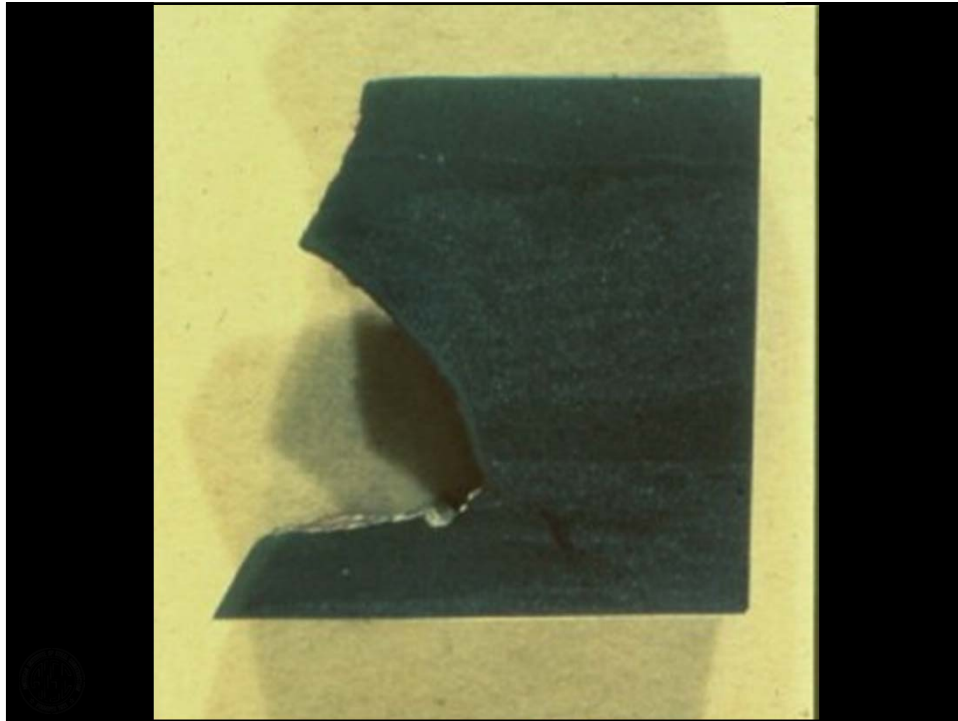
Rolled steel is anisotropic, especially insofar as ductility is concerned; therefore, weld contraction strain in the region of highly restrained welded connections may exceed the strength of the material if special attention is not given to material selection, details, workmanship and inspection.

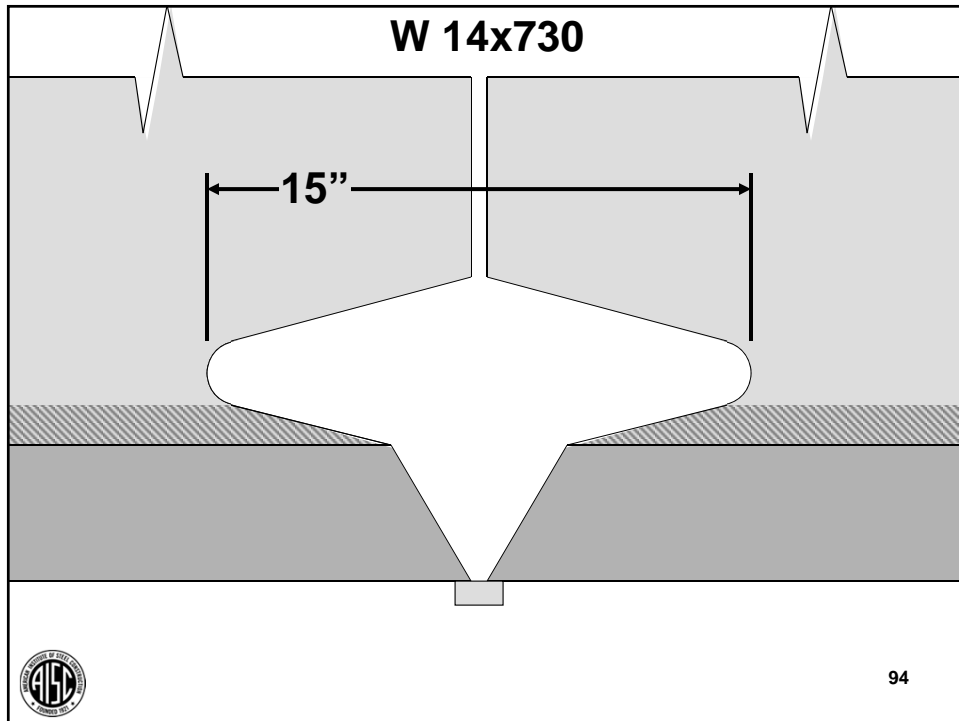
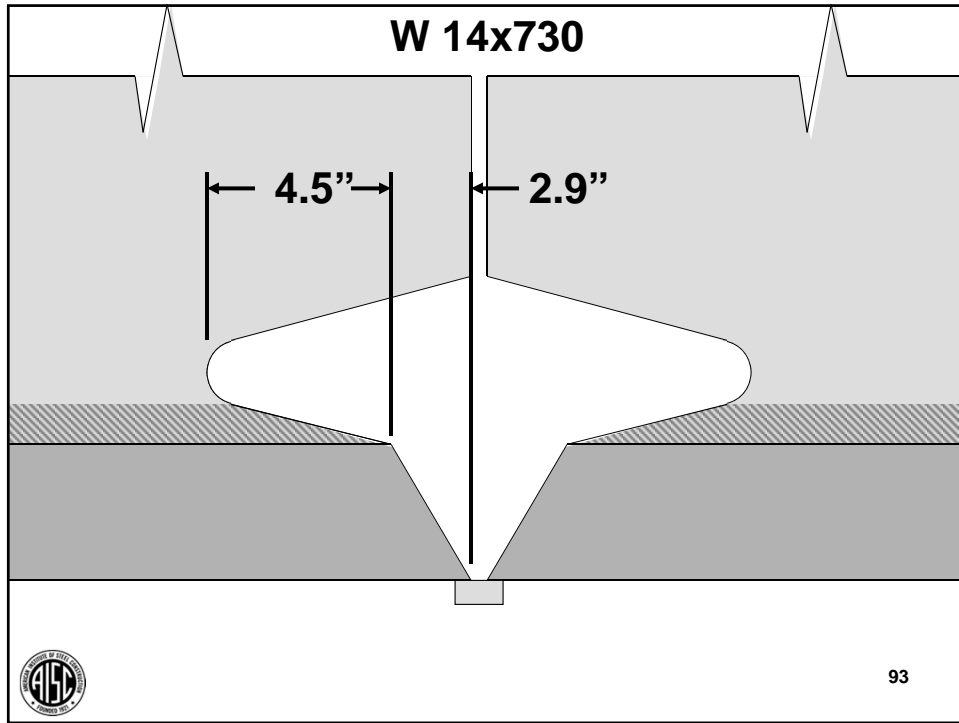


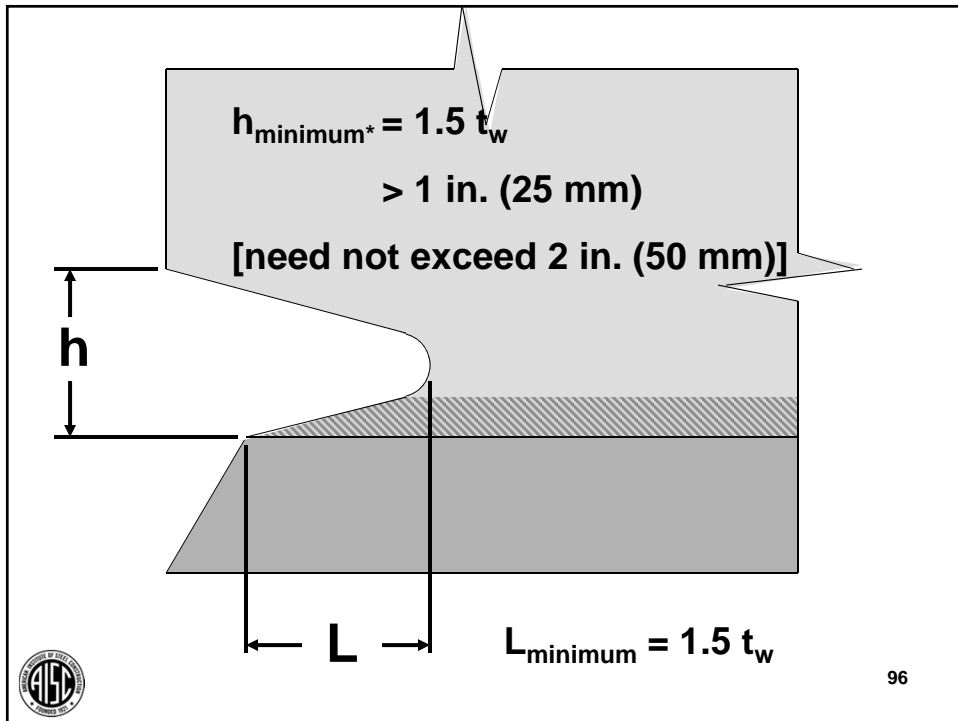
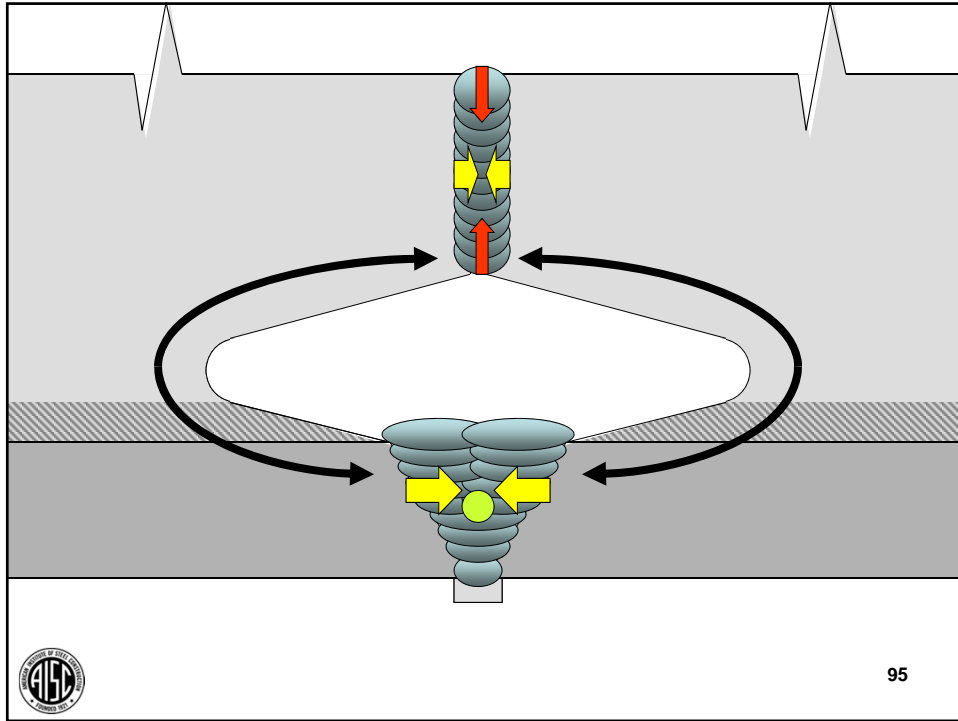
88













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M2.2 Thermal Cutting

For beam copes and weld access holes in which the curved part of the access hole is thermally cut in hot rolled ASTM A6/A6M shapes with a material thickness greater than 2 in. (50 mm), and in welded built-up shapes with a material thickness greater than 2 in. (50 mm), a preheat temperature of not less than 150 °F (66 °C) shall be applied before thermal cutting.



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AISC 360-10 SPECIFICATION



M2.2 Thermal Cutting

The thermally cut surface of access holes in ASTM A6/6M hot-rolled shapes with a flange thickness exceeding 2 in. (50 mm) and built-up shapes with a material thickness greater than 2 in. (50 mm) shall be ground.



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N5.5 Nondestructive Testing of Welded Joints

5c Access Hole NDT

Thermally cut surfaces of access holes shall be tested by QA using MT or PT, when the flange thickness exceeds 2 in. (50 mm) for rolled shapes, or when the web thickness exceeds 2 in. (50 mm) for built-up shapes.




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Preheat to 150 °F before thermal cutting

Grind after thermal cutting

Inspect with PT or MT




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Preheat to 150 °F before thermal cutting

Grind after thermal cutting

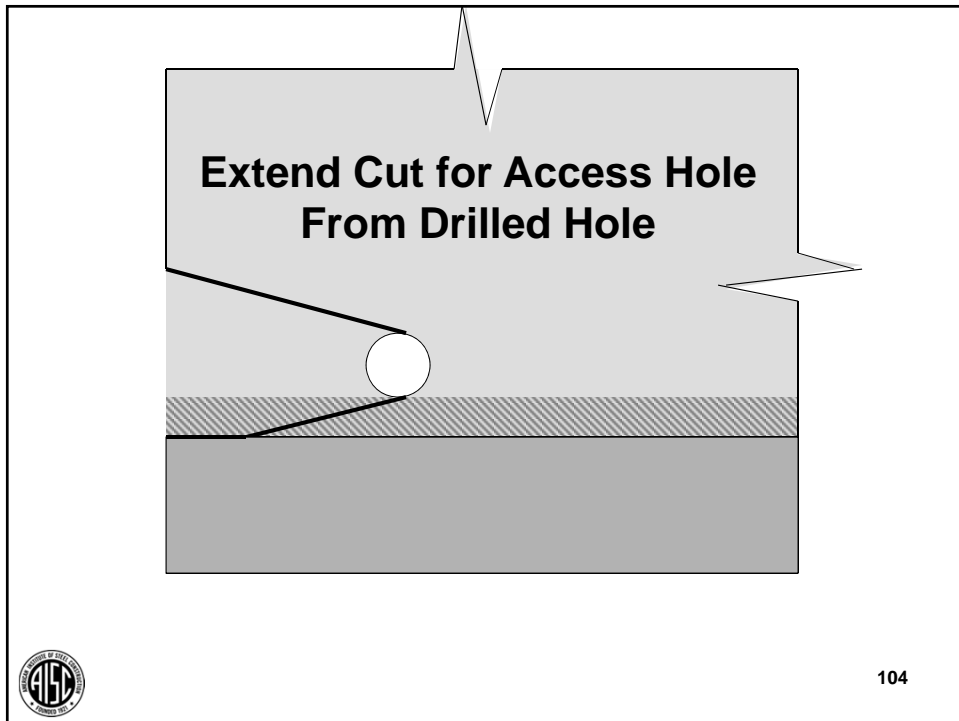
~~**Inspect with PT or MT**~~

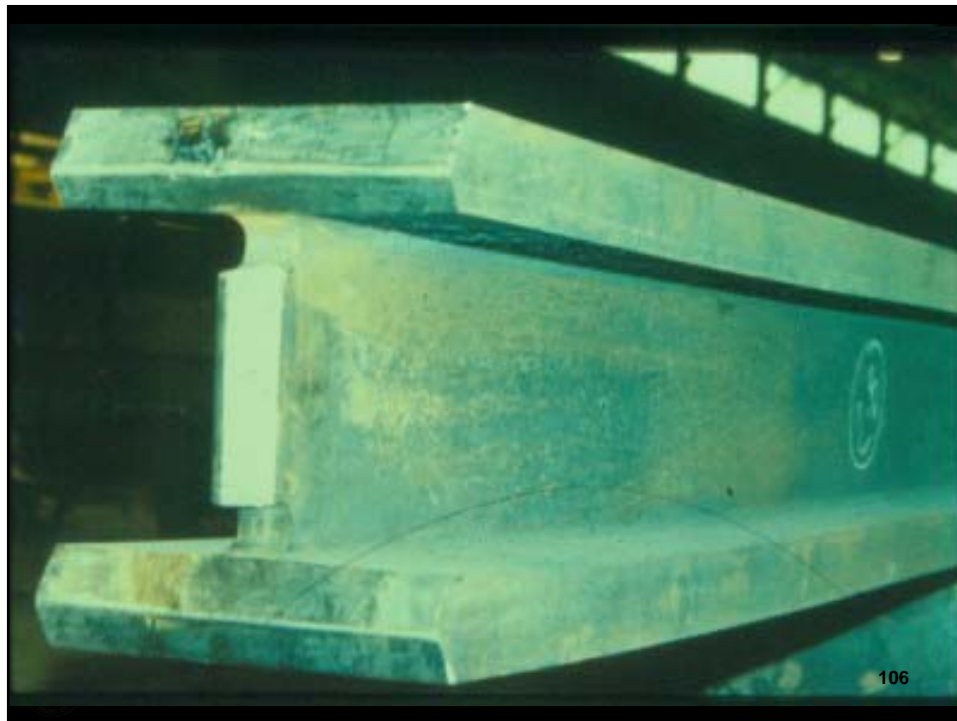
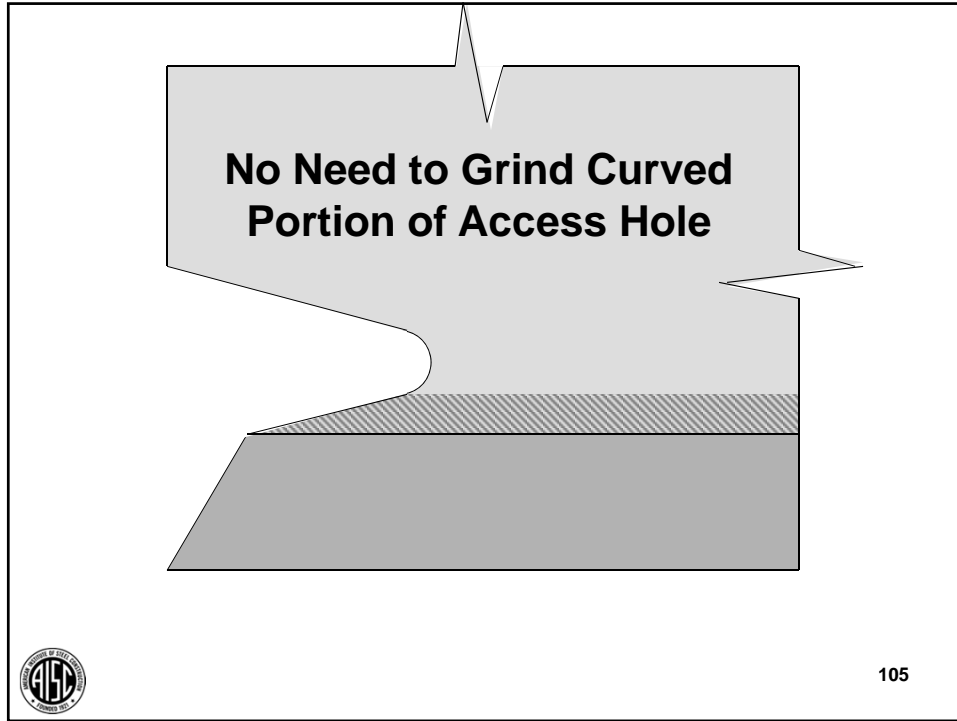
New in 2016



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AWS D1.1:2015 Structural Welding Code--Steel



5.20.6 Temperature Limitations

In making welding under conditions of severe external shrinkage restraint, once the welding has started, the joint shall not be allowed to cool below the minimum specified preheat until the joint has been completed or sufficient weld has been deposited to ensure freedom from cracking.



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Commentary C-J1.5


When splicing hot-rolled shapes with flange thicknesses exceeding 2 in. (50 mm) or heavy welded built-up members, these potentially harmful weld shrinkage strains can be avoided by using bolted splices, fillet-welded lap splices, or splices that combine a welded and bolted detail (see Figure C-J1.1).



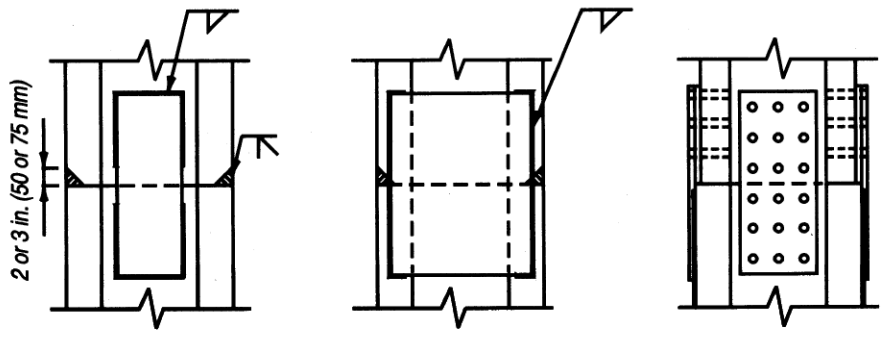
108



AISC 360-10 SPECIFICATION



SPECIFICATION
For Structural
Steel Buildings
June 21, 2010




(a) Shear plate welded to web (b) Shear plate welded to flange tips (c) Bolted splice plates

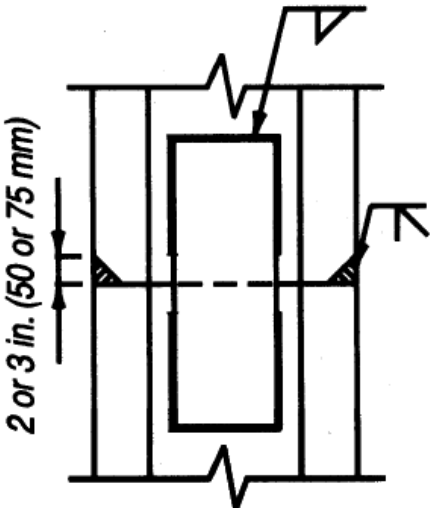
Fig. C-J1.1. Alternative splices that minimize weld restraint tensile stresses.

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AISC 360-10 SPECIFICATION



SPECIFICATION
For Structural
Steel Buildings
June 21, 2010

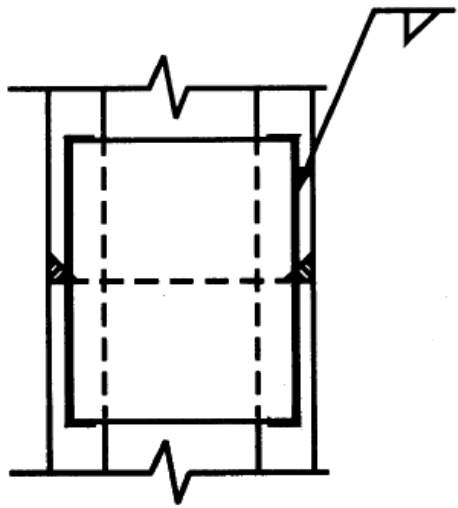


(a) Shear plate welded to web




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AISC 360-10 SPECIFICATION



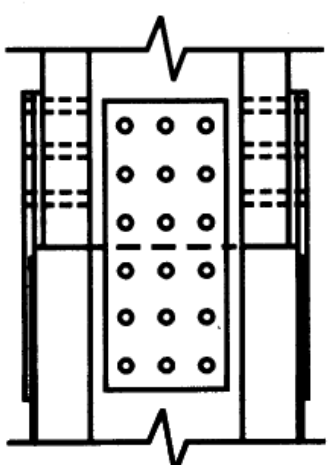
SPECIFICATION
For Structural
Steel Buildings
June 21, 2010

*(b) Shear plate welded
to flange tips*




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AISC 360-10 SPECIFICATION



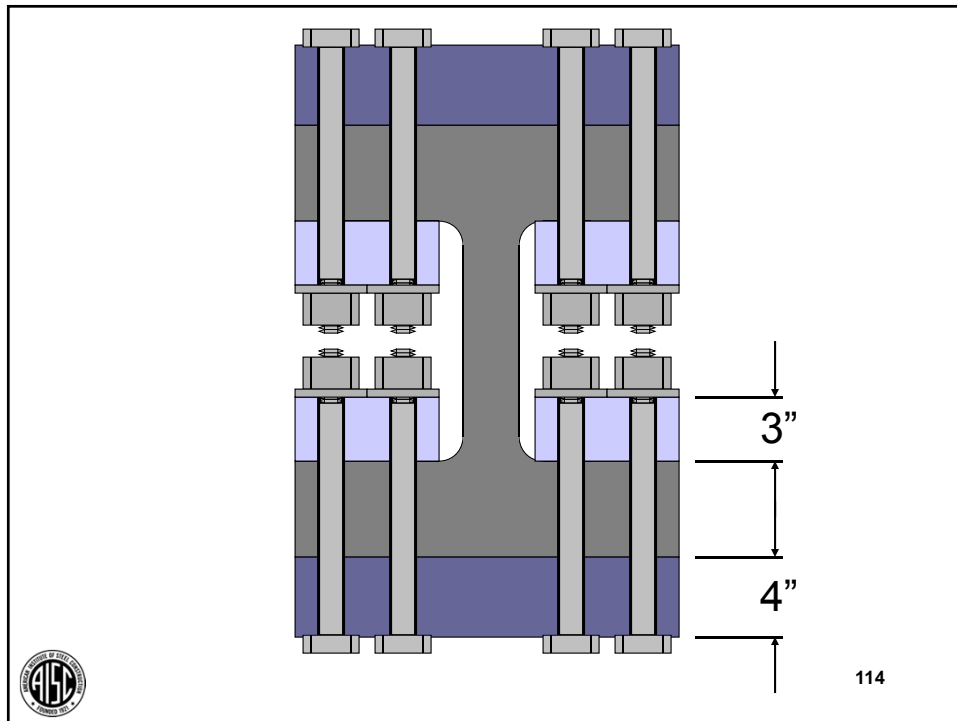
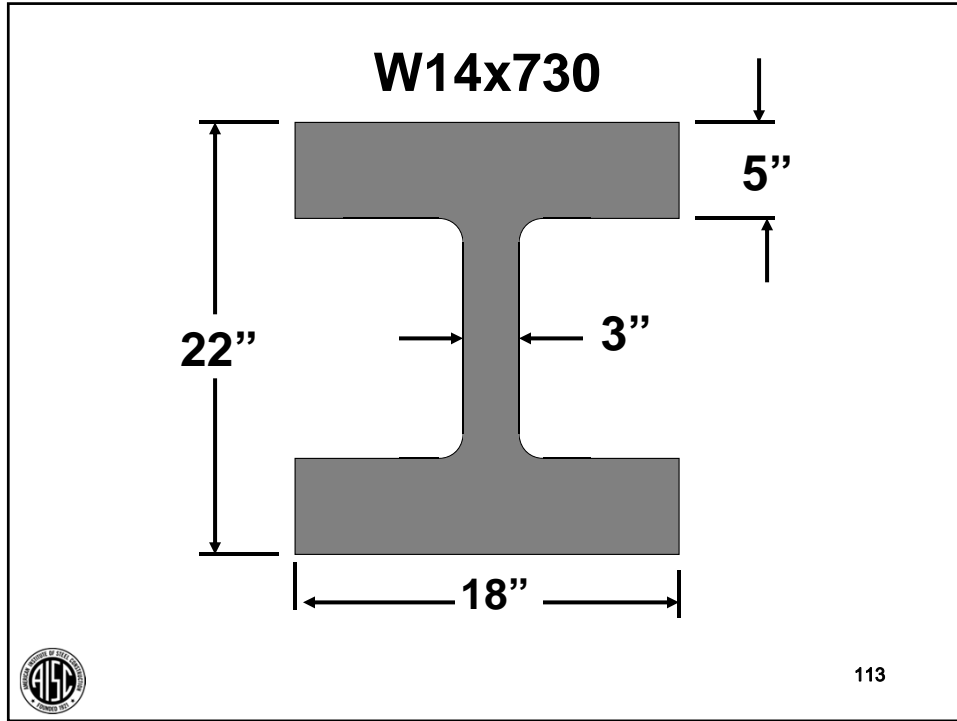
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For Structural
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June 21, 2010

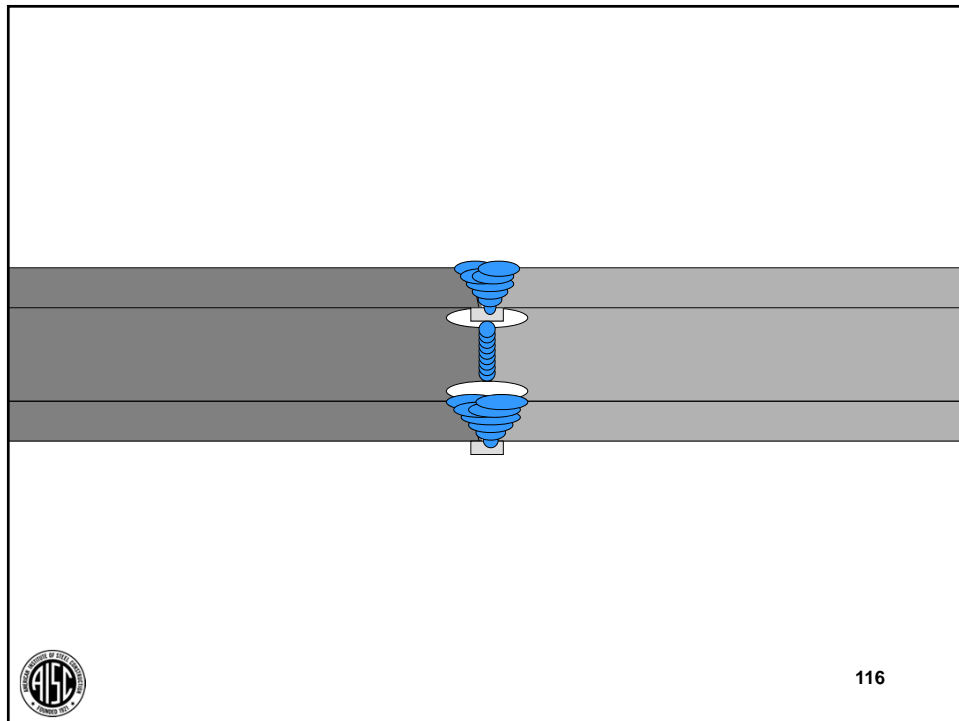
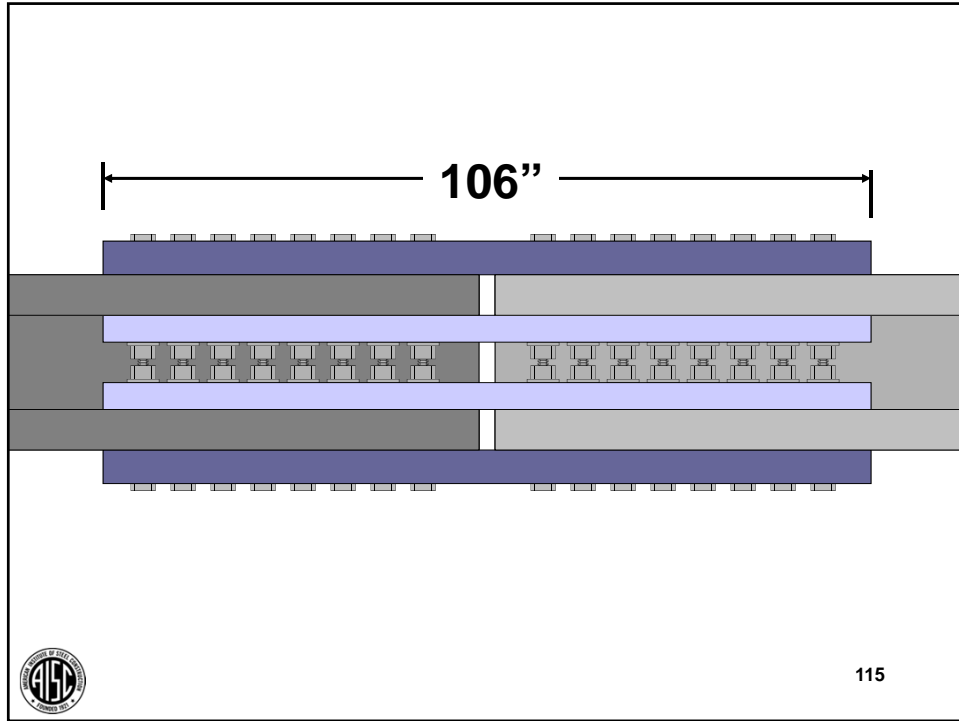
(c) Bolted splice plates

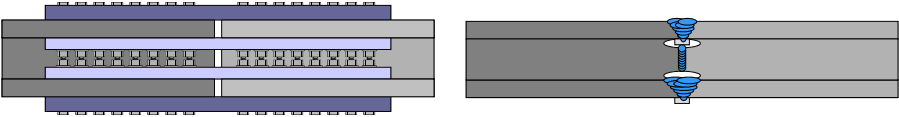


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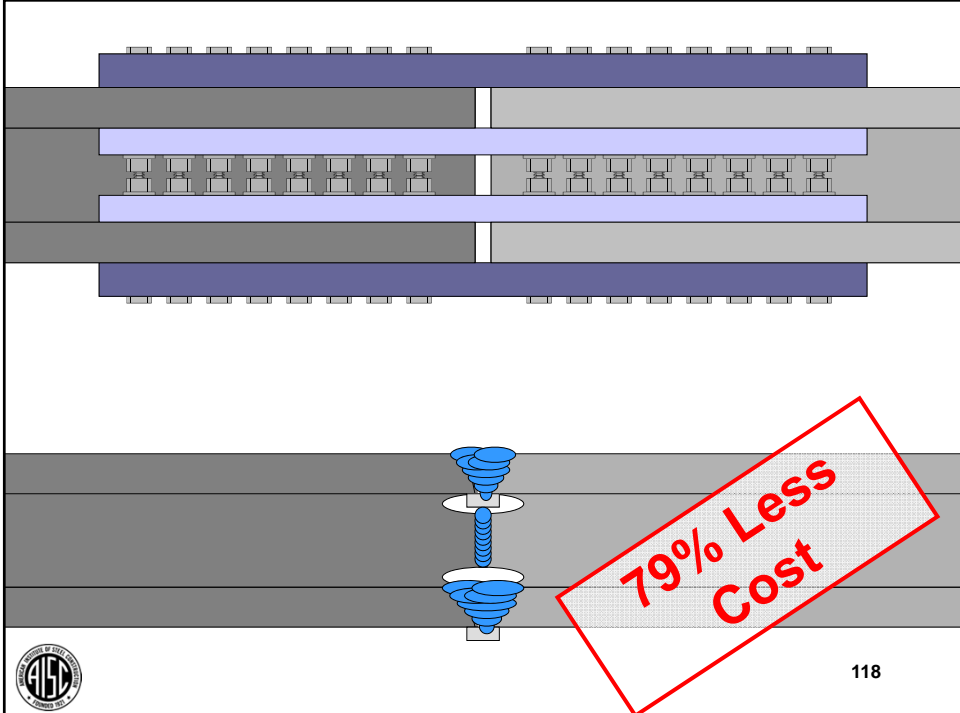






	Bolted Detail		Welded Detail	
Labor	84.3 hr	\$4974	28.6 hr	\$1687
Steel	6900#	\$3312	-	-
Bolts	128	\$1314	-	-
Electrode	-	-	70#	\$88
Flux	-	-	140#	\$164
Total	-	\$9600	-	\$1939

Costs last updated in 2010. 117



79% Less Cost

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Non-column Application of Wide-Flange Shapes

Barsom



“Such fractures can be avoided only when the material, the design, and the fabrication, inspection and erection practices are properly defined and implemented for the particular structure.”



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Non-column Application of Wide-Flange Shapes

Barsom



“Although higher fracture toughness would have been desirable, it would not have prevented the fracture of the tension cord member of the roof truss of the Orlando Civic Center because large fabrication cracks were formed along the perimeter of the thermal cut surfaces of many weld access holes.”



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Non-column Application of Wide-Flange Shapes

Barsom

“Also, because specifications present minimum requirements, the need for additional requirements must be investigated for new and unproven designs, for the use of new materials, for the use of common materials in new and unique applications, and for any other nontraditional situation.”



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Special Welding Applications and Field Fixes

- Welding on Anchor Rods
- Welding on Heavy Sections (“Jumbo Shapes”)
- ➔ • Welding HSS
- Welding AECS
- Field Welding
- Welding on Existing Structures
- Combining Welds and Bolts



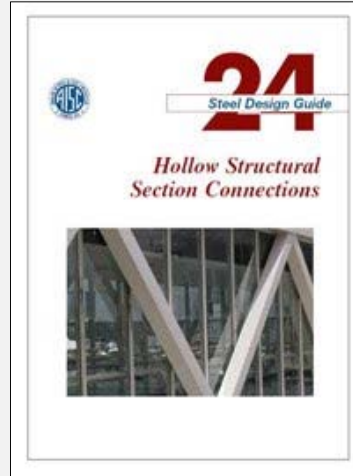
122



**Special Welding Applications and Field Fixes:
Welding HSS**

Design Guide 24

Jeffrey Packer, Ph.D., D.Sc., P.Eng.
Donald Sherman, Ph.D., P.E.
Maura Lecce, Ph.D



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**Special Welding Applications and Field Fixes:
Welding HSS**

HSS Limit States

Typically not limited by the weld.

Connection may dictate the member size

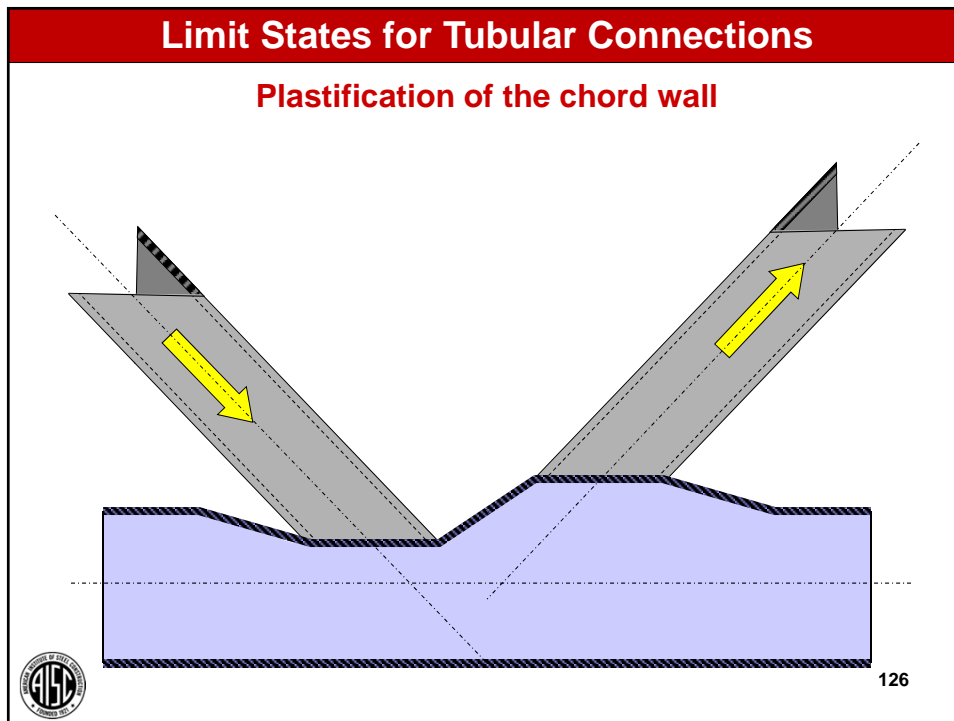
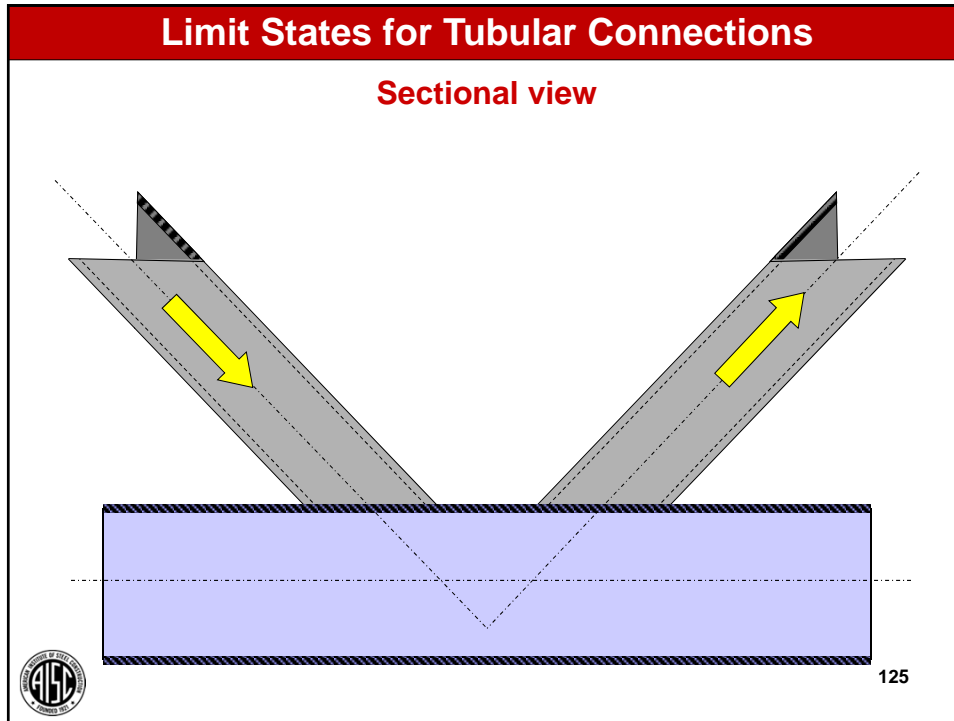
Interaction between member designer and connection designer

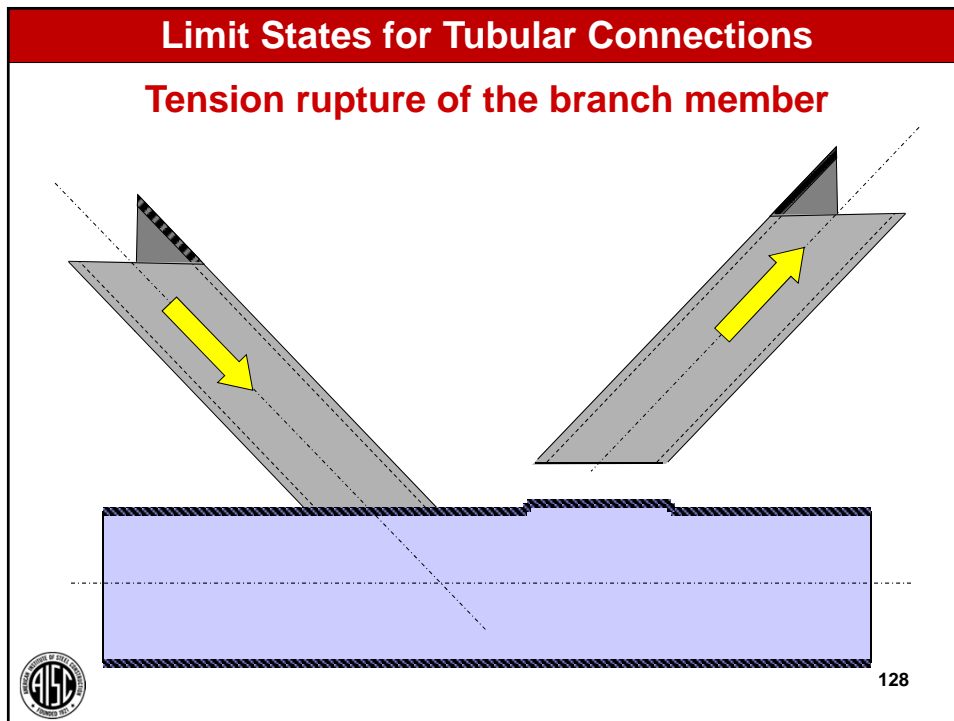
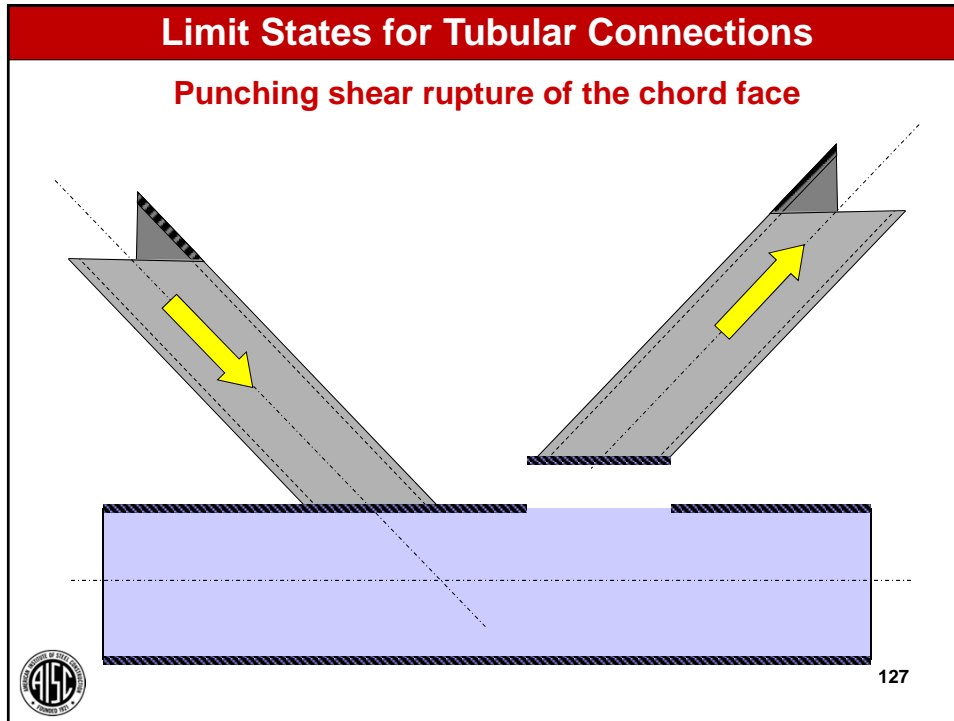


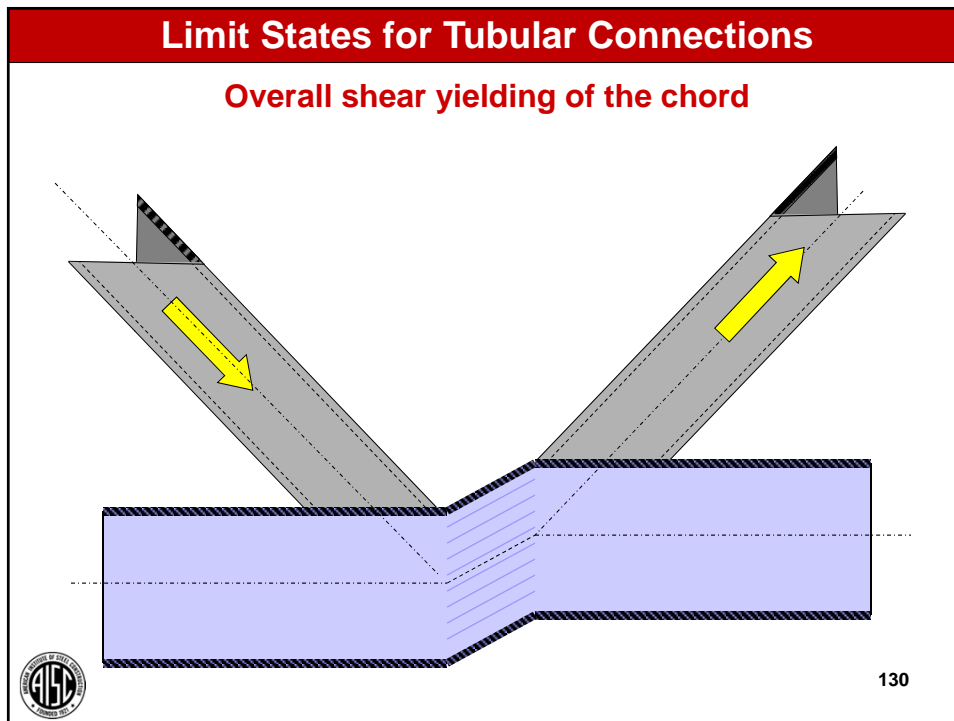
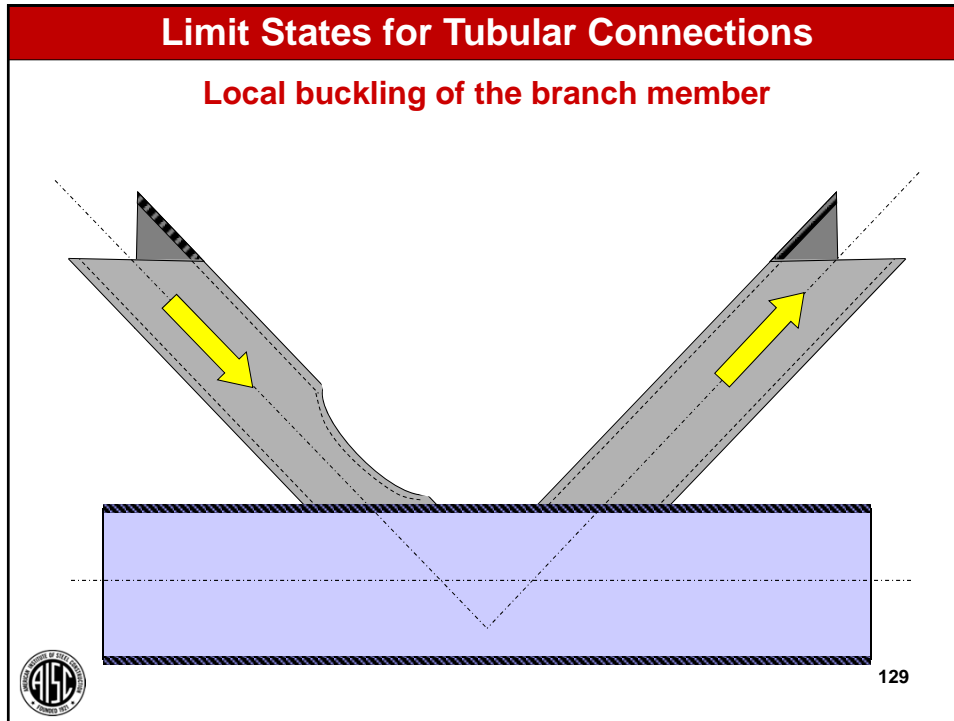
TABLE K.2.2
Available Strengths of Rectangular HSS-to-HSS Truss Connections

Connection Type	Connection Available Axial Strength
T-, Y- and Cross-Connections	<p>Limit State: Chord Wall Flattening, When $\beta \leq 0.85$</p> $P_n \leq P_n \leq F_y A_g \left[\frac{2t_1}{(1-\beta)} + \frac{4}{\sqrt{1-\beta}} \right] Q_1 \quad (K2-7)$ <p>$\phi = 1.00$ (LRFD) $\Omega = 1.50$ (ASD)</p>
	<p>Limit State: Shear Yielding (Punching), When $0.85 < \beta \leq 1 - 1/2$ or $\beta \leq 1 < 10$</p> $P_n \leq P_n \leq 0.6 F_y A_g (2t_1 + 2t_2) \quad (K2-8)$ <p>$\phi = 0.95$ (LRFD) $\Omega = 1.58$ (ASD)</p>
	<p>Limit State: Local Yielding of Chord Sidewalls, When $\beta = 1.0$</p> $P_n \leq P_n \leq 2F_y t_1 (5t_1 + t_2) \quad (K2-9)$ <p>$\phi = 1.00$ (LRFD) $\Omega = 1.50$ (ASD)</p>
Case for checking limit state of shear of chord side walls	<p>Limit State: Local Crippling of Chord Sidewalls, When $\beta = 1.0$ and Branches are in Compression, for T- or Y-Connections</p> $P_n \leq P_n \leq 1.6 F_y t_1 \left(1 + \frac{2t_2}{t_1} \right) \sqrt{E F_y} Q_1 \quad (K2-10)$ <p>$\phi = 0.75$ (LRFD) $\Omega = 2.00$ (ASD)</p>
	<p>Limit State: Local Crippling of Chord Sidewalls, When $\beta = 1.0$ and Branches are in Compression, for Cross-Connections</p> $P_n \leq P_n \leq \left(\frac{4t_1 t_2}{t_1 + t_2} \right) \sqrt{E F_y} Q_1 \quad (K2-11)$ <p>$\phi = 0.90$ (LRFD) $\Omega = 1.67$ (ASD)</p>
	<p>Limit State: Local Yielding of Branch/Branches Due to Uneven Load Distribution, When $\beta > 0.85$</p> $P_n \leq P_n \leq F_y A_g (2t_2 + 2t_{br} - 4t_1) \quad (K2-12)$ <p>$\phi = 0.95$ (LRFD) $\Omega = 1.58$ (ASD)</p>
	<p>where</p> $P_{br} = \frac{10}{\beta} \left(\frac{F_y t_2}{F_y t_1} \right) \beta \leq \beta_0 \quad (K2-13)$







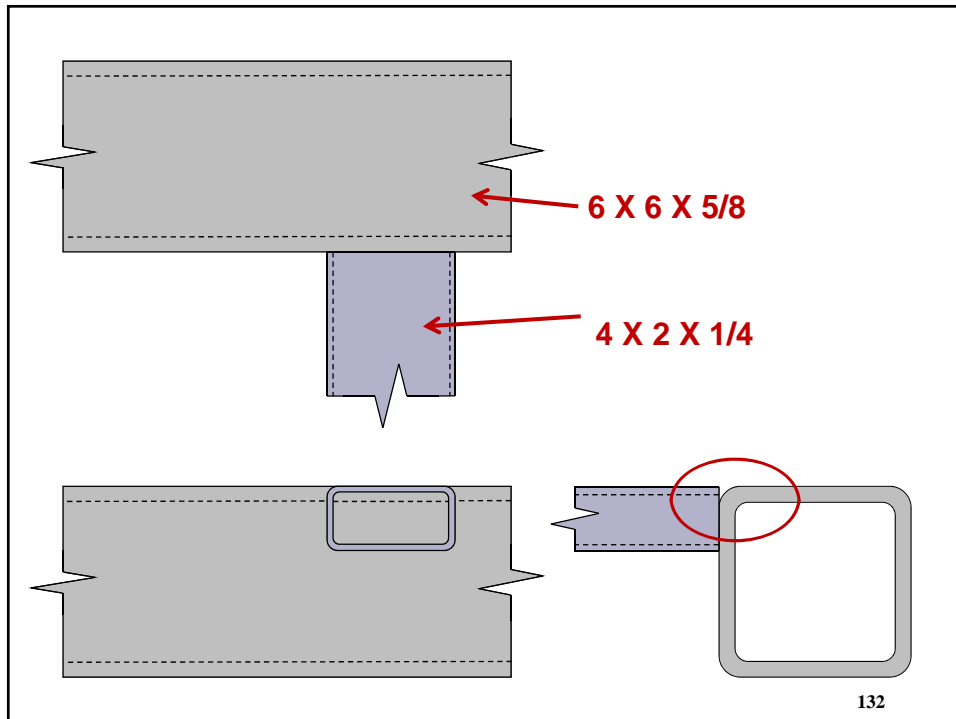


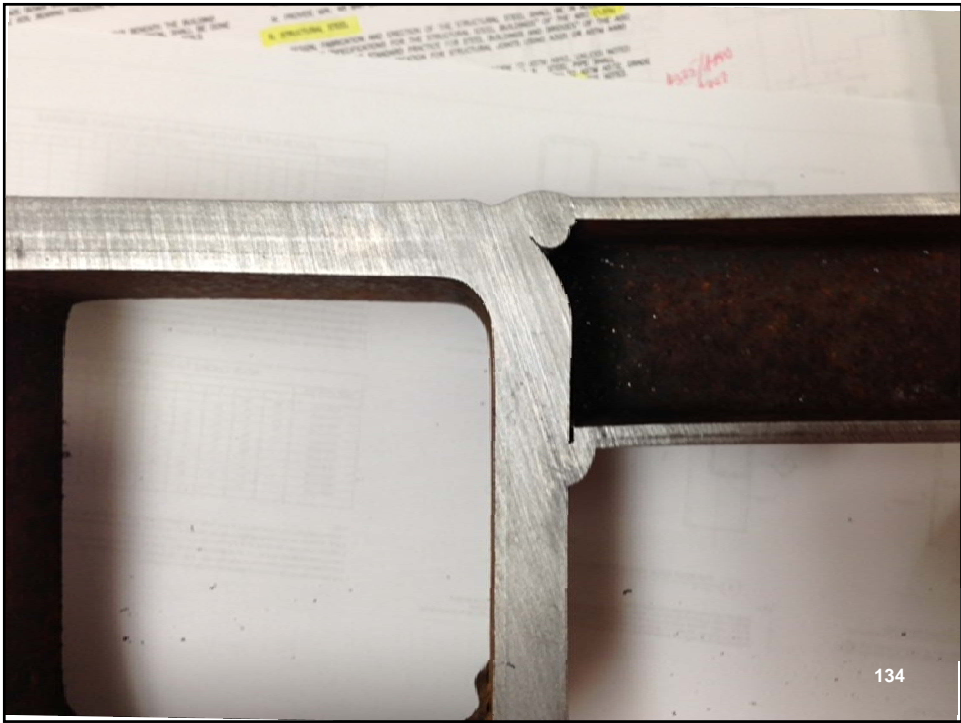
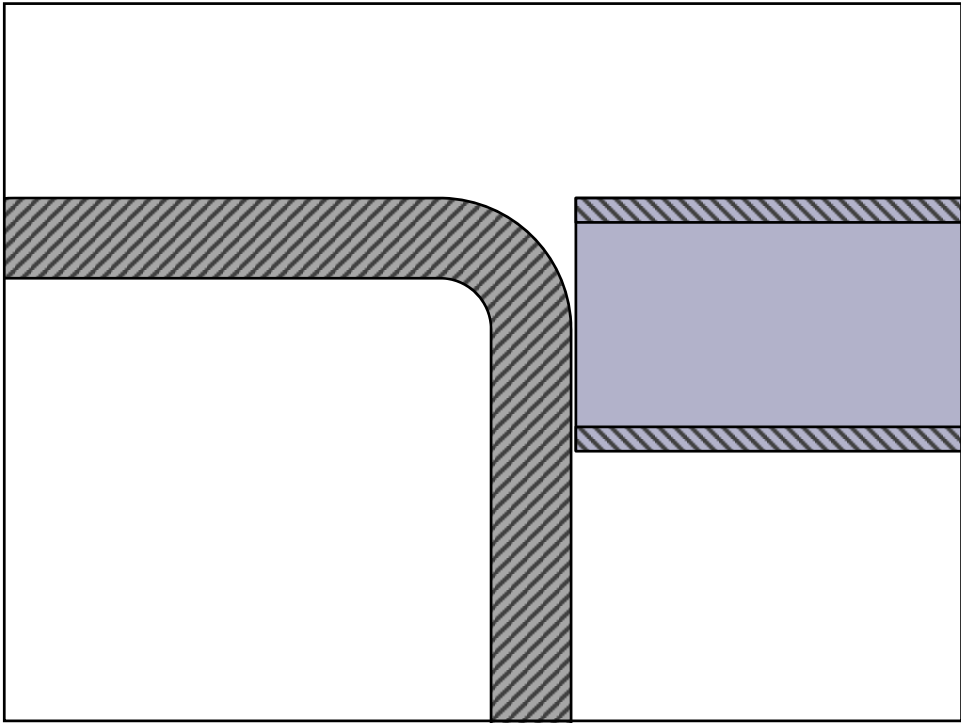
**Special Welding Applications and Field Fixes:
Welding HSS**

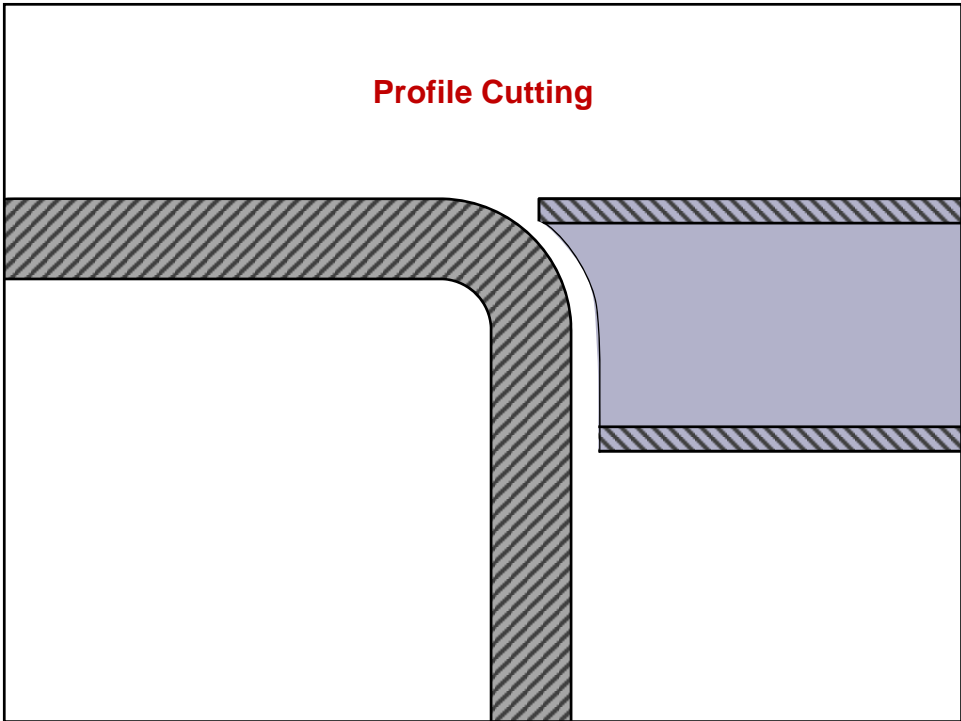
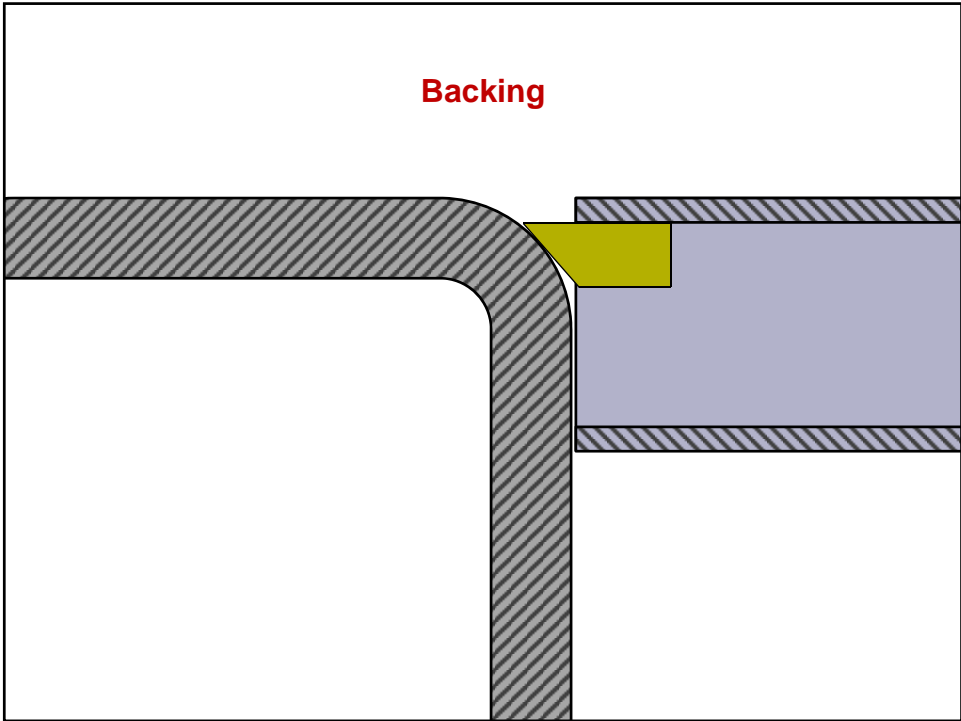
Overall Configuration

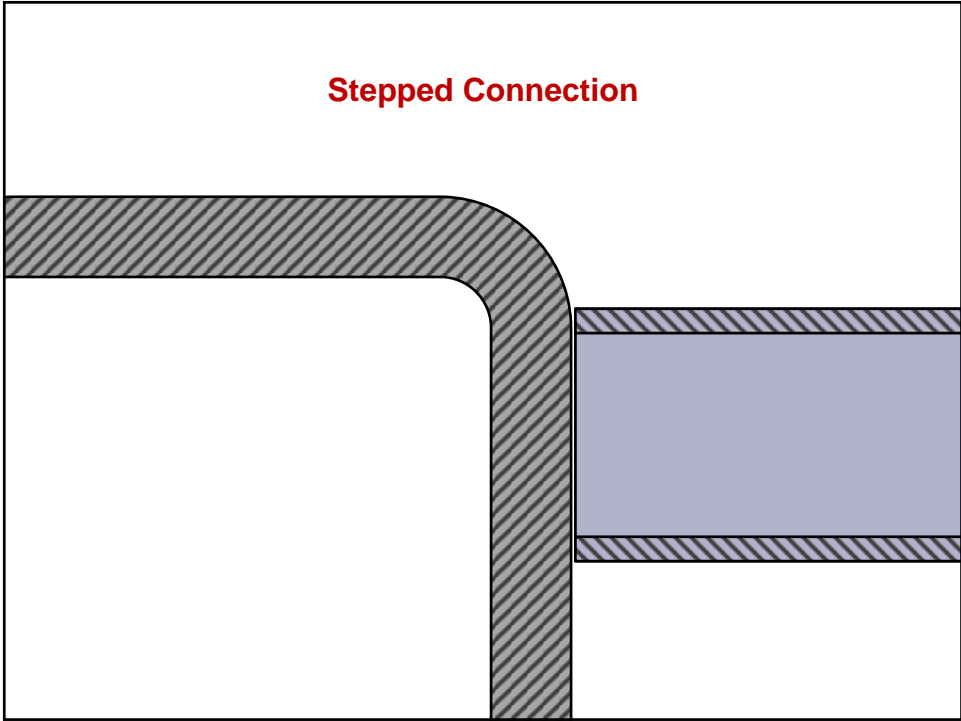
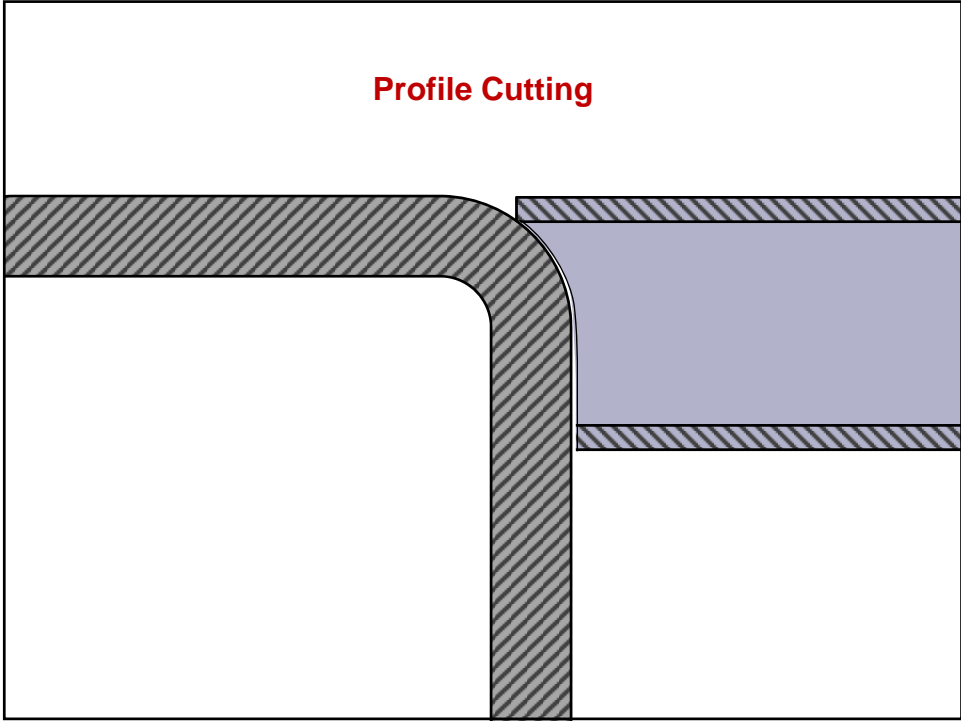


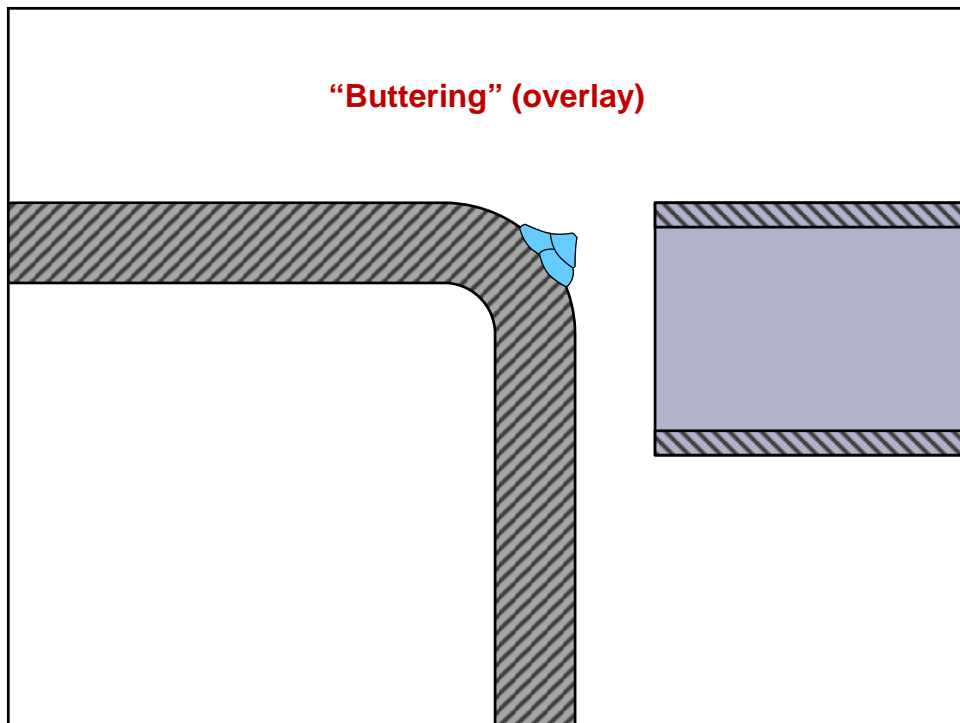
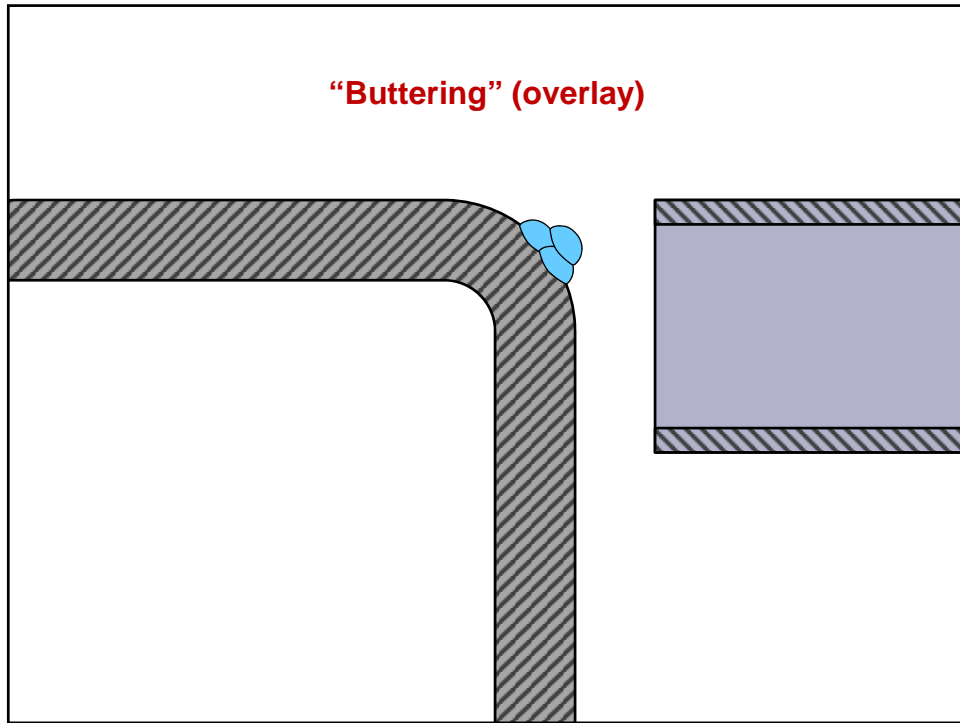
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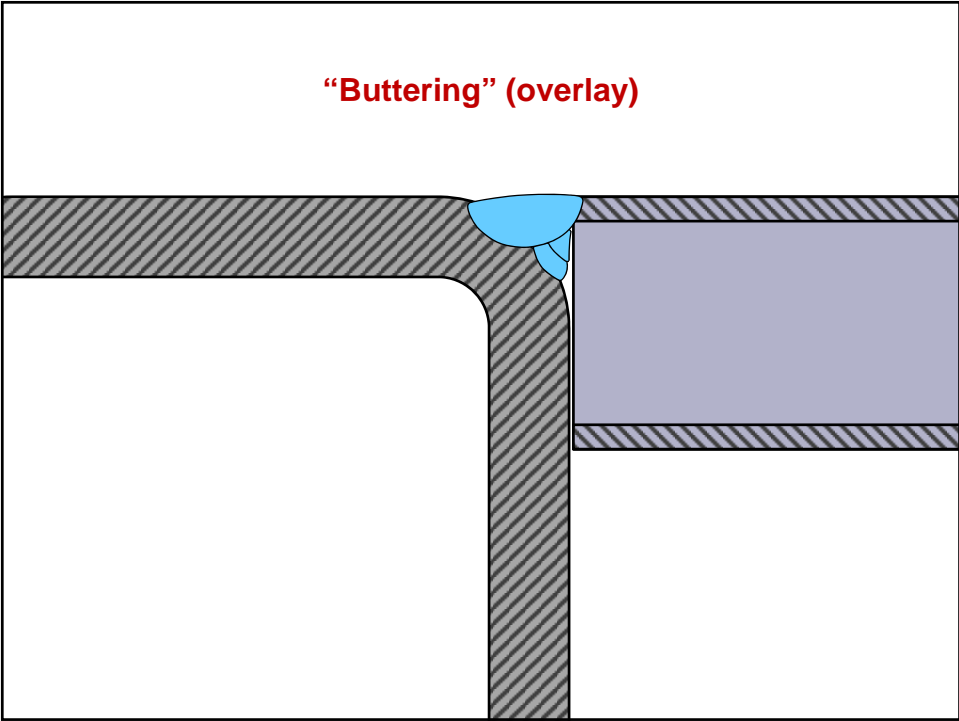
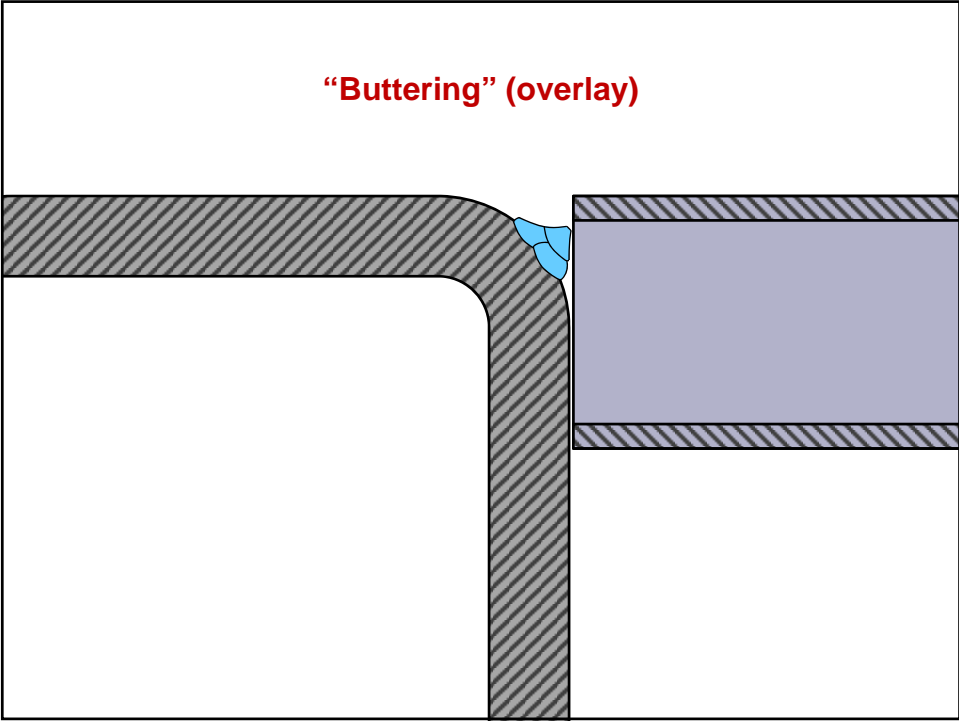


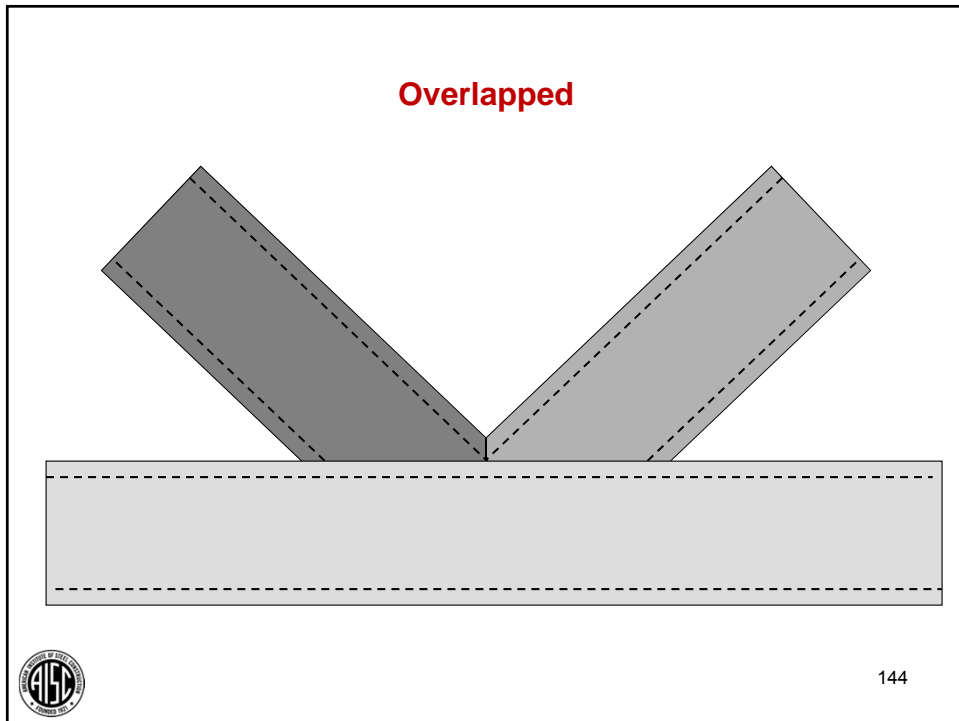


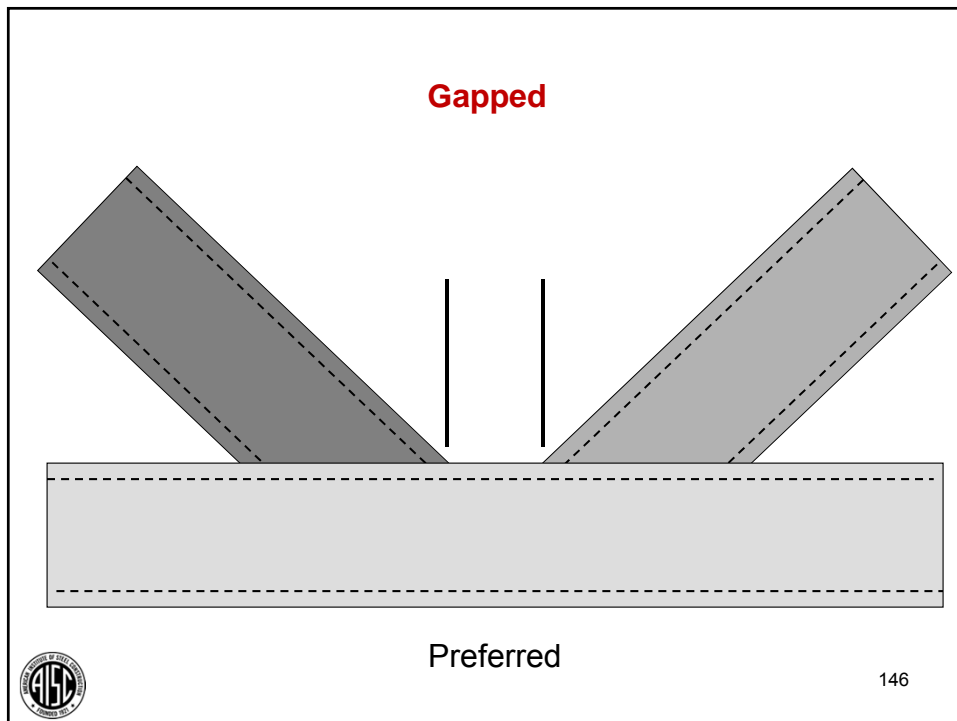
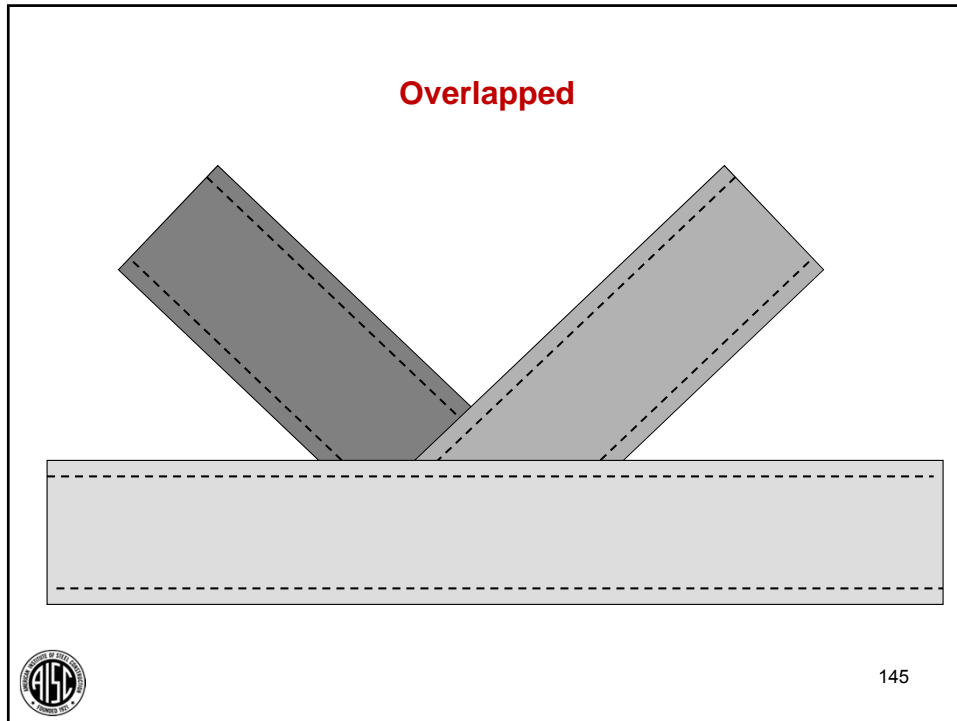


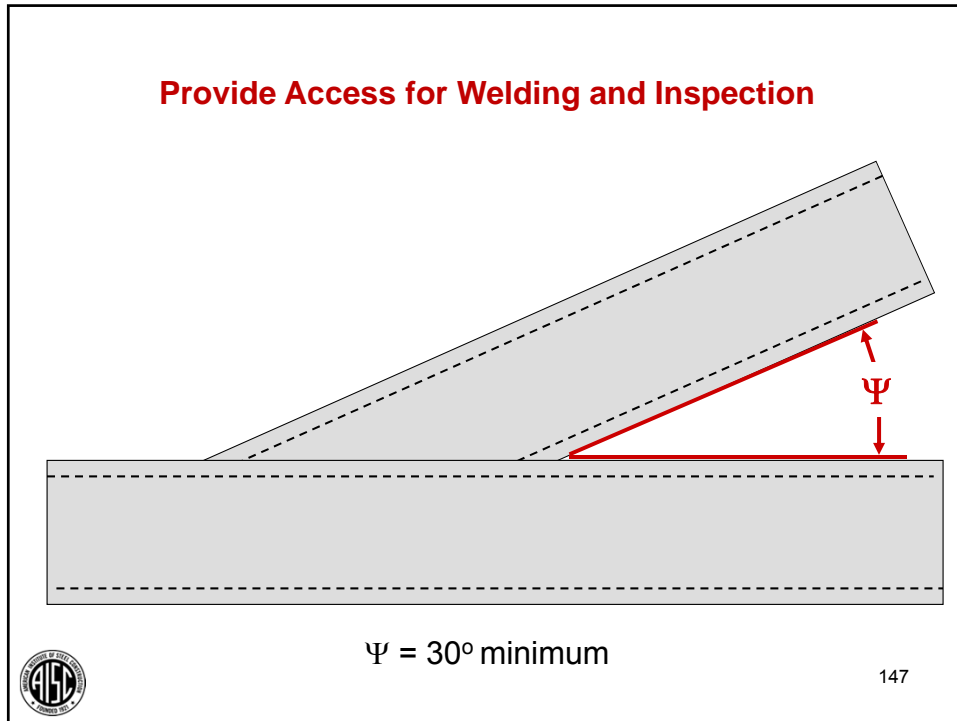











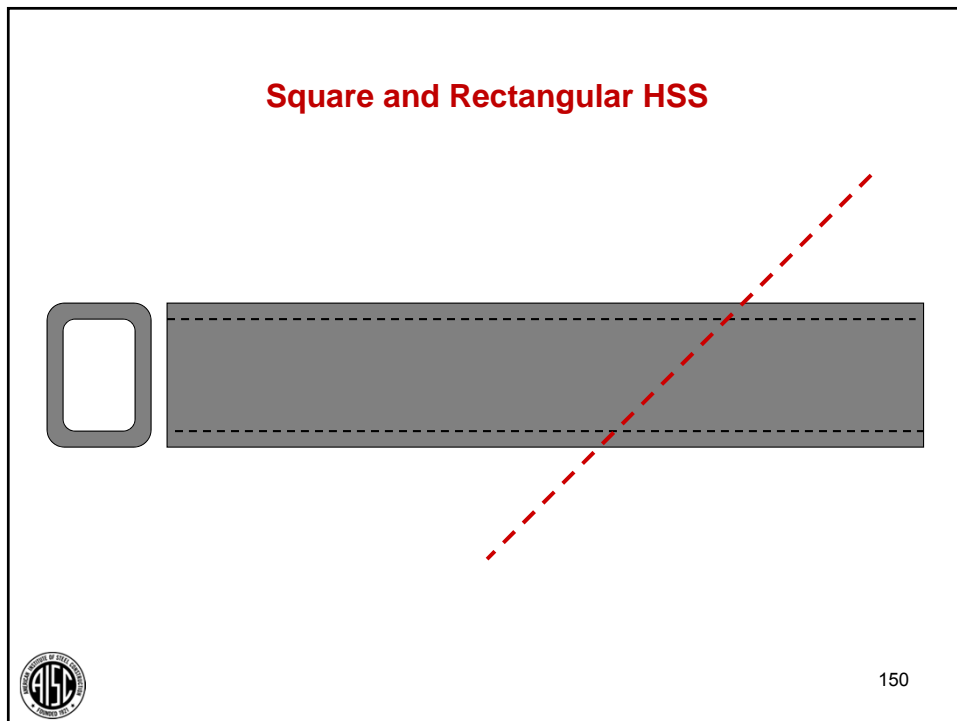
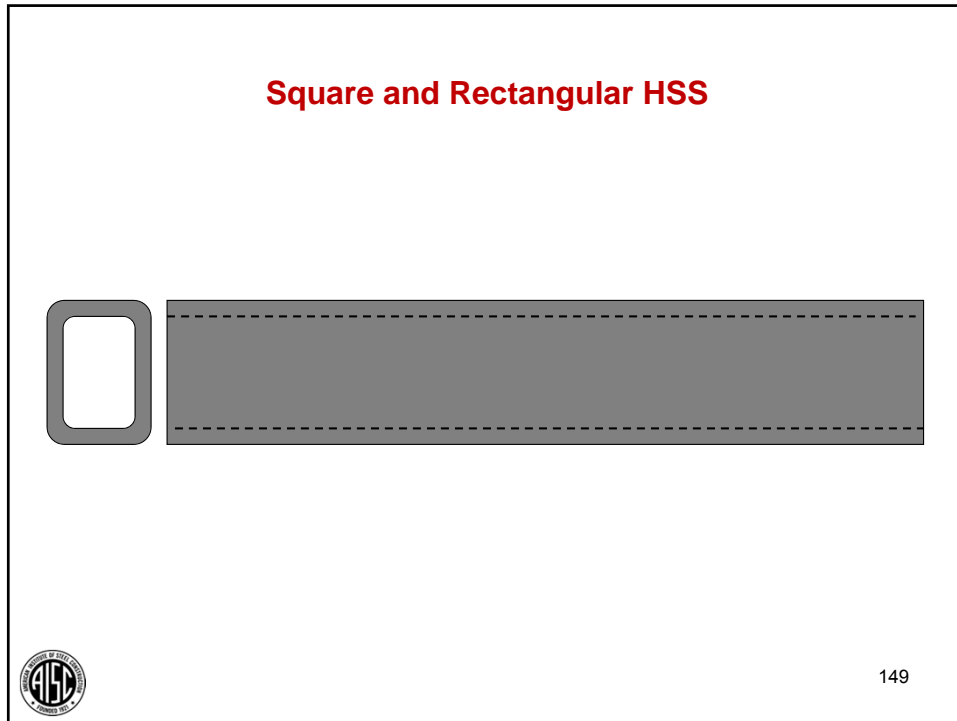


**Special Welding Applications and Field Fixes:
Welding HSS**

Cutting and Fitting



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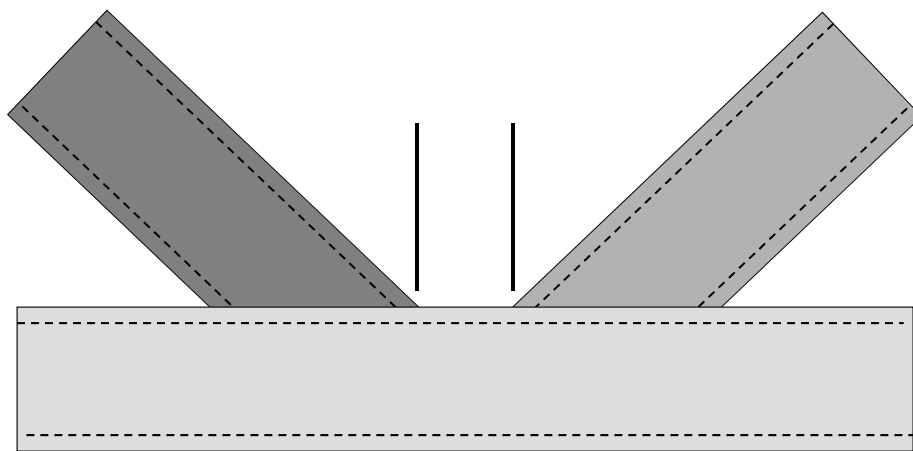


Square and Rectangular HSS



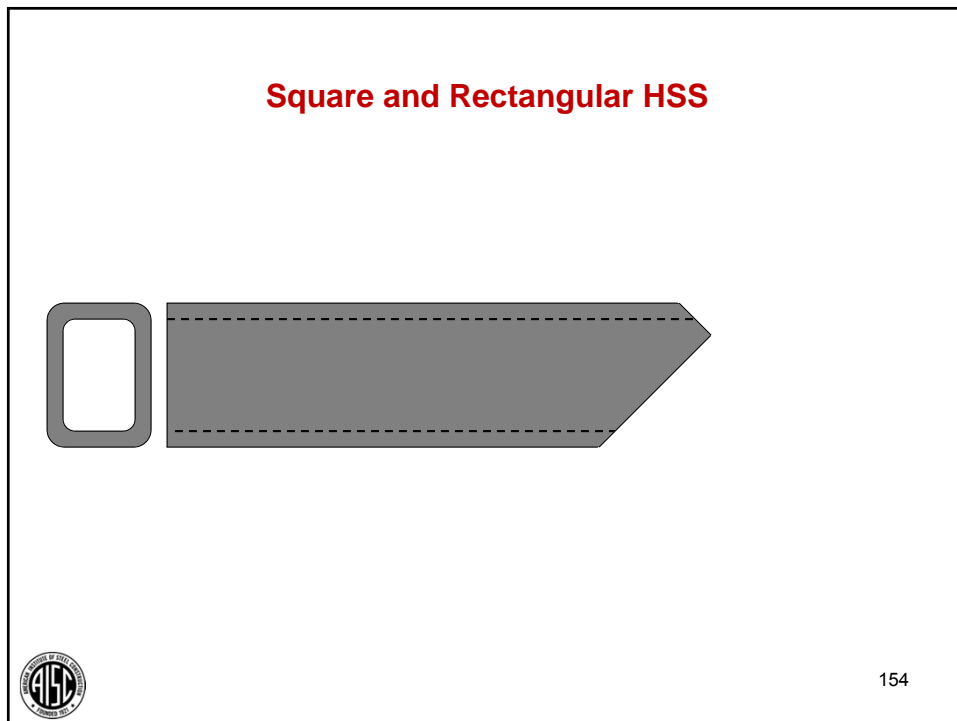
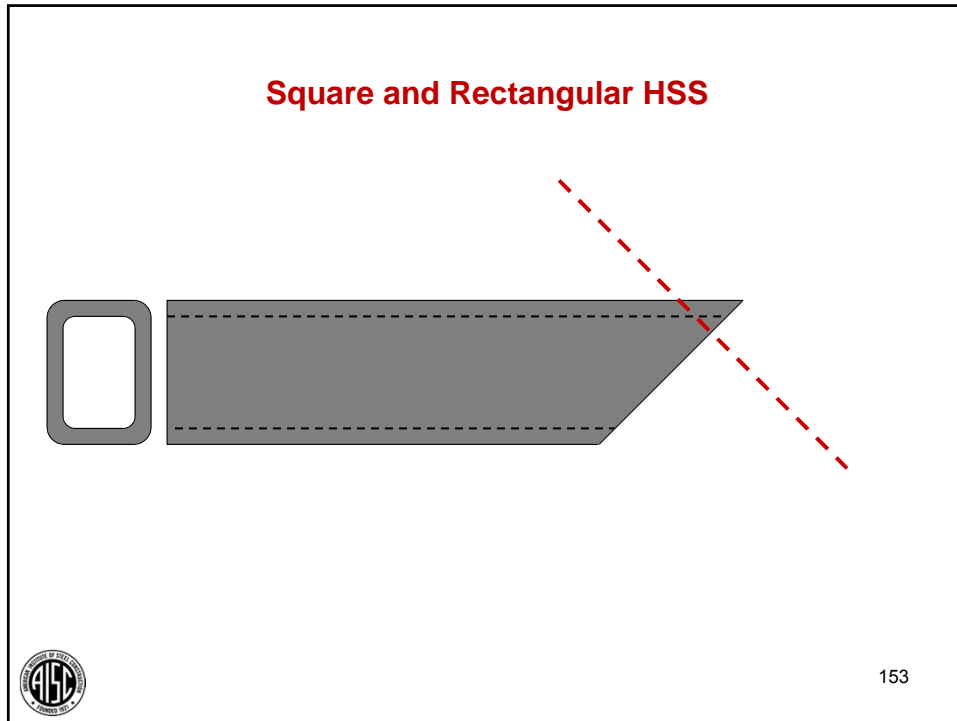
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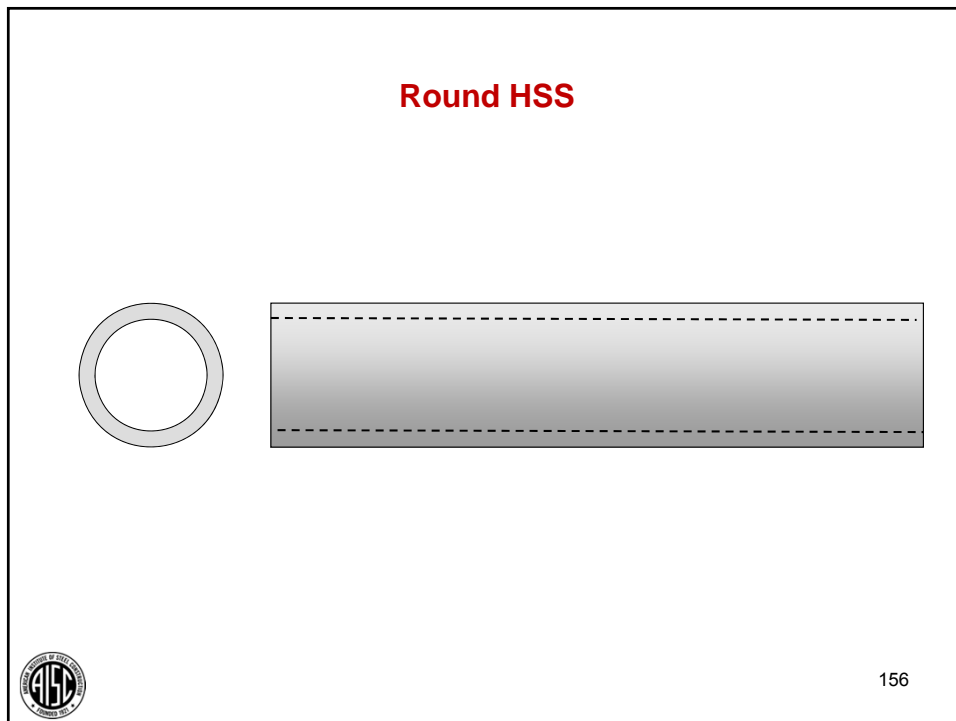
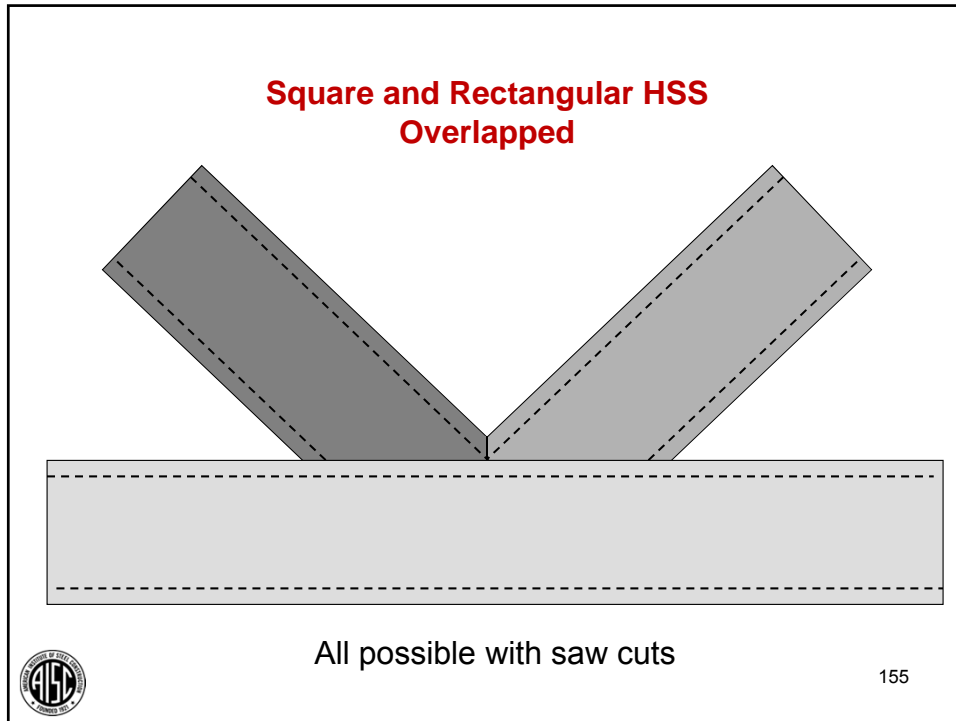
**Square and Rectangular HSS
Gapped**

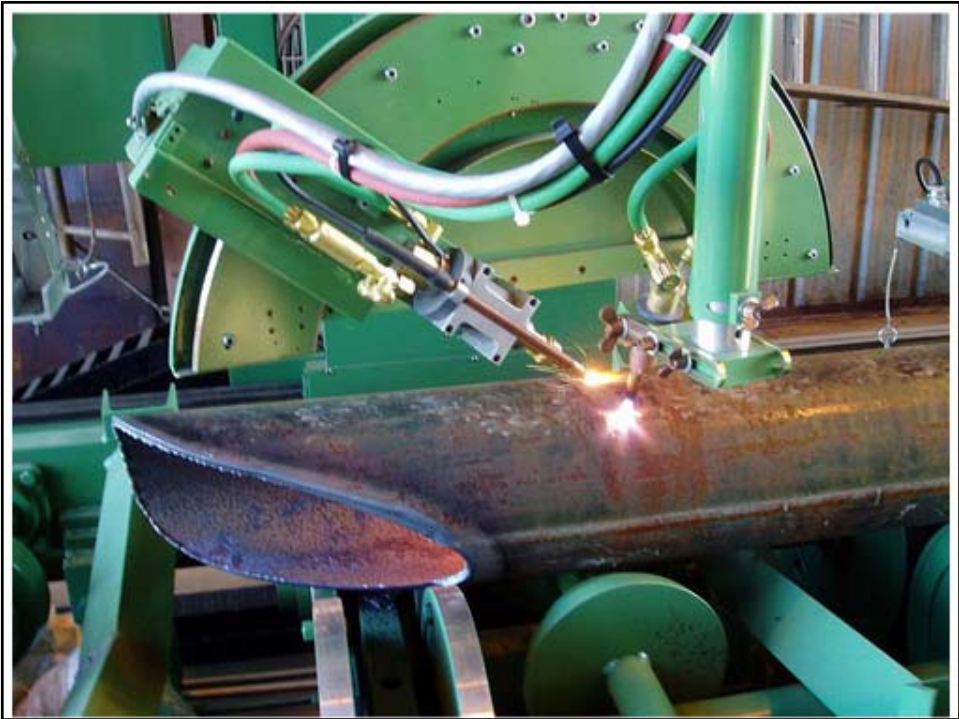
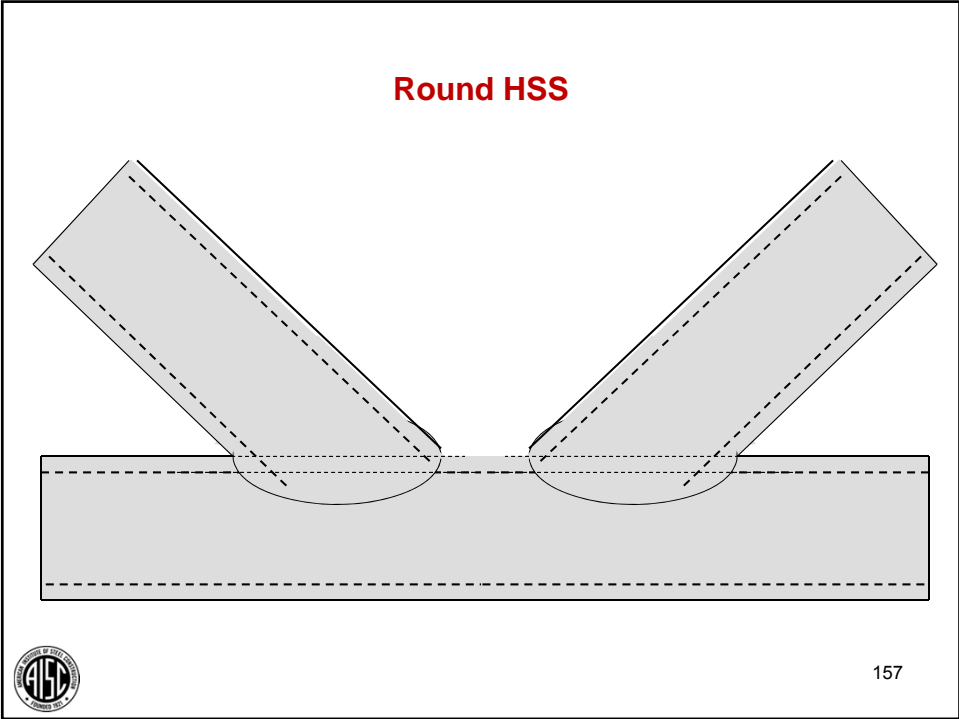


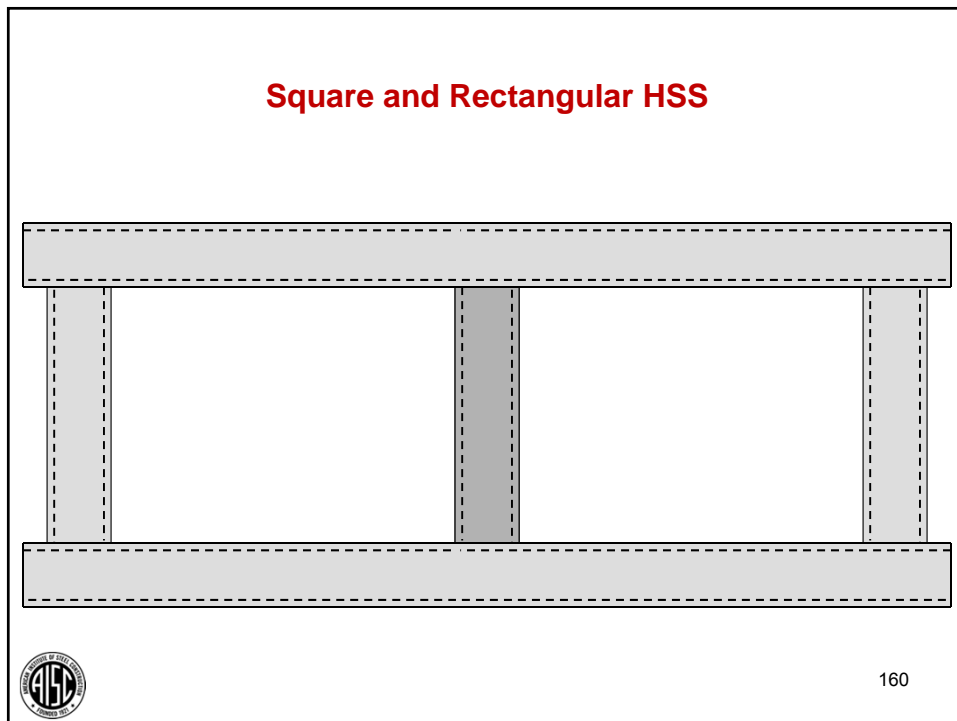
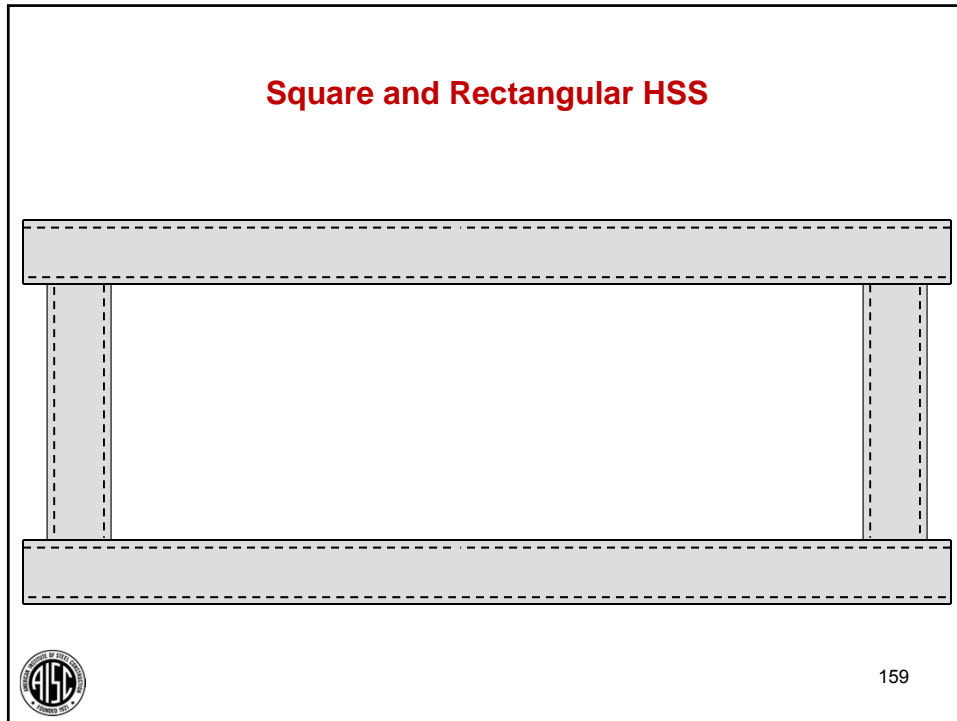
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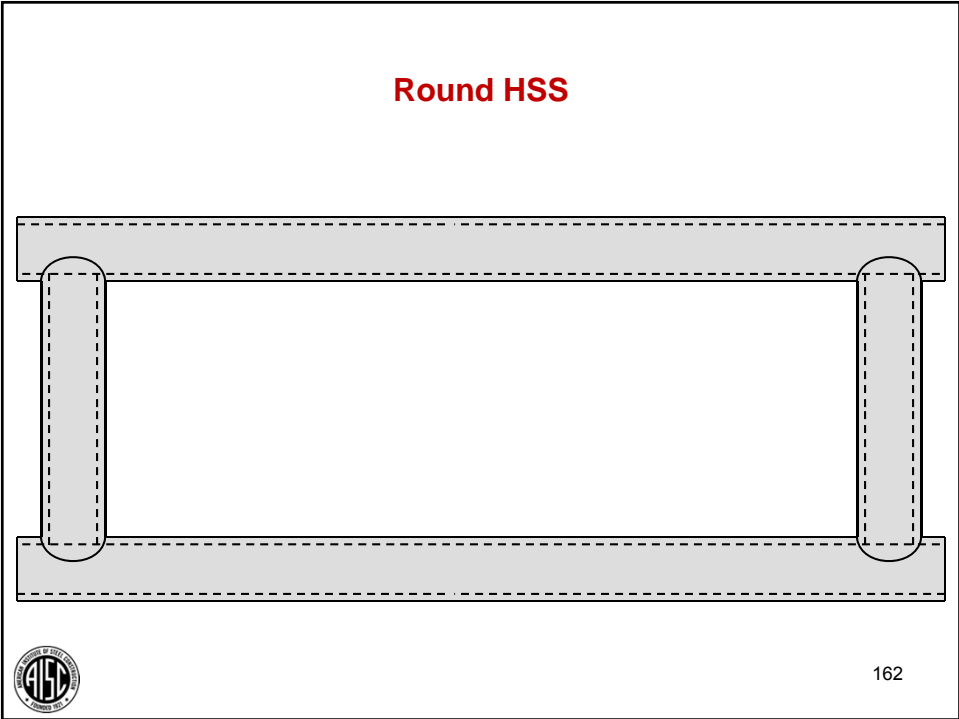
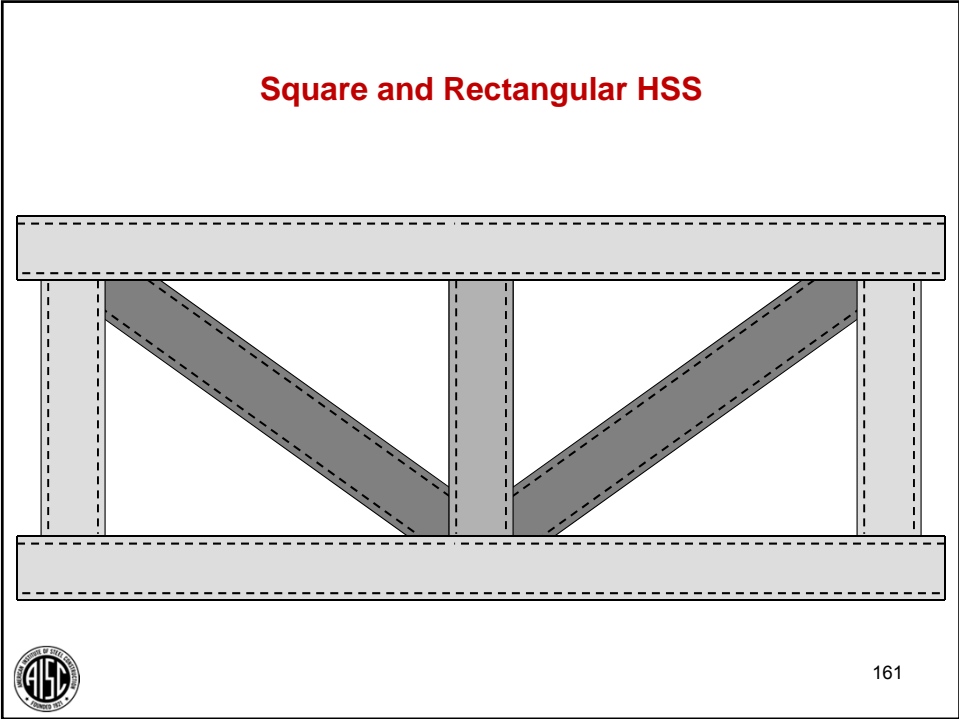


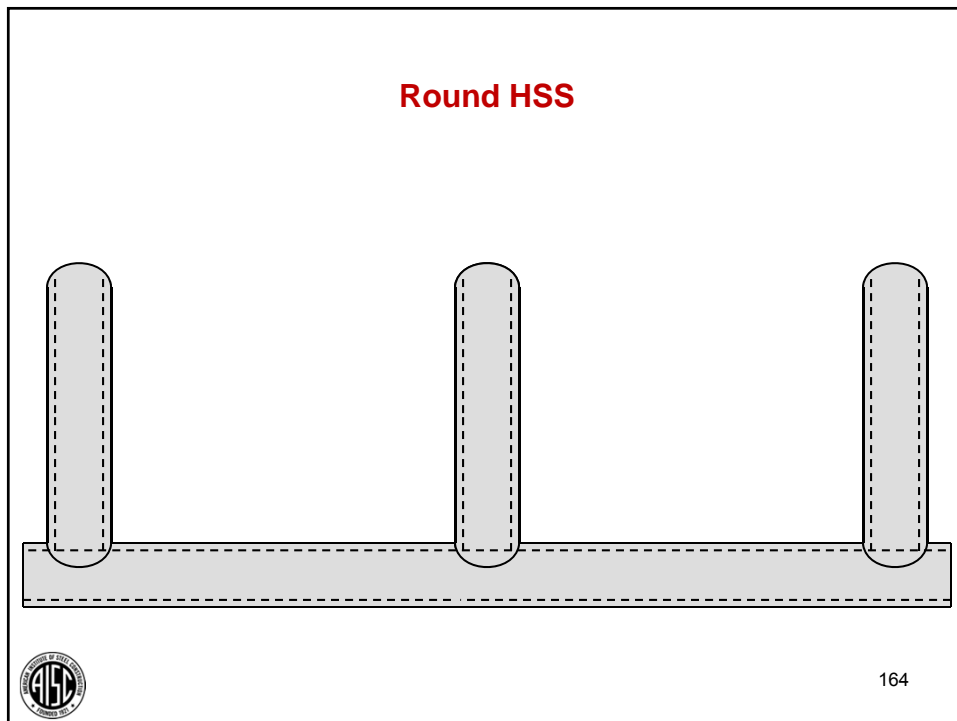
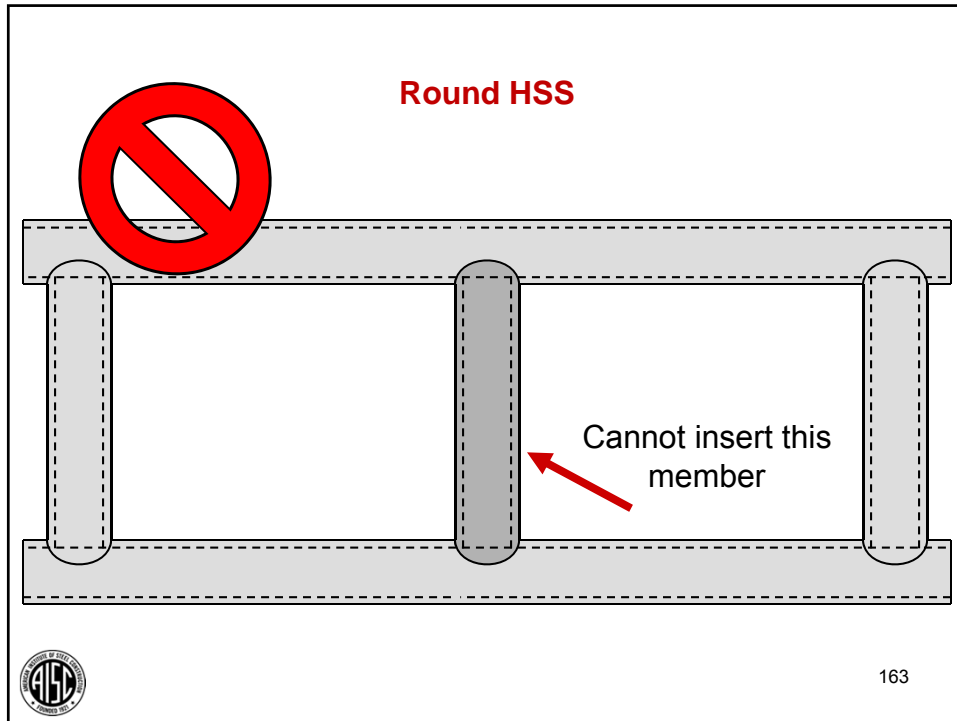


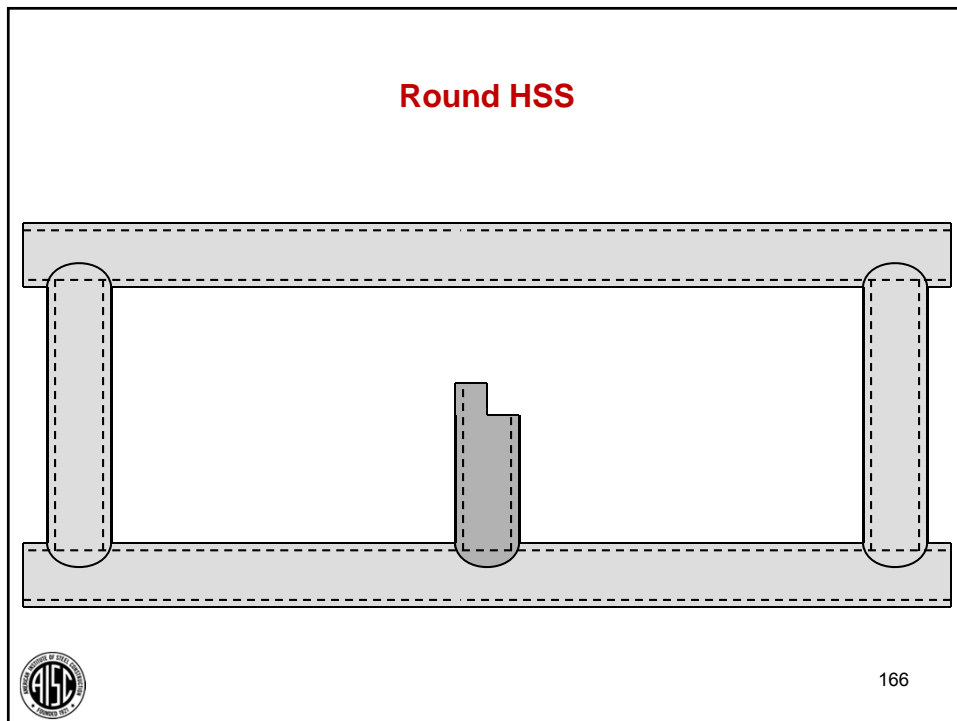
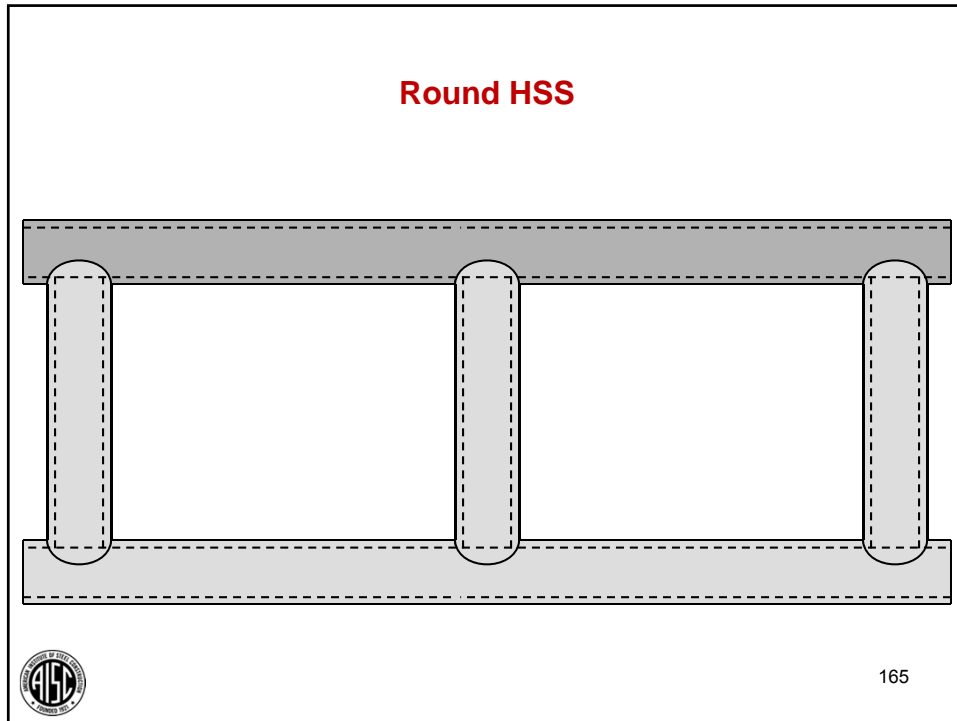


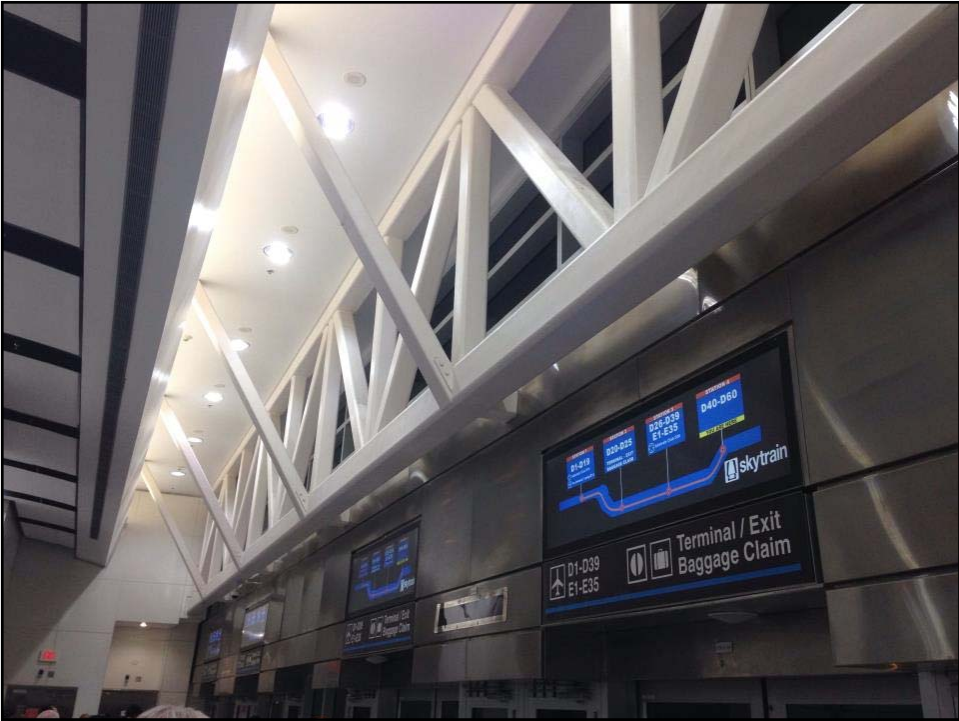
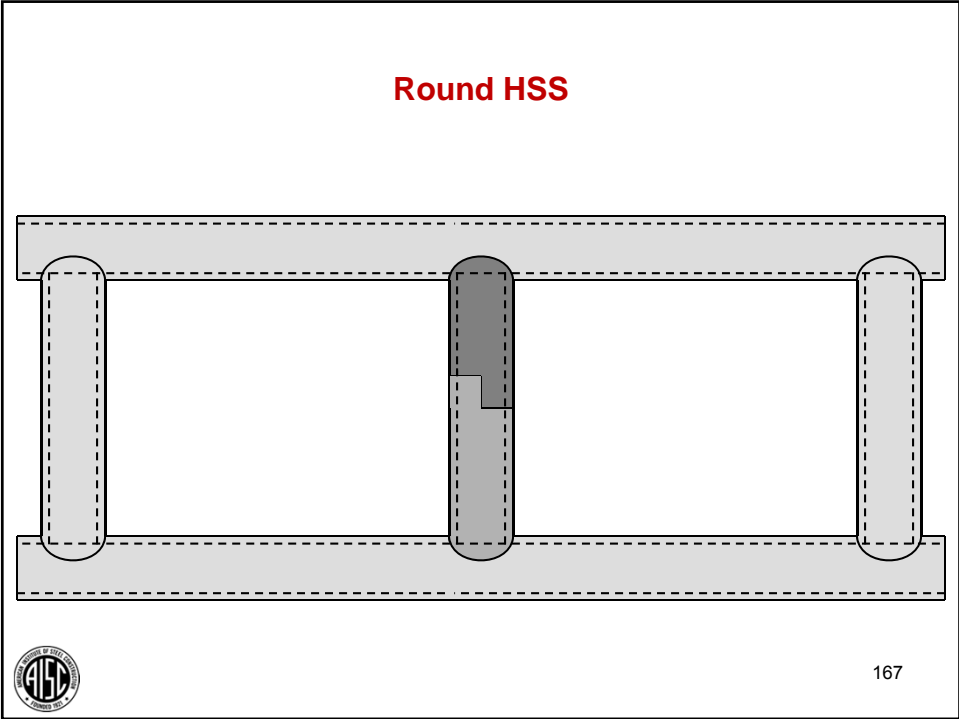


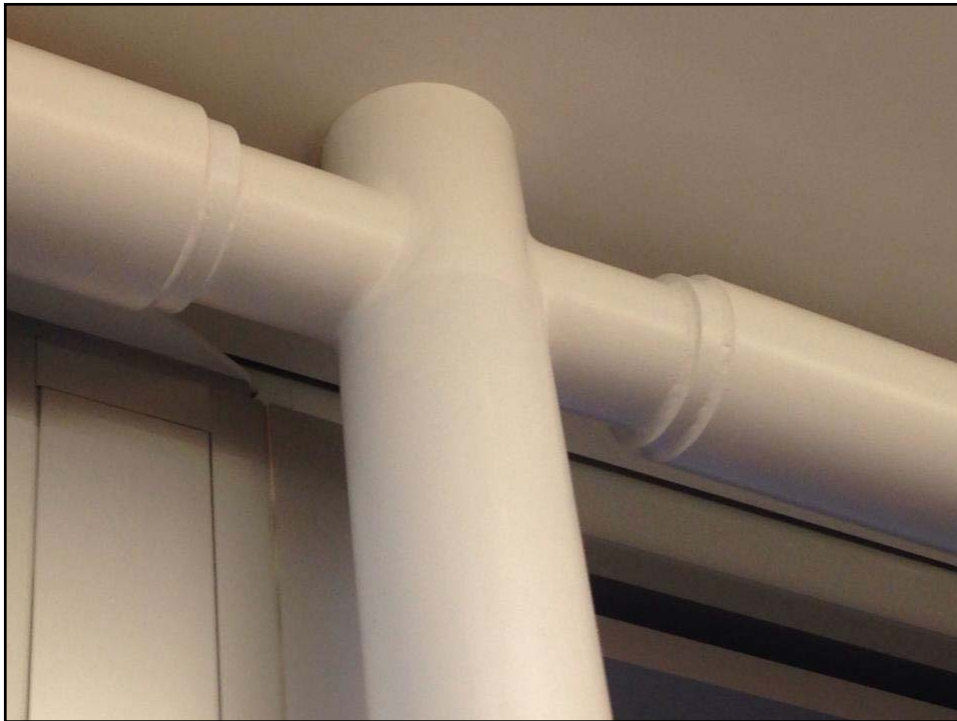


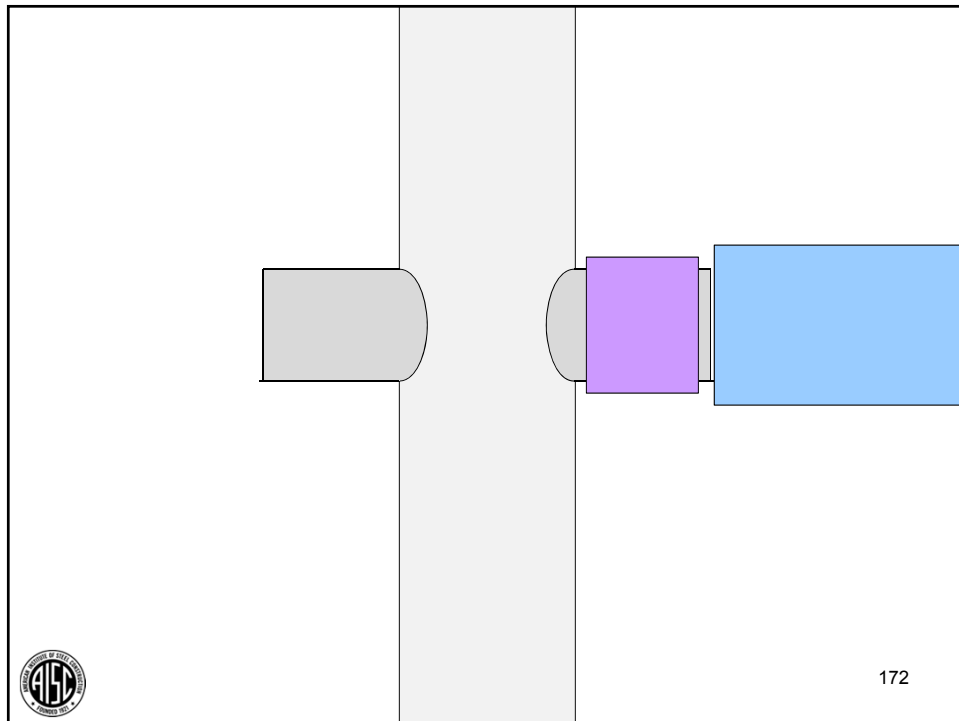
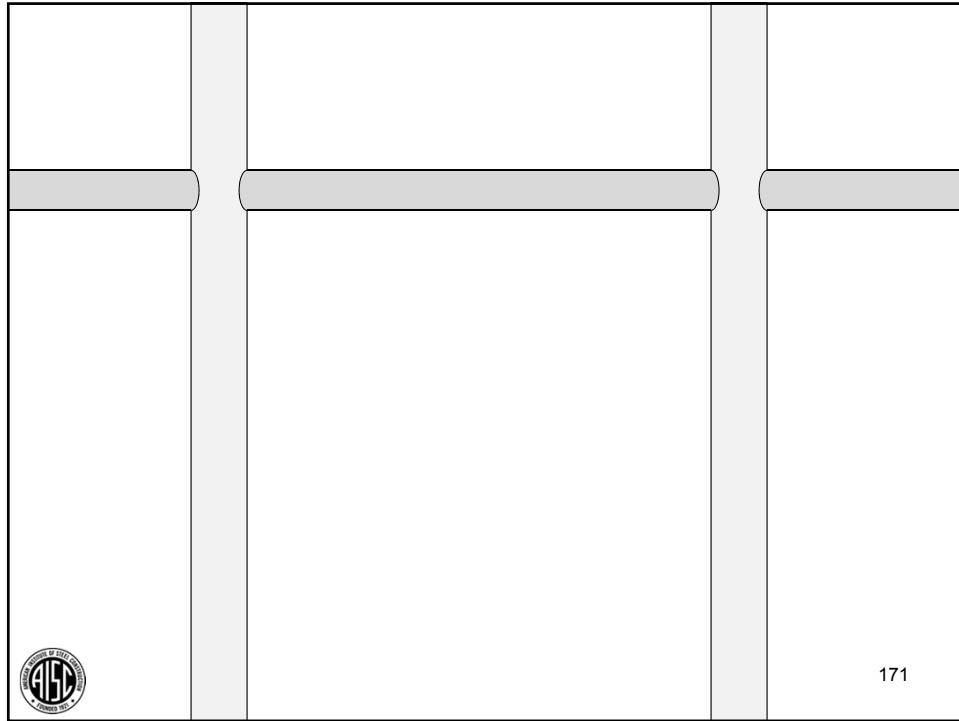


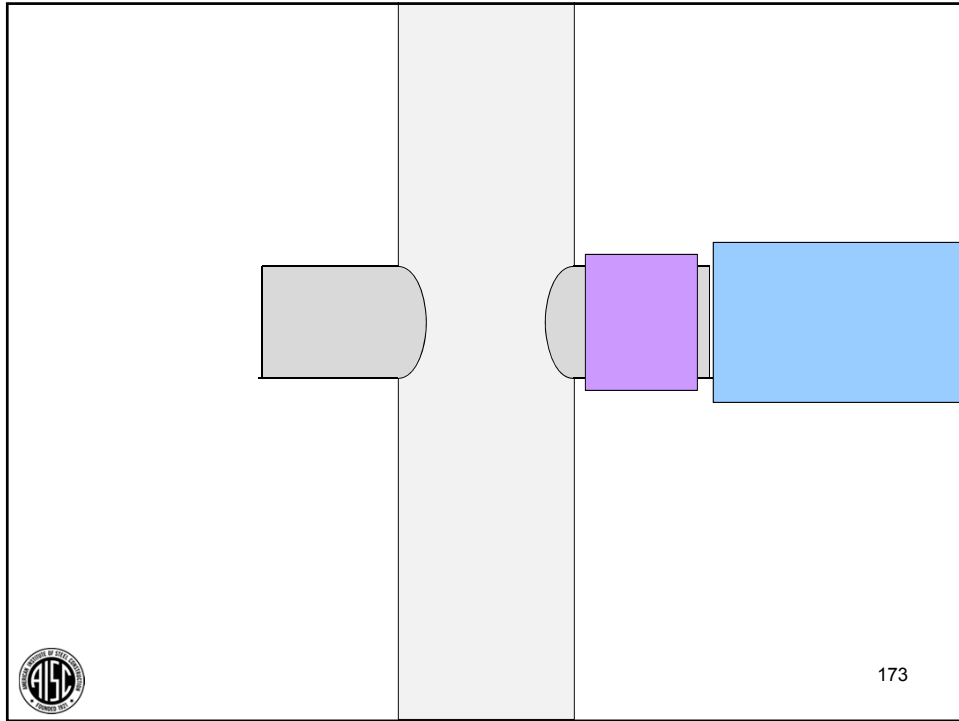


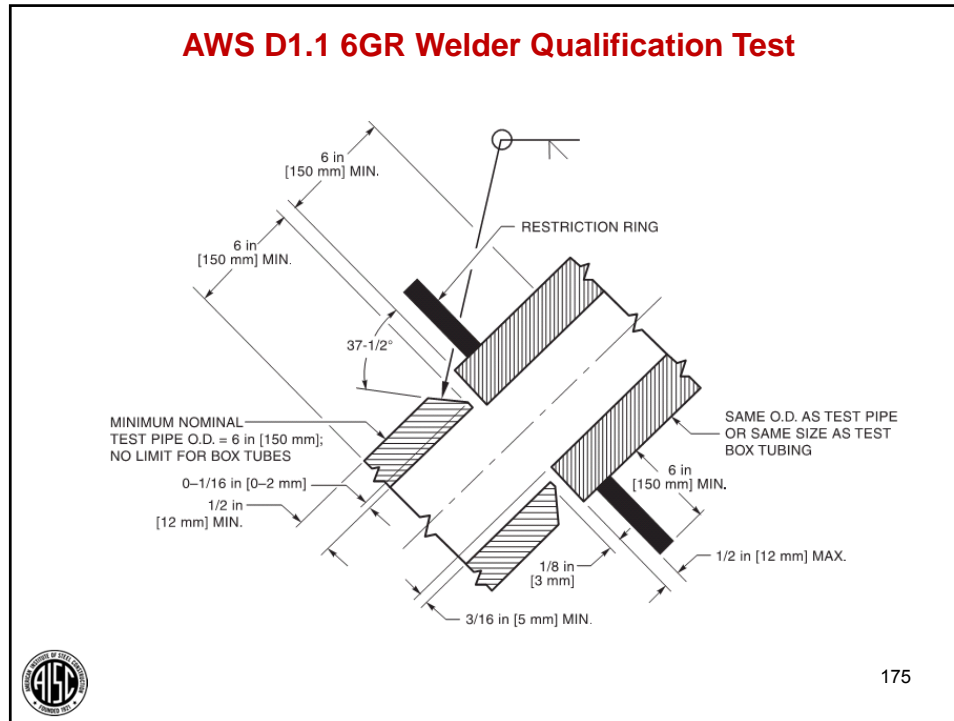







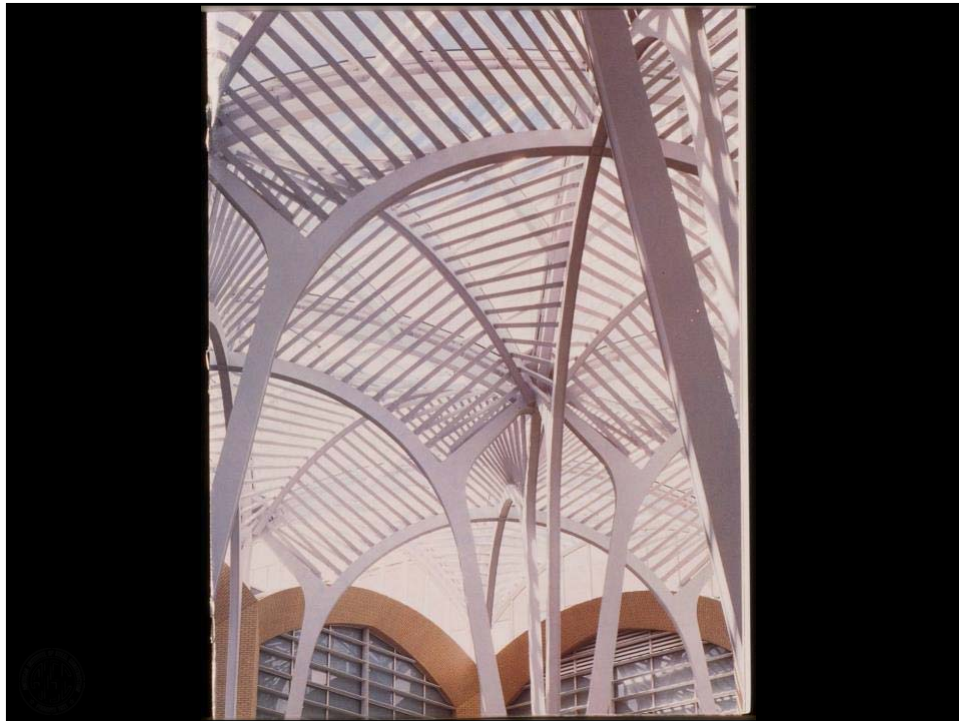






- ### Special Welding Applications and Field Fixes
- Welding on Anchor Rods
 - Welding on Heavy Sections (“Jumbo Shapes”)
 - Welding HSS
 - ➔ • Welding AESS
 - Field Welding
 - Welding on Existing Structures
 - Combining Welds and Bolts
- 
- 176







Special Welding Applications and Field Fixes Welding AESS

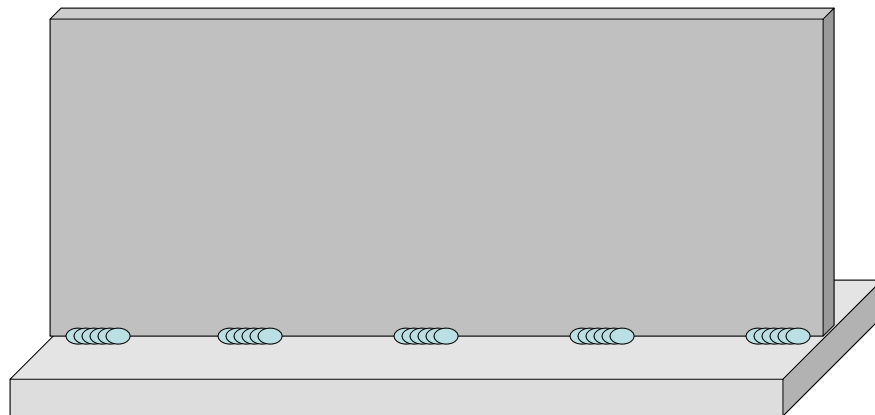
- How pretty is pretty?
- Use of mock ups (samples)
- Tolerances
- Potential code conflicts



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Special Welding Applications and Field Fixes Welding AESS

Required for strength




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Special Welding Applications and Field Fixes
Welding AESS

Required for AESS
Higher cost, more distortion



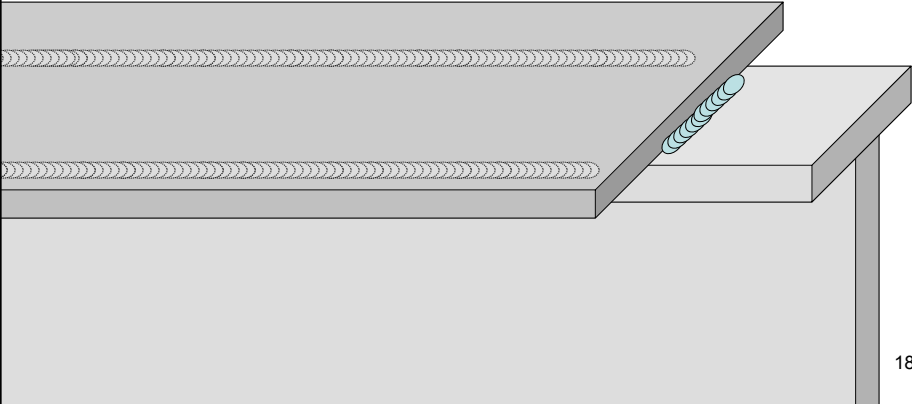
The diagram shows a 3D perspective view of a welded connection. A vertical rectangular plate is attached to a horizontal base plate. A continuous weld line runs along the bottom edge of the vertical plate, joining it to the top surface of the base plate. The weld is depicted with a series of overlapping semi-circular ripples, indicating a continuous weld bead.



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Special Welding Applications and Field Fixes
Welding AESS

Code requires interruption of welds at corners*
*Some relief in AWS D1.1:2015, and AISC 360-16

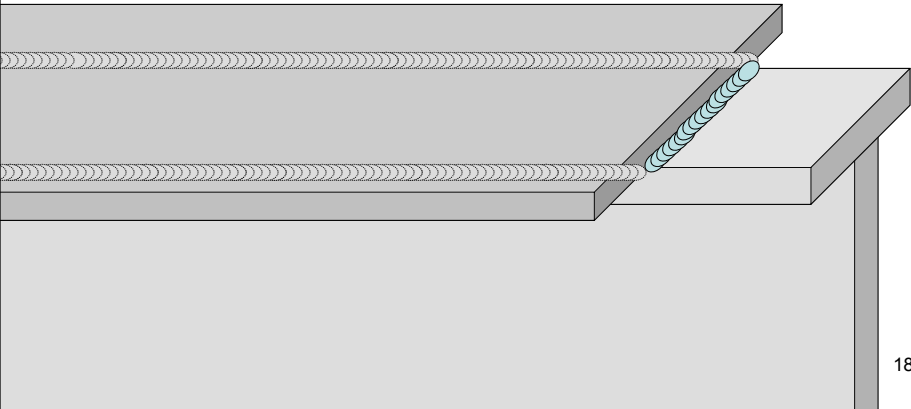


The diagram shows a 3D perspective view of a welded connection. It features a horizontal base plate and a vertical plate. The vertical plate is attached to the base plate with a weld. At the corner where the vertical plate meets the base plate, the weld is shown as a series of overlapping semi-circular ripples that stop at the corner, illustrating the requirement for interruption of welds at corners.

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Special Welding Applications and Field Fixes
Welding AESS

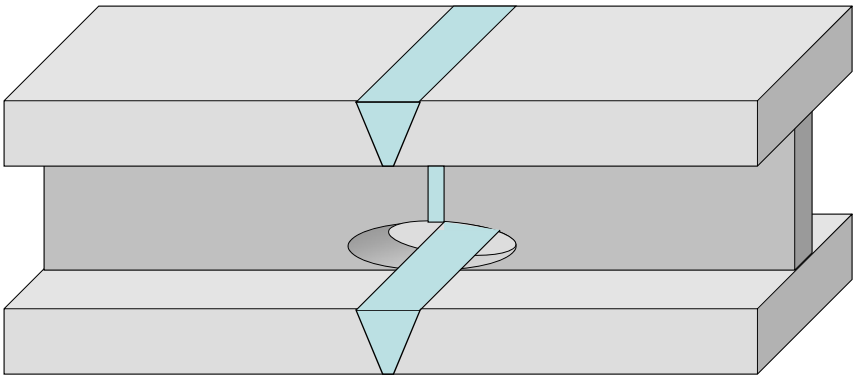
AESS may require sealed joints
Workmanship concerns, Inspection issues



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Special Welding Applications and Field Fixes
Welding AESS

Code required weld access holes



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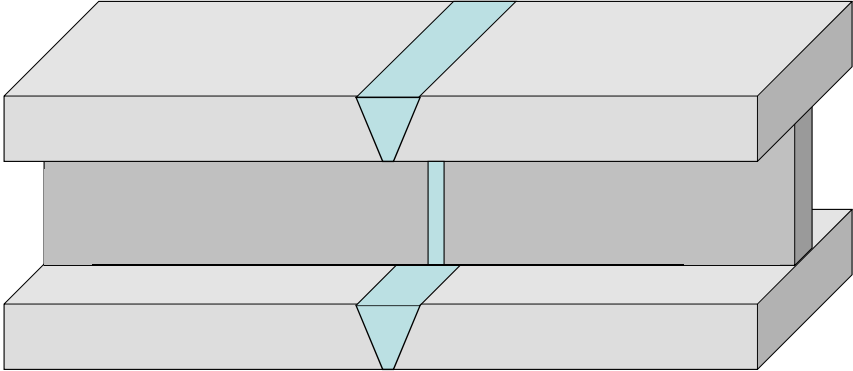


188




Special Welding Applications and Field Fixes
Welding AESS

AESS may prohibit weld access holes



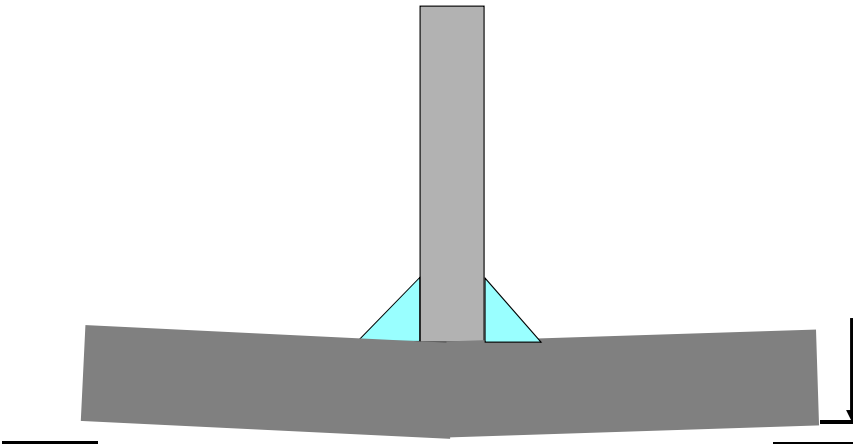
The diagram shows a 3D perspective view of an I-beam welded to a plate. Two light blue welds are shown on the top and bottom flanges. A vertical weld access hole is present in the web of the I-beam, which is highlighted in light blue. The AESS (Asymmetric Erection Sequence) text indicates that such holes may be prohibited.




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Special Welding Applications and Field Fixes
Welding AESS

AWS D1.1 acceptable distortion



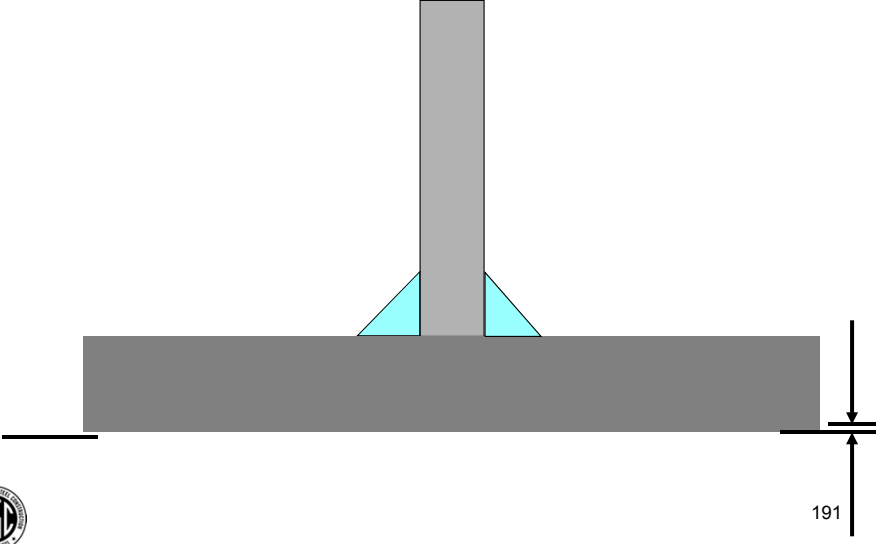
The diagram shows a T-joint where a vertical plate is welded to a horizontal plate. The horizontal plate is shown with a slight downward curvature, indicating distortion. A vertical dimension line on the right side of the horizontal plate indicates a distance of 190 units from the bottom surface to the top surface of the horizontal plate.



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Special Welding Applications and Field Fixes
Welding AESS

AESS may limit permissible distortion



The diagram illustrates a T-joint weld. A vertical grey bar is welded to a horizontal grey bar. Two cyan triangles are shown at the base of the vertical bar, representing the weld metal. A vertical double-headed arrow on the right side of the horizontal bar indicates a distance of 191 units. The AISC logo is located in the bottom left corner of the diagram area.

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http://www.cisc-icca.ca/docs/aess/ASteel31_AESS.pdf



**THE CANADIAN MATRIX:
A CATEGORY APPROACH FOR SPECIFYING AESS**

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Since the turn of the millennium, a robust frame has been the mainstay when it comes to framing machines within their small volume to the point where the steel structure becomes the architecture, or architecturally exposed structural steel (AESS).

Although architects look for the one having fun, it has created a paradigm shift in the structural construction that usually takes place in a more conventional building where the steel structure is hidden. The architect now needs direct access to the fabricator shop to verify and contract on the edges and surfaces of the exposed product, and the engineer in dealing with members means that they are the structural integrity of the frame. The focus has shifted from the steel members to the visible beams, columns and technical requirements.

The paradigm shift could not be a big deal if everyone understood it but the other way round. It is not, and that "one looking over their shoulder" or a "second look" has very different meanings whether you are looking to an architect, an engineer or a fabricator. Such a situation creates a misalignment of expectations between

what can be accomplished within a specific budget envelope. Make that one conventional and AESS are not the same as an ASTM A572 structural I-beam for example.

For these reasons, CISC formed a national Ad Hoc Committee on AESS that met and formed the Architectural Categories because not all AESS need to be treated equal. For example, a long slender, cooling tower and decorative beam should require different design. To facilitate communication, Categories and their associated characteristics are presented in a Matrix. In total, three AESS documents reference the Matrix: A, Sample Specifications, in addition to the CISC Code of Standard Practice and a Guide.

CATEGORIES AND CHARACTERISTICS OF THE MATRIX

The Committee felt that the best way needed to be established that could characterize each of the Categories, and that each Category could reference an appropriate building type or a set of steel conditions. The final goal of this reference was outlined in Standard Structural Steel (SSS) as defined in CSO 18 as it was always an established and well-understood baseline in

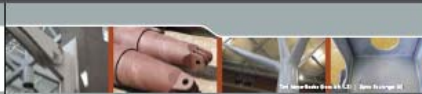


THE NEW CISC CATEGORY MATRIX FOR SPECIFYING ARCHITECTURALLY EXPOSED STRUCTURAL STEEL (AESS)

The CISC Category Matrix encompasses 8 Categories (AESS1 through AESS8). Each category represents a set of dimensions, which defines what type of steel will be required for each of the categories to meet and it is a steel grade to be used. In AESS1, the associated dimensions are 1 through 4, for AESS2, dimensions 1 through 4, and so on. The categories are subject to the architect. They are specified as follows, per AISC definition of the Structural Steel Institute (SSI) and the engineer's discretion. The categories represent an advisory and advisory, advisory and advisory documents. In general, it is required that AESS1 for reference used in a document and AESS2 for reference used in other steel specifications. For more detailed information, see www.aisc.org/aess.

TABLE 1 - AESS CATEGORY MATRIX

Category	AESS C Catenary Systems	AESS 4 Structural Beams	AESS 3 Tension Elements Members ≥ 8 Members < 8	AESS 2 Tension Elements Members ≥ 8 Members < 8	AESS 1 Rods Elements	SSS Standard Structural Steel
1) Orientation:						
11 Surface preparation to SSPC-SP 4	4	4	4	4	4	
12 Sharp edge ground smooth	4	4	4	4	4	
13 Continuous weld appearance	4	4	4	4	4	
14 Ground corner and hole	4	4	4	4	4	
15 Weld surface smooth	4	4	4	4	4	
2) Visual Quality:		material	material	material		
2.1 Visual quality	4	4	4	4		
2.2 Critical structural fabrication tolerances	4	4	4	4		
2.3 Fabrication welds not exposed	4	4	4	4		
2.4 Weld uniform and smooth	4	4	4	4		
3) Mill marks removed	4	4	4	4		
3.1 Mill marks removed	4	4	4	4		
3.2 Bar and plate mill marks smooth and filed	4	4	4	4		
3.3 HSS mill marks smoothed for reduced friction	4	4	4	4		
3.4 Cover mill marks during surface ground	4	4	4	4		
3.5 Avoid gas turbulence introduced	4	4	4	4		
3.6 All weld connections	material	material	material	material		
4) HSS beam not exposed	4	4	4	4		
4.1 HSS beam not exposed	4	4	4	4		
4.2 Make structural and AESS1	4	4	4	4		
4.3 Curves filed and smoothed	4	4	4	4		
4.4 Weld shown through structural	4	4	4	4		
C1						
C2						
C3						
C4						
C5						
Sample Use	Structure with various requirements	Structure or structure elements	Arched, slanted vertical, horizontal, diagonal	Steel and non-ferrous buildings used in a structure	Steel access for various, steel connections, systems	
General Cost Premium	Low to High (25-200%)	High (100-1500%)	Medium (50-100%)	Low to Medium (50-100%)	Low (20-40%)	None 0%



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TABLE 1 - AESS CATEGORY MATRIX

Category	AESS C Custom Elements	AESS 4 Showcase Elements	AESS 3 Feature Elements Viewed at a Distance \leq 6 m	AESS Feature Elements Viewed Distance
<i>Id</i> Characteristics				
1.1 Surface preparation to SSPC-SP 6		√	√	√
1.2 Sharp edges ground smooth		√	√	√
1.3 Continuous weld appearance		√	√	√
1.4 Standard structural bolts		√	√	√
1.5 Weld spatters removed		√	√	√
2.1 Visual Samples		optional	optional	optional
2.2 One-half standard fabrication tolerances		√	√	√
2.3 Fabrication marks not apparent		√	√	√
2.4 Welds uniform and smooth		√	√	√
3.1 Mill marks removed		√	√	
3.2 Butt and plug welds ground smooth and filled		√	√	
3.3 HSS weld seam oriented for reduced visibility		√	√	
3.4 Cross sectional abutting surface aligned		√	√	
3.5 Joint gap tolerances minimized		√	√	
3.6 All welded connections		optional	optional	
4.1 HSS seam not apparent		√		
4.2 Welds contoured and blended		√		
4.3 Surfaces filled and sanded		√		
4.4 Weld show-through minimized		√		
C.1				
C.2				



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**Special Welding Applications and Field Fixes
Welding AESS**

NEW

AISC 303-16
Code of Standard Practice



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Table 10.1. AESS Category Matrix

Category	AESS C Custom Elements	AESS 4 Showcase Elements	AESS 3 Feature Elements in close view	AESS 2 Feature Elements not in close view	AESS 1 Basic Elements	SSS Standard Structural Steel
<i>Id</i>						
<i>Characteristics</i>						
1.1 Surface preparation to SSPC-SP 6		✓	✓	✓	✓	
1.2 Sharp edges ground smooth		✓	✓	✓	✓	
1.3 Continuous weld appearance		✓	✓	✓	✓	
1.4 Standard structural bolts		✓	✓	✓	✓	
1.5 Weld spatters removed		✓	✓	✓	✓	
2.1 Visual Samples		optional	optional	optional		
2.2 One-half standard fabrication tolerances		✓	✓	✓		
2.3 Fabrication marks not apparent		✓	✓	✓		
2.4 Welds uniform and smooth		✓	✓	✓		
3.1 Mill marks removed		✓	✓			
3.2 Butt and plug welds ground smooth and filled		✓	✓			
3.3 HSS weld seam oriented for reduced visibility		✓	✓			
3.4 Cross sectional abutting surface aligned		✓	✓			
3.5 Joint gap tolerances minimized		✓	✓			
3.6 All welded connections		optional	optional			
4.1 HSS seam not apparent		✓				
4.2 Welds contoured and blended		✓				
4.3 Surfaces filled and sanded		✓				
4.4 Weld show-through minimized		✓				
C.1						
C.2						
C.3						
C.4						
C.5						
<i>Sample Use:</i>	Elements with special requirements to be defined in	Showcase or dominant elements	Airports, shopping centers, hospitals, lobbies	Retail and architectural buildings viewed at a distance	Roof trusses for arenas, retail warehouses, canopies	
<i>Estimated Cost Premium:</i>	Low to High (20-250%)	High (100-250%)	Moderate (60-150%)	Low to Moderate (40-100%)	Low (20-60%)	None 0%

Special Welding Applications and Field Fixes

- Welding on Anchor Rods
- Welding on Heavy Sections (“Jumbo Shapes”)
- Welding HSS
- Welding AESS
- ➔ • Field Welding
- Welding on Existing Structures
- Combining Welds and Bolts



Special Welding Applications and Field Fixes Field Welding

- Shop versus field welding: primarily an issue of cost.
- Some environmental issues (wind, rain, cold)
- Out-of-position welding
- Primary issue: managerial



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Special Welding Applications and Field Fixes Field Welding

Myths

- Can't get quality welds out-of-position
- Can't get quality in the field
- No codes govern field work
- Field welders aren't "certified" (i.e., qualified)
- There is no QC inspection in the field
- There is no audit program for field erectors



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Special Welding Applications and Field Fixes

- Welding on Anchor Rods
- Welding on Heavy Sections (“Jumbo Shapes”)
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- Welding AESS
- Field Welding
- ➔ • Welding on Existing Structures
- Combining Welds and Bolts



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Special Welding Applications and Field Fixes Welding on Existing Structures

- ➔ • Historic steels
- Welding on members under load
- Fire
- Cold worked steel/strain aged steel
- Comprehensive plans

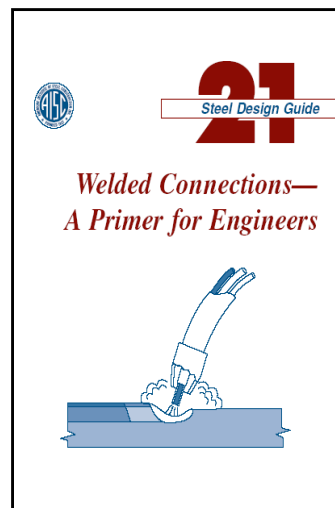


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Chapter 4 Metallurgical Issues

Historic (Obsolete) Steels

- ASTM A9
- ASTM A7
- ASTM A373
- ASTM A242



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Special Welding Applications and Field Fixes Welding on Existing Structures

Historic steels

- Check weldability, especially for riveted structures
- Rule of thumb (not 100% reliable):
If steel was produced after WWII, steel will likely have acceptable weldability
- Weldability of steel does not decrease with time
- Steel does corrode with time



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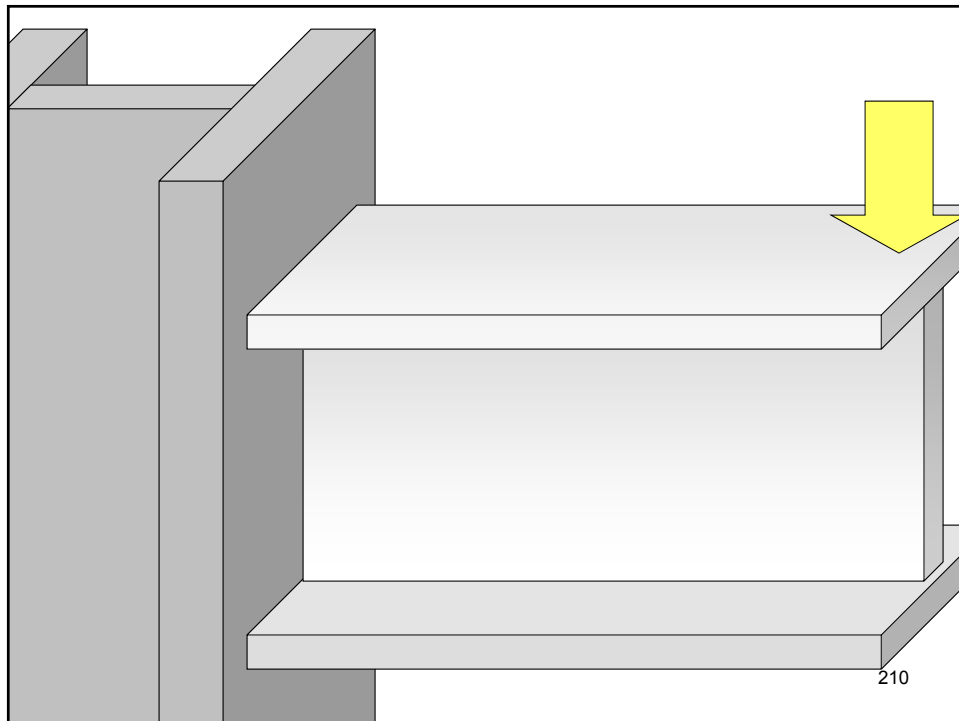
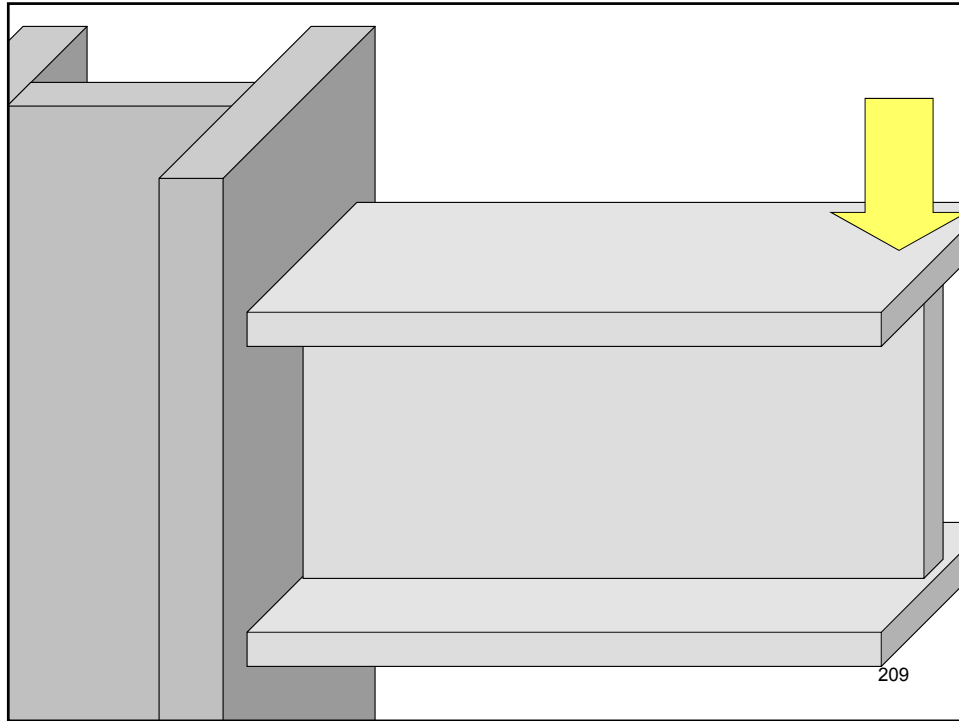
Special Welding Applications and Field Fixes Welding on Existing Structures

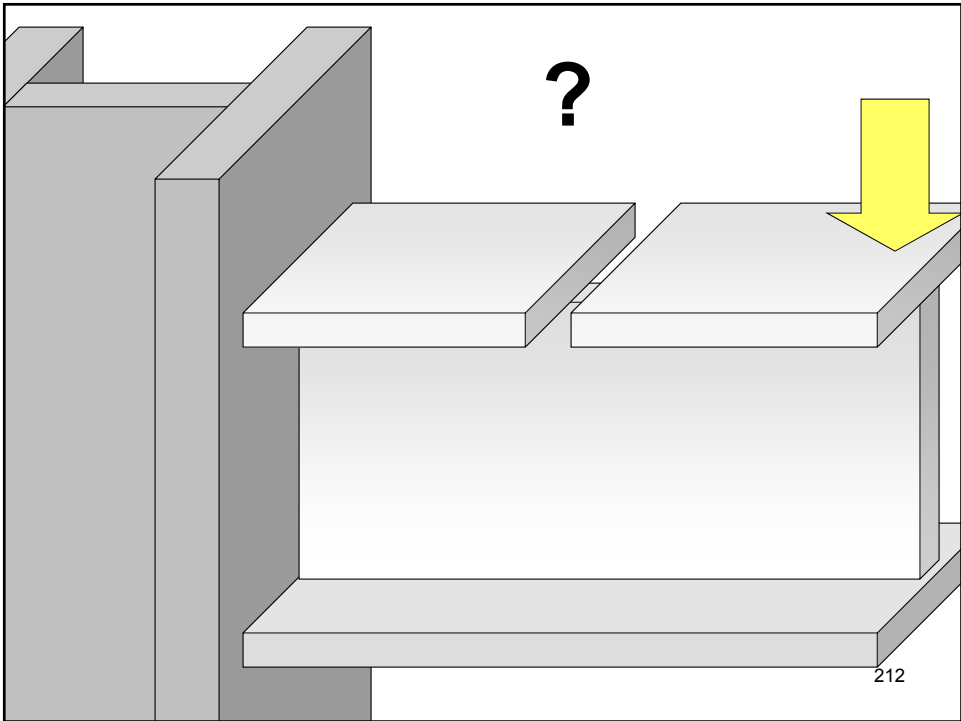
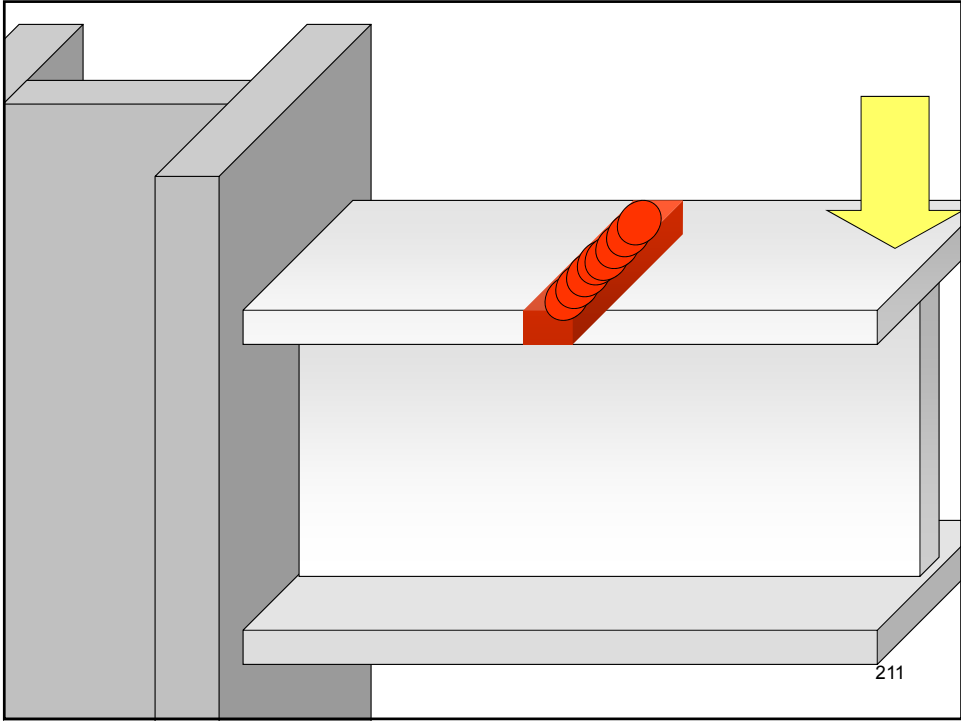
- Historic steels
- ➔ • Welding on members under load
- Fire
- Cold worked steel/strain aged steel
- Comprehensive plans

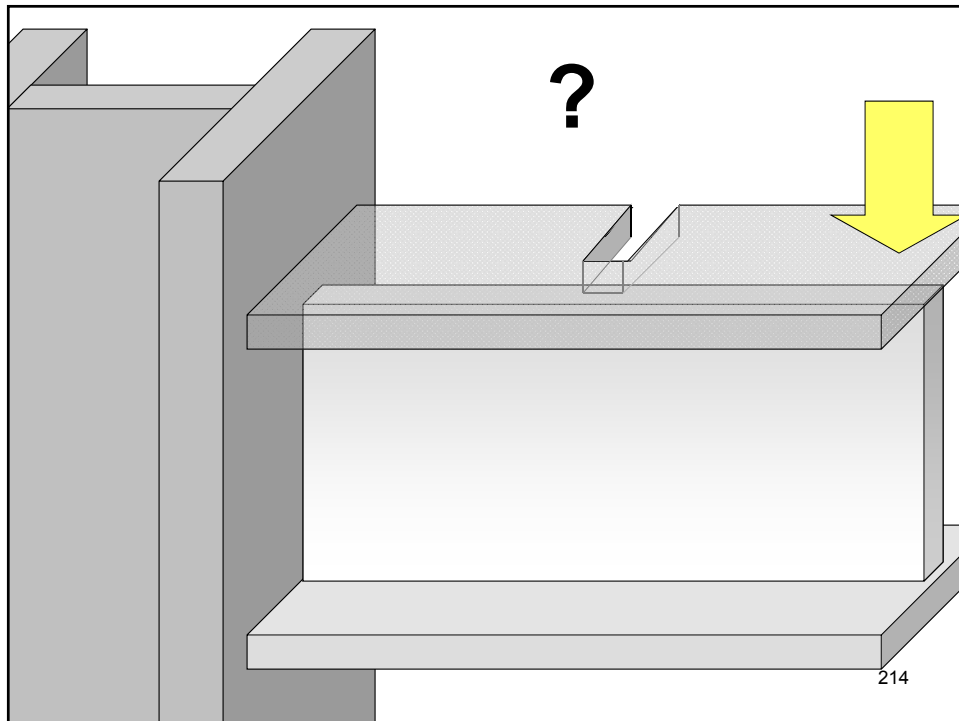
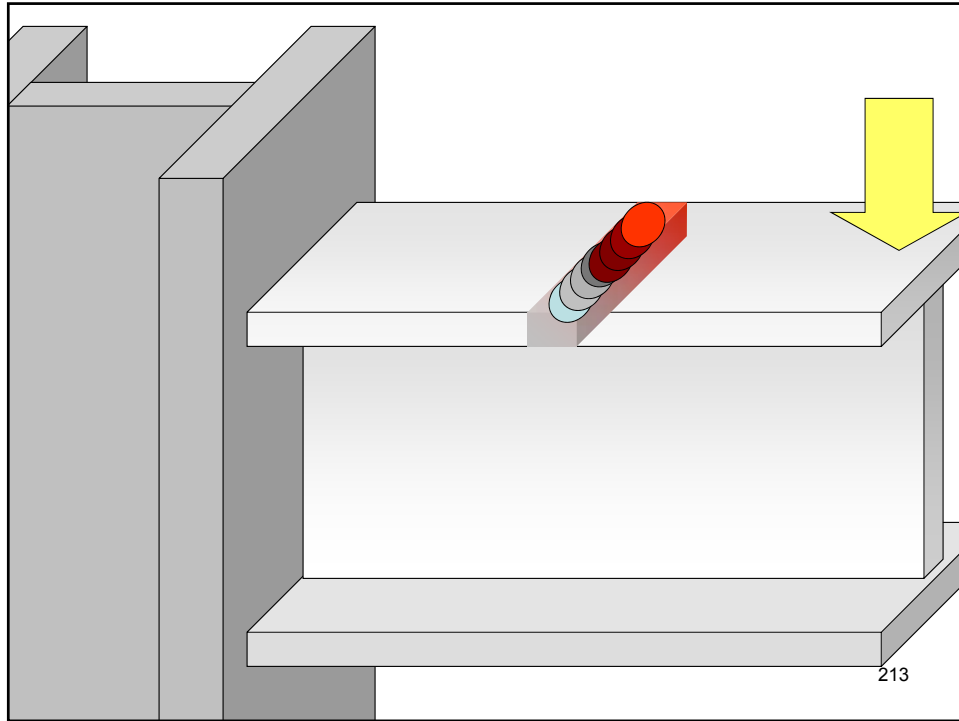


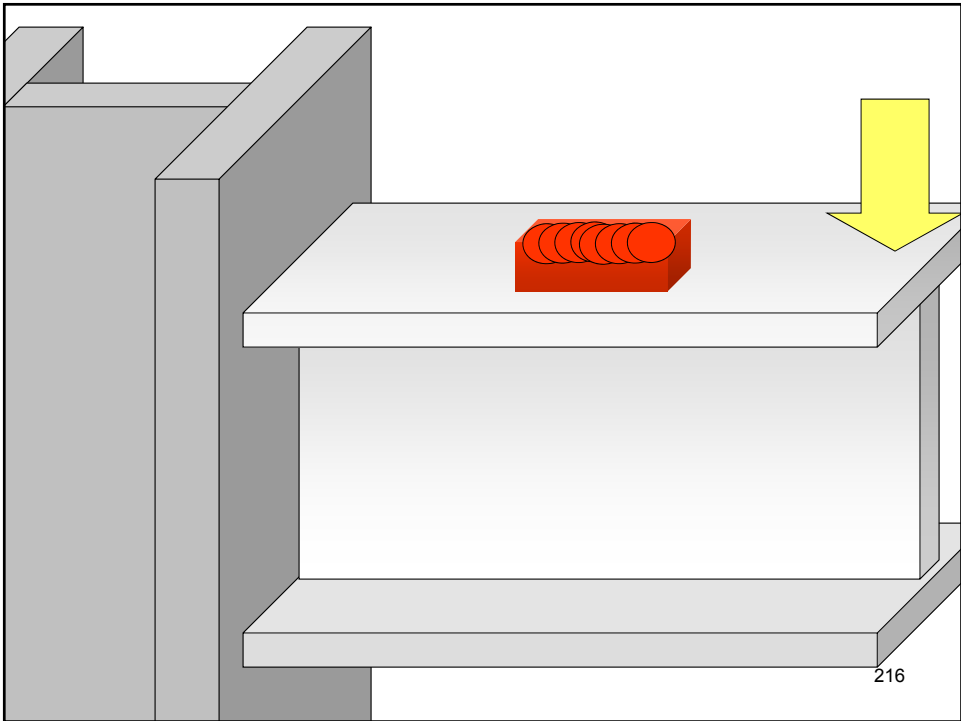
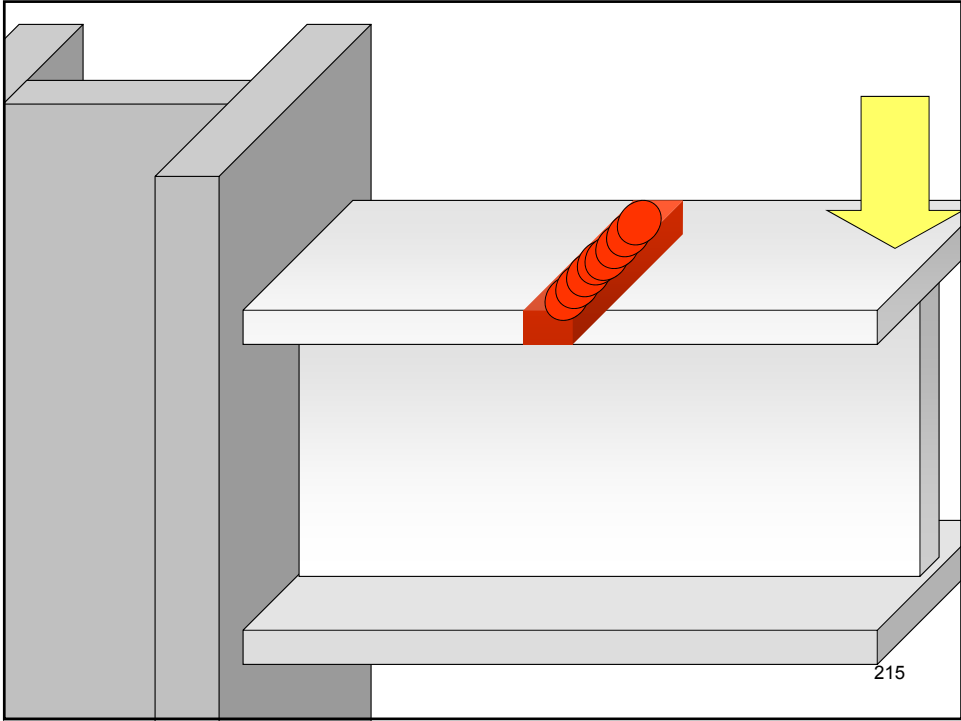
208

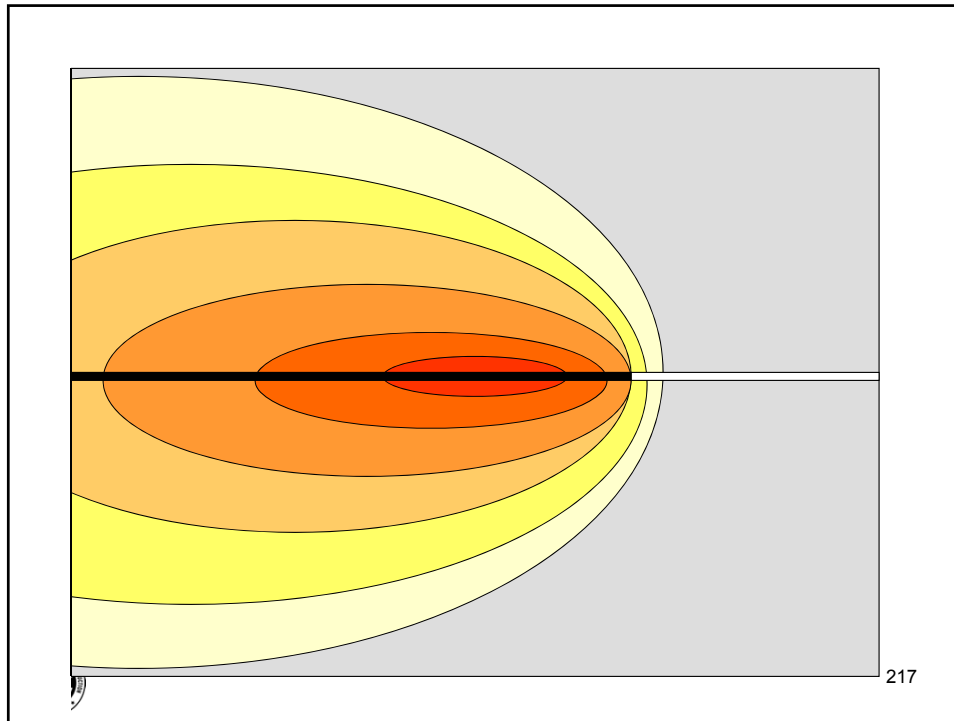












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Table A-4.2.1
Properties of Steel at Elevated Temperatures

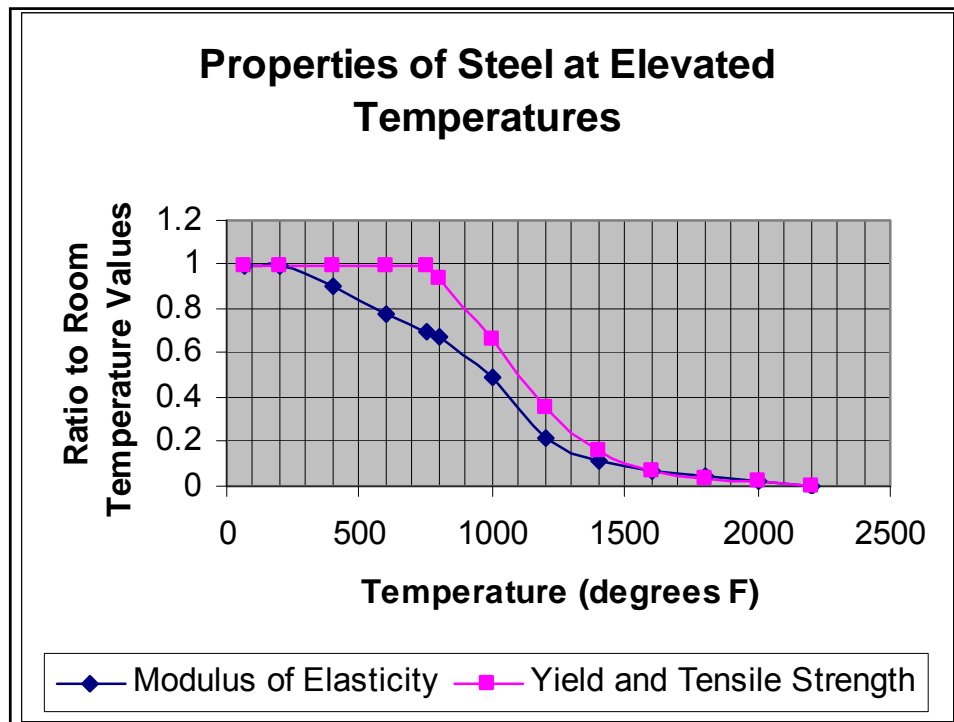
Steel Temperature (°F)[°C]	$k_E = E_m / E$	$k_y = F_{ym} / F_y$	$k_u = F_{um} / F_y$
68 [20]	*	*	*
200 [93]	1.00	*	*
400 [204]	0.90	*	*
600 [316]	0.78	*	*
750 [399]	0.70	1.00	1.00
800 [427]	0.67	0.94	0.94
1000 [538]	0.49	0.66	0.66
1200 [649]	0.22	0.35	0.35
1400 [760]	0.11	0.16	0.16
1600 [871]	0.07	0.07	0.07
1800 [982]	0.05	0.04	0.04
2000 [1093]	0.02	0.02	0.02
2200 [1204]	0.00	0.00	0.00

*Use ambient properties.



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Special Welding Applications and Field Fixes Welding on Existing Structures

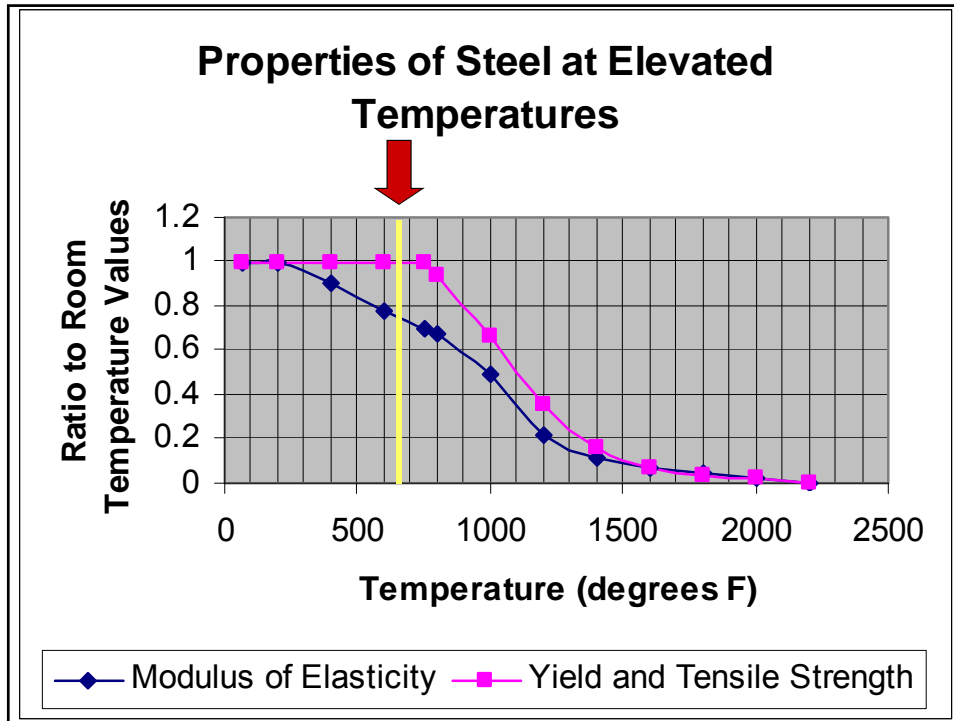
Welding on members under load

- The amount of material at temperatures >650 °F is negligible (Blodgett)
- Only a very small percentage of the cross section experiences reduced properties (Tide)
- The impact of the weld orientation (longitudinal versus transverse) is typically inconsequential (Ricker)
- Each situation should be checked



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Special Welding Applications and Field Fixes Welding on Existing Structures

- Historic steels
- Welding on members under load
- Fire
- Cold worked steel/strain aged steel
- Comprehensive plans

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Special Welding Applications and Field Fixes Welding on Existing Structures

Fire

- Unlike new steel frames, existing structures may have many combustibles in the area.
- Unlike new construction, working on existing structures often involves cutting torches—big concern.
- Unintended welding work lead (“ground”) paths



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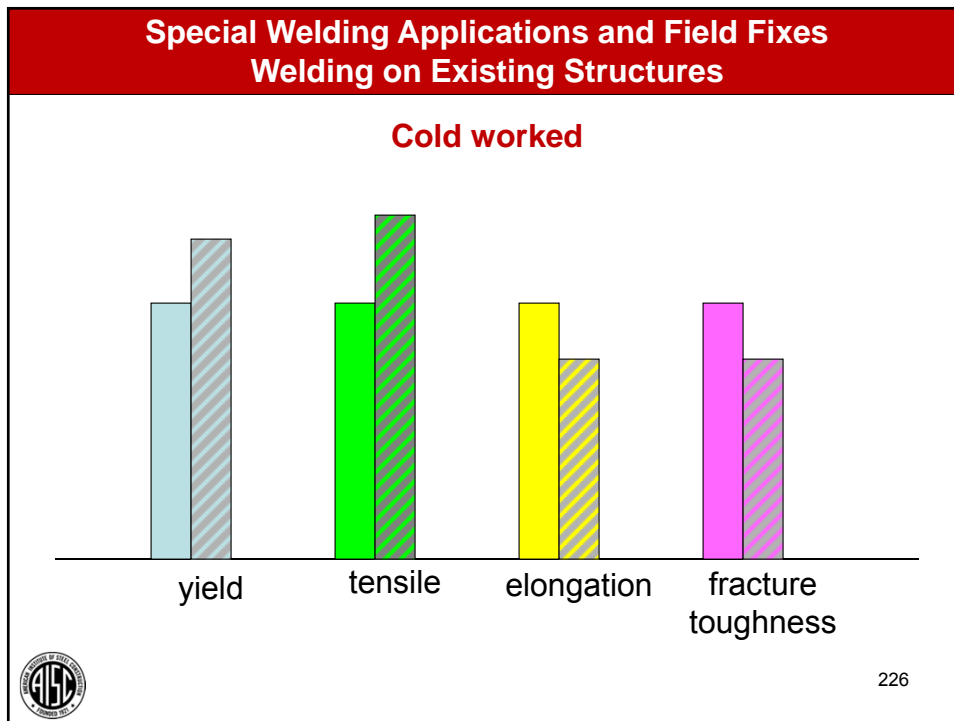
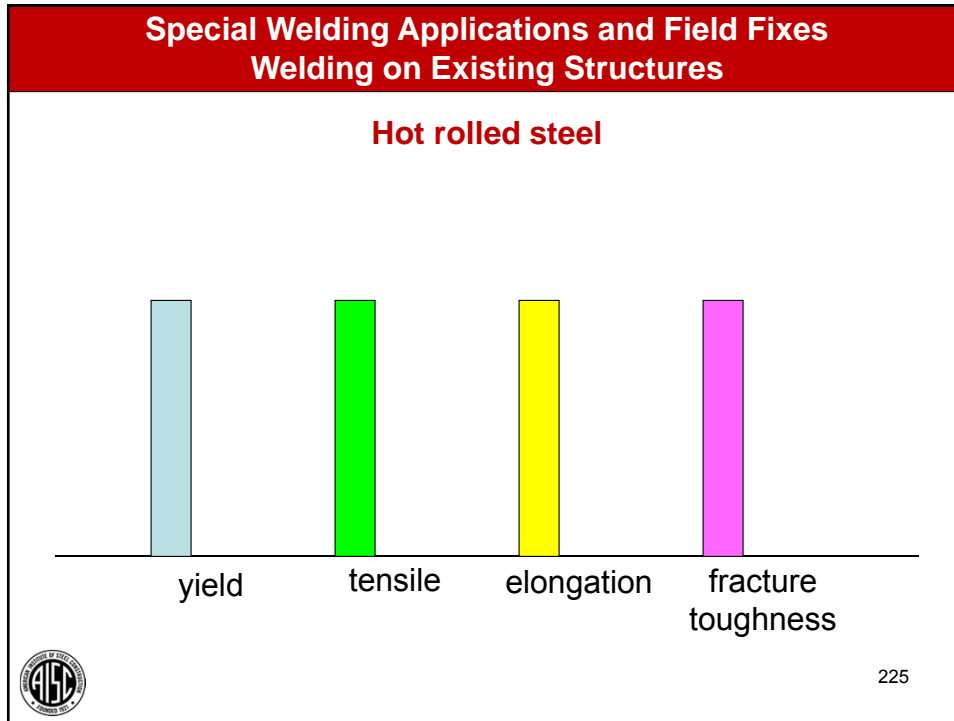
Special Welding Applications and Field Fixes Welding on Existing Structures

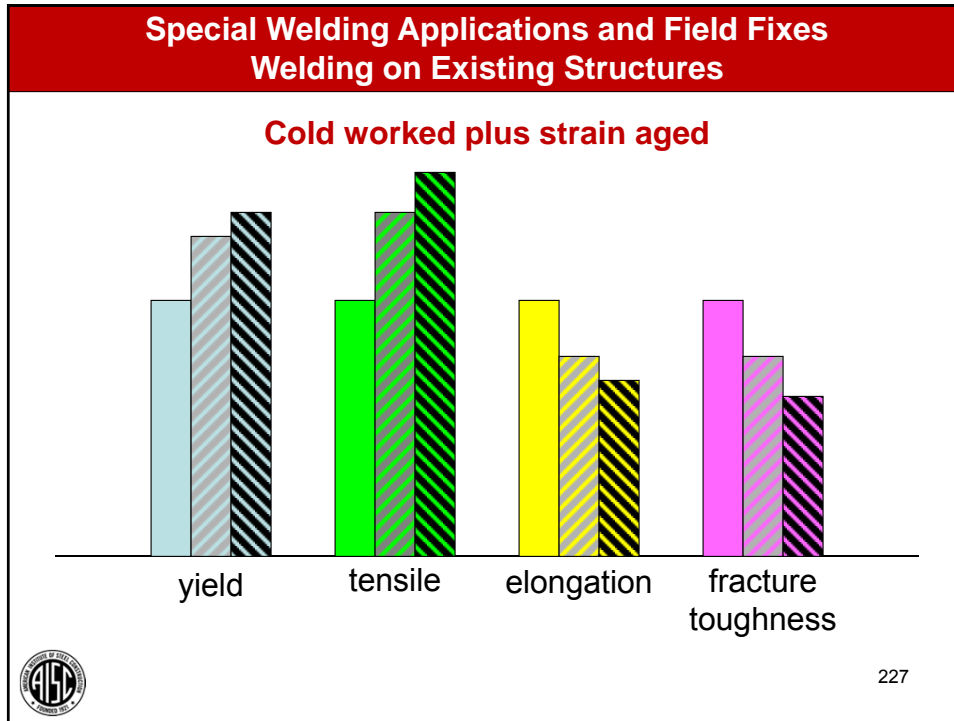
- Historic steels
- Welding on members under load
- Fire
- ➔ • Cold worked steel/strain aged steel
- Comprehensive plans




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- Special Welding Applications and Field Fixes**
Welding on Existing Structures
- Strain aging**
- Occurs when steel is heated to 400-700 °F
 - Yield, tensile increase
 - Ductility, notch toughness decrease
 - Aggravated by presence of “free” nitrogen
 - Stress relief helps, but...
 - Typically impractical
 - Depending on alloy, may experience cracking (Cr, Mo, V, B)
- 
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Special Welding Applications and Field Fixes Welding on Existing Structures

Strain aging: practical implications

- Cold worked steel will be higher in strength, lower in ductility and toughness, and less forgiving.
- Take extra precautions to eliminate cracks and other stress raisers before welding.



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Special Welding Applications and Field Fixes

- Welding on Anchor Rods
- Welding on Heavy Sections (“Jumbo Shapes”)
- Welding HSS
- Welding AESS
- Field Welding
- Welding on Existing Structures
- ➔ • Combining Welds and Bolts



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Special Welding Applications and Field Fixes Combining Welds and Bolts

- Normally, connections are initially designed to be all welded, or all bolted.
- Retrofit work often necessitates more capacity from connections; adding welds to riveted or bolted connections is often an attractive solution.
- Changes in plans for projects under construction may require additional capacity for bolted connections, and welds may offer an attractive solution.



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Special Welding Applications and Field Fixes Combining Welds and Bolts

The “rules” seem to constantly change.

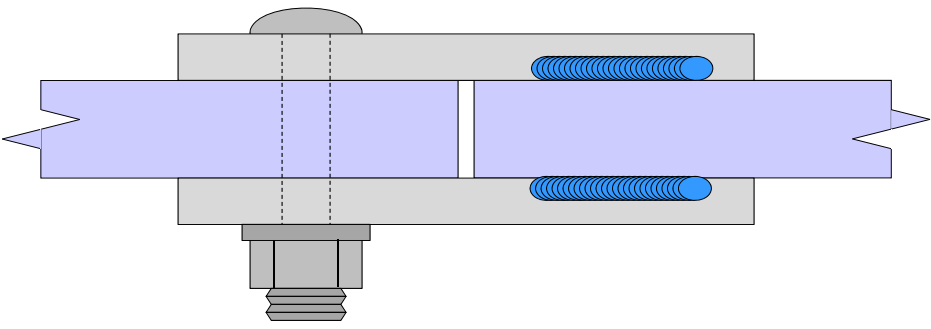


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**Special Welding Applications and Field Fixes
Combining Welds and Bolts**

What is not of concern:



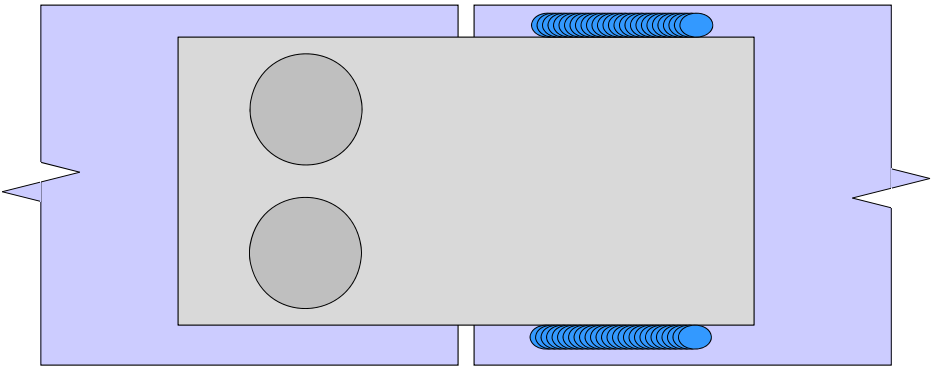
The diagram shows a cross-section of a bolted connection. A central bolt passes through two horizontal plates. The plates are joined by two blue welds, one on the top and one on the bottom. The bolt is shown in a grey color. The plates are shown in a light blue color. The bolt is positioned in the center of the plates. The welds are positioned on the top and bottom surfaces of the plates. The bolt is shown in a grey color. The plates are shown in a light blue color. The bolt is positioned in the center of the plates. The welds are positioned on the top and bottom surfaces of the plates.




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**Special Welding Applications and Field Fixes
Combining Welds and Bolts**

What is not of concern:



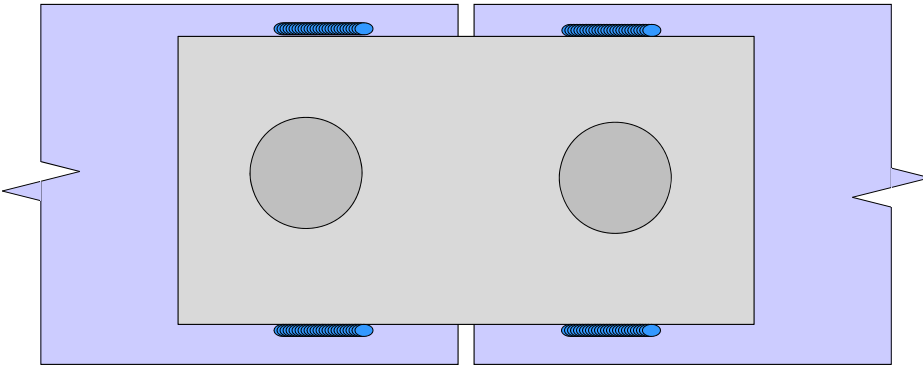
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**Special Welding Applications and Field Fixes
Combining Welds and Bolts**

What is of concern:




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AISC 360-16

J1.8. Bolts in Combination with Welds

Bolts shall not be considered as sharing the load in combination with welds, except in the design of shear connections on a common faying surface where strain compatibility between the bolts and welds is considered.

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AISC 360-16

J1.8. Bolts in Combination with Welds (cont'd)

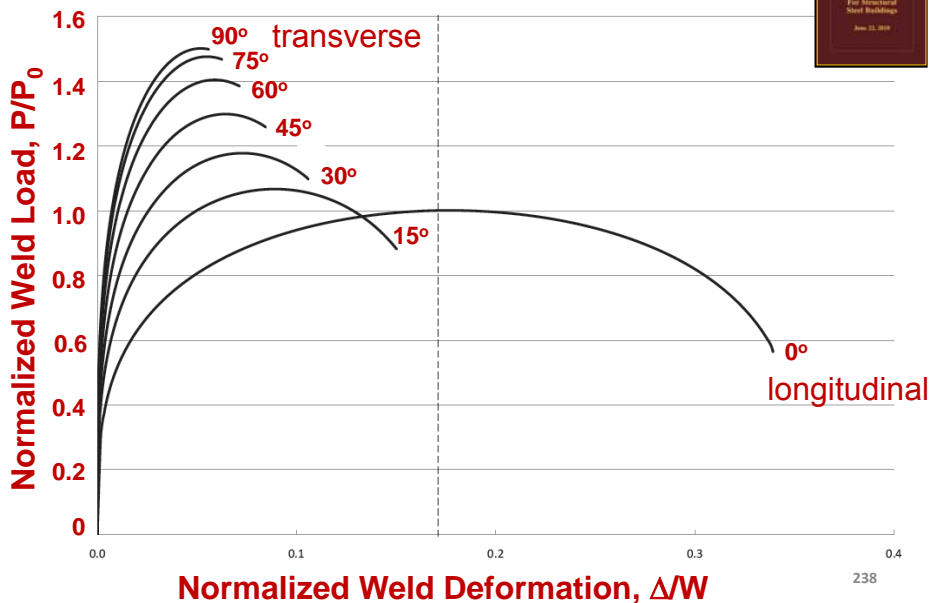
It is permitted to determine the available strength, ΦR_n and R_n/Ω , as applicable, of a joint combining the strengths of high-strength bolts and longitudinal fillet welds as the sum of (1) the nominal slip resistance, R_n , for bolts as defined in Equation J3-4 according to the requirements of a slip critical connection and (2) the nominal weld strength, R_n , as defined in Section J2.4, when the following apply:



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AISC 360-10 SPECIFICATION

Figure C-J2.13



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AISC 360-16

J1.9. Welded Alterations to Structures With Existing Rivets or Bolts

In making welded alterations to structures, existing rivets and high-strength bolts in standard or short-slotted holes transverse to the direction of load, tightened to the requirements of slip-critical connections are permitted to be utilized for resisting loads present at the time of alteration and the welding need only provide the additional required strength.



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AISC 360-16

J1.9. Welded Alterations to Structures With Existing Rivets or Bolts (cont'd)

The weld available strength shall provide the additional required strength, but not less than 25% of the required strength of the connection.



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Special Welding Applications and Field Fixes

- Welding on Anchor Rods
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- Welding on Existing Structures
- Combining Welds and Bolts



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Special Welding Applications and Field Fixes



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- Completely fill out online form. Don't forget to check the boxes next to each attendee's name!



Individual Webinar Registrants

PDH Certificates

Within 2 business days...

- Reporting site (URL will be provided in the forthcoming email).
- Username: Same as AISC website username.
- Password: Same as AISC website password.



3-Session Package Registrants

PDH Certificates

One certificate will be issued at the conclusion of
all 3 sessions.



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Reasons for quiz:

PROFESSIONAL DEVELOPMENT HOURS – If you watch a
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REINFORCEMENT – Reinforce what you learn. Get more out
of the course.

NOTE: If you attend the live presentation, you do not have to
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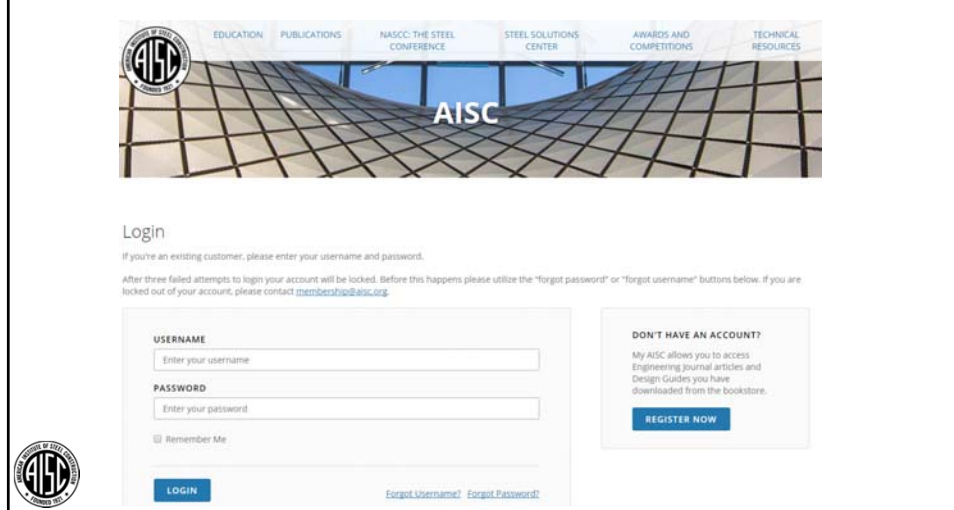
Course Resources

Find all your handouts, quizzes, quiz scores, recording access, and attendance records in one place!

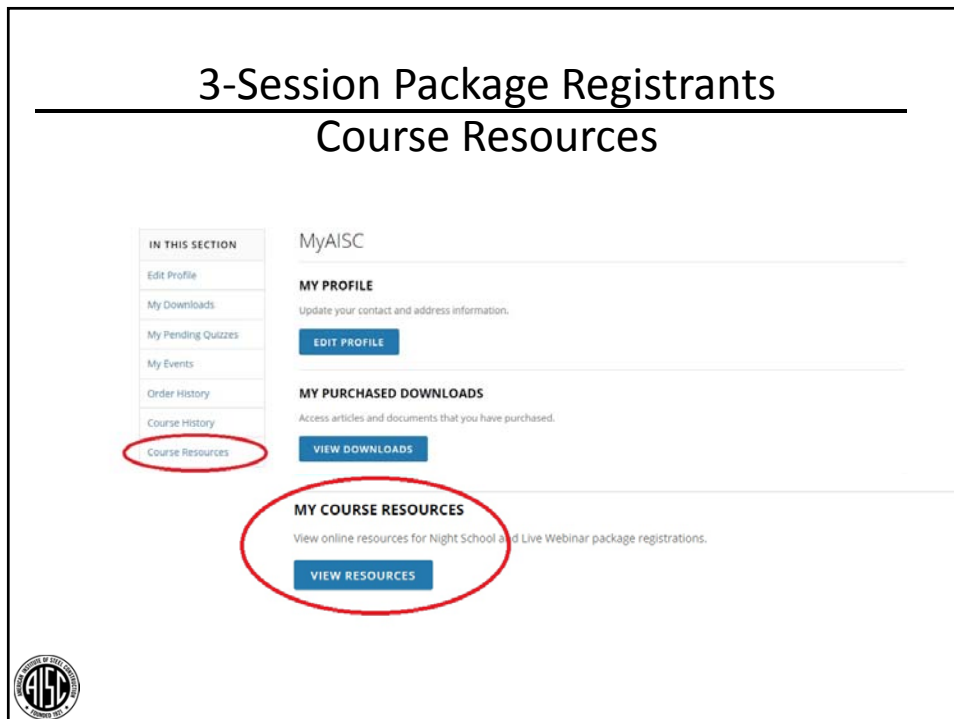


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Course Resources

Event	Start Date
Live Webinar - 3-Session Package: Welded Connections - A Three-Part Webinar Series	6/29/2017 1:30:00 PM
NS 14 8-Session Package-Night School 14 - Fundamentals of Stability	6/5/2017 7:00:00 PM
NS 13 8-Session Package-Night School 13 - Design of Industrial Buildings	1/30/2017 7:00:00 PM



3-Session Package Registrants Course Resources



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Welded Connections

3-SESSION PACKAGE RESOURCES

Event	Date	Handouts	Video	Quiz	Attendance
Part 1: Fundamentals of Welded Connections	Jun 29 2017 1:30PM EDT	Handouts	Available 07/01/2017 5pm EDT	Available 07/01/2017 5pm EDT	Pending
Part 2: Welded Connections for Seismic Service	Jul 6 2017 1:30PM EDT	Handouts	Available 07/08/2017 5pm EDT	Available 07/08/2017 5pm EDT	Pending
Part 3: Special Welding Applications and Field Fixes	Jul 13 2017 1:30PM EDT	Handouts	Available 07/15/2017 5pm EDT	Available 07/15/2017 5pm EDT	Pending




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Within two days, you will receive an email notification regarding access to the quiz and recording for this session. The email will include links to the quiz and recording.

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Webinar connection information:

- Can be found in your confirmation/registration receipt
- Reminder sent out Wednesday afternoon

Link to handouts also found here



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Thank You

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Survey at conclusion of webinar.

