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Course Description

Session 6: Frame Member and Connection Design
March 13, 2017

Lesson 6 incorporates the results of the frame analysis discussed in lesson 5 to demonstrate the design of the building columns, crane columns, and moment connections. The AISC Manual beam-column tables are used for the design of the beam columns to illustrate their use. The design of the Ordinary Moment Frame connection of a truss to the building column is provided. The development of the specification for the joist girders for the example building using the Steel Joist Institute's Technical Digest 11 is also discussed. The design of the column anchor rods is provided including evaluation of limit states according to ACI 318 Chapter 17. Discussion of the recommendations of AISC Design Guide 1 are included in the example as well as the calculation for the thickness of the column base plate.

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Learning Objectives

- Discuss how the results of a frame analysis are used to design columns, crane columns and moments connections.
- List where column and beam-column design values are found in the AISC Steel Construction Manual.
- List the requirements of an Ordinary Moment Frame design per AISC 341-10.
- List the criteria to establish the length and diameter of column anchor rods.

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Design of Industrial Buildings

Session 6: Frame Member and Connection Design
March 13, 2017

Presented by
Jules Van de Pas, SE, PE
Vice President, Computerized Structural Design

structural STEEL

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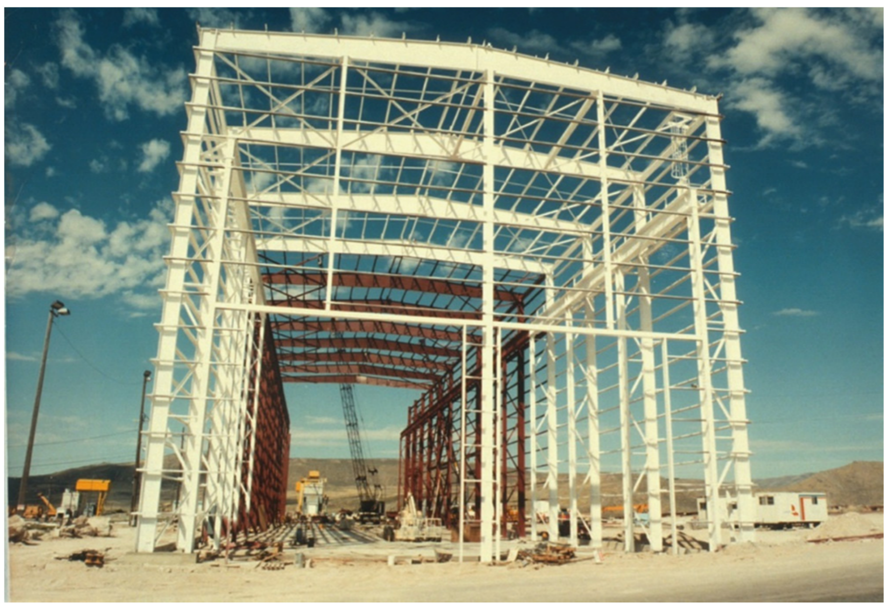
Design of Industrial Buildings
Lesson 6



Presenter:
Jules Van de Pas

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Design of an Industrial Crane Building

- **Lesson 6**
  - Final Design of the Building Columns
  - Final Design of the Crane Columns
  - Final Design of the Truss
  - Design of the Frame Connections
  - Design of the Anchor Rods

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Review of Design Criteria

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Project Description

- 50 ton, top running crane, Class D
- Quantity: 1 per aisle
- Hook height: 45 ft
- Roof type: Standing Seam on Joists
- Wall type: R- panel with continuous Zs
- Automatic Sprinkler System

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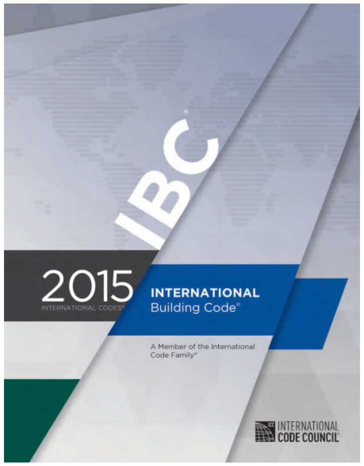
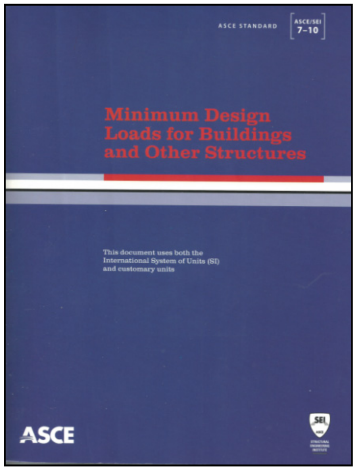
Codes and Standards

- Building Code: IBC 2015
- Minimum Design Loads For Buildings And Other Structures (ASCE 7-10)
- Building Department Contact: John Smith
- Date: July 6, 2016
- Local Ordinances: None
- Wind Speed: 115 mph
- Wind Exposure: C





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Local Code Requirements

- Ground Snow Load: 15 psf
- Seismic Spectral Acceleration:
  - S_s = 1.054 g
  - S_1 = 0.400 g

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Loads

- ROOF DEAD LOAD

– Roofing (SSR)	2.0 psf
– Insulation	1.0 psf
– Roof Bracing	1.0 psf
– Joists	3.0 psf
– Joist Girders	3.0 psf
– Columns	6.0 psf
– MEP Allowance	3.0 psf
– **Total**	**19.0 psf**

- WALL DEAD LOAD (Includes Girts) **3.0 psf**

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Loads

- ROOF LIVE LOADS
  - 20.0 psf (reducible)

- SNOW LOADS
  - Ground Snow Load (P_g): 15.0 psf
  - Building Category: II –> Importance Factor, I_S = 1.0
  - Thermal Factor, C_t: 1.0
  - Exposure Factor, $C_{e,}$ Partially Exposed: 1.0

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Load Calculations - Snow

- Low Slope Roof Snow Load (slope <15°):

$$P_f = 0.7 C_e C_t I P_g = 10.5 \text{ psf}$$

- Minimum Roof Snow for Low Slope Roof

$$P_m = I_S P_g = 15 \text{ psf}$$ controls

- Check Rain-on-Snow Surcharge, slope ¼" per ft.

$$(Slope = 1.19°) < (W/50 = 60/50 = 1.2)$$ Add Surcharge

$$P_f = 15\,psf + 5\,psf = 20 \text{ psf}$$

- Must consider unbalanced snow per 7.6 if slope is ½" per ft or greater.

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Loads

- SEISMIC LOADS
  - Spectral Acceleration, S_s: 1.054 g
  - Spectral Acceleration, S_1: 0.40 g
  - Occupancy Category: II
  - Site Class: D
    - Soil shear wave velocity, $\overline{v}_s$ 800 ft/sec
    - Standard penetration resistance, $\overline{N}$ 15 blows
    - Soil undrained shear strength, $\overline{s}_u$ 1500 psf
  - Importance Factor, I_e : 1.0
  - Seismic Design Category: D

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Load

- Structure is considered to be a "Nonbuilding Structure Similar to Buildings" per Chapter 15 of ASCE 7-10
- Transverse Direction from Table 15.4-1 OMF – Ordinary Moment Frame with permitted height increase

  $R = 2.5$ $\Omega_o = 2.0$ $C_d = 2.5$

  Detailing per AISC 341 Height limit =100 feet.
- Longitudinal Direction from Table 15.4-1 OCBF – Ordinary Concentrically Braced Frame with permitted height increase

  $R = 2.5$ $\Omega_o = 2.0$ $C_d = 2.0$

  Detailing per AISC 341 Height limit of 160 ft.

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Design of an Industrial Crane Building

- **Lesson 6**
  - Final Design of the Building Columns
  - Final Design of the Truss
  - Design of the Frame Connections
  - Design of the Anchor Rods

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Column Design

- Check preliminary building column sizes for forces and moments from the analysis.
- Reanalyze if column sizes change, including adjusted joist girder properties
- Re-check members
- Check drift (serviceability and seismic)
- Final design of the crane columns

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Design of Beam Columns

- Beam Column Design using Manual Tables
  - Part 6 of the Manual contains tables to assist in the design of members for combined forces
  - Table entries included for all W-shapes
  - Could actually be used to design for pure bending, pure compression, and pure tension
  - Available for W-shapes only
  - Includes ALL W-shapes

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Design for Combined Forces

- Interaction Equations
- H1-1a and H1-1b

$$\text{For } \frac{P_r}{P_c} \geq 0.2$$

$$\frac{P_r}{P_c} + \frac{8}{9}\left[\frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}}\right] \leq 1.0$$

$$\text{For } \frac{P_r}{P_c} < 0.2$$

$$\frac{P_r}{2P_c} + \left[\frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}}\right] \leq 1.0$$

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Design for Combined Forces

- These may be rewritten as

$$pP_r + b_x M_{rx} + b_y M_{ry} \leq 1.0 \qquad \text{(H1-1a)}$$

and

$$0.5\,pP_r + \frac{9}{8}\left(b_x M_{rx} + b_y M_{ry}\right) \leq 1.0 \qquad \text{(H1-1b)}$$

respectively

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Design for Combined Forces

- Where

$$p = \frac{1}{P_c}$$

$$b_x = \frac{8}{9M_{cx}}$$

$$b_y = \frac{8}{9M_{cy}}$$

Units are 1/kips and 1/ft-kips

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AISC Manual Table 6-1

W14

Table 6–1 (continued)
Combined Axial and Bending
W Shapes

F_y = 50 ksi

Shape		W14×											
		90[f]				82				74			
Design		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$	
		ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
Effective length KL (ft) with respect to least radius of gyration r_y or Unbraced Length L_b (ft) for X-X axis bending	7	1.31	0.872	2.33	1.55	1.51	1.00	[illegible]	1.71	1.67	1.11	[illegible]	[illegible]
	8	1.33	0.882	2.33	1.55	1.55	1.03	2.56	1.71	1.71	1.14	2.83	1.88
	9	1.34	0.894	2.33	1.55	1.60	1.06	2.57	1.71	1.76	1.17	2.84	1.89
	10	1.36	0.907	2.33	1.55	1.65	1.10	2.61	1.74	1.82	1.21	2.89	1.92
	11	1.38	0.921	2.33	1.55	1.71	1.14	2.66	1.77	1.89	1.26	2.94	1.96
	12	1.41	0.938	2.33	1.55	1.78	1.18	2.70	1.80	1.96	1.31	2.99	1.99
	13	1.44	0.956	2.33	1.55	1.85	1.23	2.75	1.83	2.05	1.36	3.05	2.03
	14	1.47	0.976	2.33	1.55	1.94	1.29	2.79	1.86	2.14	1.43	3.10	2.07
	15	1.50	0.998	2.33	1.55	2.04	1.36	2.84	1.89	2.25	1.50	3.16	2.10
	16	1.54	1.02	2.35	1.57	2.15	1.43	2.89	1.92	2.38	1.58	3.22	2.15
	17	1.58	1.05	2.38	1.59	2.28	1.52	2.94	1.96	2.52	1.67	3.29	2.19
	18	1.62	1.08	2.42	1.61	2.42	1.61	3.00	1.99	2.67	1.78	3.35	2.23
	19	1.67	1.11	2.45	1.63	2.58	1.71	3.05	2.03	2.85	1.89	3.42	2.28
	20	1.72	1.14	2.48	1.65	2.75	1.83	3.11	2.07	3.04	2.02	3.50	2.33
	22	1.83	1.22	2.55	1.70	3.18	2.12	3.23	2.15	3.51	2.34	3.65	2.43
	24	1.97	1.31	2.62	1.74	3.73	2.48	3.37	2.24	4.12	2.74	3.82	2.54
	26	2.12	1.41	2.70	1.79	4.38	2.91	3.51	2.34	4.83	3.22	4.00	2.66
	28	2.31	1.53	2.78	1.85	5.08	3.38	3.67	2.44	5.61	3.73	4.20	2.80
	30	2.52	1.68	2.86	1.91	5.83	3.88	3.84	2.55	6.44	4.28	4.42	2.94
	32	2.77	1.85	2.95	1.97	6.63	4.41	4.03	2.68	7.32	4.87	4.73	3.15
	34	3.07	2.04	3.05	2.03	7.49	4.98	4.28	2.85	8.27	5.50	5.09	3.38

Other Constants and Properties

	90 ASD	90 LRFD	82 ASD	82 LRFD	74 ASD	74 LRFD
$b_y \times 10^3$ (kip-ft)$^{-1}$	4.90	3.26	7.95	5.29	8.80	5.85
$t_y \times 10^3$ (kips)$^{-1}$	1.26	0.840	1.39	0.924	1.53	1.02
$t_r \times 10^3$ (kips)$^{-1}$	1.55	1.03	1.71	1.14	1.88	1.26
r_x/r_y	1.66		2.44		2.44	

[f] Shape does not meet compact limit for flexure with F_y = 50 ksi.

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Table 6-1

- See AISC Manual page 6-4
  - If C_b = 1.0 no adjustments are necessary to use Table 6-1.
  - If $C_b \geq 1.0$, then select b_x from Table 6-1 using L_b and the divide b_x by C_b for checking the section. ($b_x / C_b > b_{xmin.}$)
  - If $pP_r < 0.2$ then divide p by 2 and multiply b_x by 9/8 for checking the section.

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AISC Manual Table 6-1

W30-W27

Table 6-1 (continued)
Combined Flexure and Axial Force
W-Shapes

F_y = 50 ksi

Shape	W30×								W27×			
	99[c]				90[c, v]				539[h]			
Design	$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$	
Effective length, KL (ft), with respect to [illegible] radius of gyration, r_y, or Unbraced Length, L_b (ft), fo[illegible] axis bending	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
0	1.31	0.872	1.14	0.760	1.49	0.994	1.26	0.838	0.210	0.140	0.189	0.125
11	1.63	1.08	1.27	0.846	1.85	1.23	1.41	0.936	0.231	0.154	0.189	0.125
12	1.70	1.13	1.31	0.874	1.93	1.28	1.45	0.968	0.235	0.157	0.189	0.125
13	1.79	1.19	1.36	0.903	2.02	1.35	1.51	1.00	0.240	0.160	0.189	0.125
14	1.89	1.26	1.41	0.935	2.13	1.42	1.56	1.04	0.245	0.163	0.190	0.126
15	2.01	1.33	1.46	0.969	2.26	1.50	1.62	1.08	0.251	0.167	0.191	0.127
16	2.14	1.43	1.51	1.01	2.41	1.60	1.68	1.12	0.257	0.171	0.192	0.128
17	2.30	1.53	1.57	1.04	2.59	1.72	1.75	1.16	0.264	0.176	0.193	0.128
18	2.50	1.66	1.63	1.09	2.79	1.86	1.82	1.21	0.271	0.181	0.194	0.129
19	2.73	1.81	1.70	[illegible]	[illegible]	2.02	1.90	1.27	0.279	0.186	0.195	0.130
20	3.00	1.99	1.78	[illegible]	[illegible]	[illegible]	1.99	1.32	0.288	0.192	0.196	0.131
22	3.63	2.41	2.00	1.33	4.04	2.69	2.28	1.52	0.308	0.205	0.199	0.132
24	4.31	2.87	2.32	1.54	4.80	3.20	2.65	1.76	0.331	0.220	0.201	0.134
26	5.06	3.37	2.65	1.76	5.64	3.75	3.04	2.02	0.358	0.238	0.203	0.135
28	5.87	3.91	2.99	1.99	6.54	4.35	3.44	2.29	0.390	0.260	0.206	0.137
30	6.74	4.49	3.34	2.22	7.51	4.99	3.85	2.56	0.428	0.285	0.208	0.139
32	7.67	5.10	3.69	2.46	8.54	5.68	4.27	2.84	0.472	0.314	0.211	0.140
34	8.66	5.76	4.06	2.70	9.64	6.41	4.70	3.13	0.524	0.348	0.213	0.142
36									0.586	0.390	0.216	0.144
38									0.653	0.435	0.219	0.146
40									0.724	0.481	0.222	0.148
42									0.798	0.531	0.225	0.149
44									0.876	0.583	0.228	0.151
46									0.957	0.637	0.231	0.154
48									1.04	0.693	0.234	0.156
50									1.13	0.752	0.237	0.158

Other Constants and Properties

	W30×99 ASD	W30×99 LRFD	W30×90 ASD	W30×90 LRFD	W27×539 ASD	W27×539 LRFD
$b_y \times 10^3$, (kip-ft)$^{-1}$	9.23	6.14	10.3	6.83	0.815	0.542
$t_y \times 10^3$, (kips)$^{-1}$	1.15	0.766	1.27	0.845	0.210	0.140
$t_r \times 10^3$, (kips)$^{-1}$	1.41	0.943	1.56	1.04	0.258	0.172
r_x/r_y	5.57		5.60		3.48	
r_y, in.	2.10		2.09		3.65	

[c] Shape is slender for compression with $F_y = 50$ ksi.
[h] Flange thickness greater than 2 in. Special requirements may apply per AISC *Specification* Section A3.1c.
[v] Shape does not meet the h/t_w limit for shear in AISC *Specification* Section G2.1(a) with $F_y = 50$ ksi; therefore, $\phi_v = 0.90$ and $\Omega_v = 1.67$.
Note: Heavy line indicates KL/r_y equal to or greater than 200.

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Table 6-1

- Exterior columns: W30x99 P_r = 16.9 kips, M_r =359 kip- ft
- Since the column has large bending moments compared to axial forces check first by using the beam Table 3-10. Try an unbraced length of 20 ft.

$$px10^3 = 3.00; b_x x10^3 = 1.78$$

$$pP_r = (3x10^{-3})(16.9) = (0.003)(16.9) = .051 < 0.2$$

$$(1/2)(.003)(16.9) + (9/8)(0.00178)(359 kip - ft) = .74$$

$$.74 < 1.0 \ OK$$

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Table 6-1

- Interior columns: W24x146 P_a = 29.3 kips, M_a =430 kip- ft.
- Laterally braced at top of crane column = 42.5 ft.

$$px10^3 = 4.45; b_x = 1.88x10^{-3}$$

$$pP_a = (4.45x10^{-3})(29.3) = (0.00445)(29.3) = 0.13 < 0.2$$

$$(1/2)pP_r + 9/8(b_x M_{rx} + b_y M_{ry}) \leq 1.0$$

$$(.5)(0.00445)(29.3\ kips) + \left({}^{9}/_{8}\right)(.00188)(430 kip - ft) =$$

$$.97 < 1.00 \quad OK \quad \text{-demonstrate adjustment for } C_b$$

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AISC Manual Table 6-1

F_y = 50 ksi

Table 6-1 (continued)
Combined Flexure and Axial Force
W-Shapes

W24

Shape	W24×											
	176				162				146			
Design	$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$		$p \times 10^3$ (kips)$^{-1}$		$b_x \times 10^3$ (kip-ft)$^{-1}$	
	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
0	0.646	0.430	0.697	0.464	0.699	0.465	0.761	0.506	0.777	0.517	0.852	0.567
11	0.742	0.493	0.700	0.466	0.801	0.533	0.764	0.508	0.894	0.595	0.857	0.571
12	0.761	0.506	0.710	0.472	0.822	0.547	0.776	0.516	0.918	0.611	0.872	0.580
13	0.783	0.521	0.721	0.479	0.846	0.563	0.788	0.524	0.945	0.629	0.887	0.590
14	0.808	0.537	0.731	0.487	0.872	0.580	0.801	0.533	0.975	0.649	0.902	0.600
15	0.835	0.555	0.743	0.494	0.901	0.600	0.814	0.541	1.01	0.671	0.918	0.611
16	0.865	0.575	0.754	0.502	0.934	0.621	0.827	0.550	1.05	0.696	0.935	0.622
17	0.898	0.597	0.766	0.510	0.969	0.645	0.841	0.560	1.09	0.723	0.952	0.633
18	0.934	0.622	0.778	0.518	1.01	0.671	0.855	0.569	1.13	0.753	0.970	0.645
19	0.975	0.649	0.791	0.526	1.05	0.700	0.870	0.579	1.18	0.786	0.988	0.657
20	1.02	0.678	0.804	0.535	1.10	0.731	0.886	0.589	1.24	0.823	1.01	0.670
22	1.12	0.746	0.832	0.553	1.21	0.804	0.918	0.611	1.36	0.907	1.05	0.697
24	1.25	0.829	0.861	0.573	1.34	0.892	0.953	0.634	1.52	1.01	1.09	0.727
26	1.40	0.928	0.893	0.594	1.50	0.999	0.991	0.660	1.70	1.13	1.14	0.759
28	1.58	1.05	0.927	0.617	1.70	1.13	1.03	0.687	1.93	1.29	1.19	0.794
30	1.80	1.20	0.964	0.641	1.94	1.29	1.08	0.716	2.21	1.47	1.25	0.832
32	2.05	1.37	1.00	0.668	2.21	1.47	1.13	0.749	2.52	1.68	1.31	0.874
34	2.32	1.54	1.05	0.697	2.49	1.66	1.18	0.784	2.84	1.89	1.39	0.926
36	2.60	1.73	1.09	0.728	2.79	1.86	1.24	0.826	3.19	2.12	1.50	1.00
38	2.90	1.93	1.15	0.767	3.11	2.07	1.33	0.886	3.55	2.36	1.62	1.08
40	3.21	2.13	1.23	0.818	3.45	2.29	1.42	0.947	3.93	2.62	1.73	1.15
42	3.54	2.35	1.31	0.869	3.80	2.53	[illegible]	[illegible]	4.34	2.89	1.85	1.23
44	3.88	2.58	1.38	0.920	4.17	2.78	1.60	1.07	4.76	3.17	1.96	1.30
46	4.24	2.82	1.46	0.970	4.56	3.03	1.69	1.13	5.20	3.46	2.07	1.38
48	4.62	3.07	1.53	1.02	4.96	3.30	1.78	1.19	5.67	3.77	2.19	1.45
50	5.01	3.34	1.61	1.07	5.39	3.58	1.87	1.25	6.15	4.09	2.30	1.53

Effective length, *KL* (ft), with respect to least radius of gyration, r_y, or Unbraced Length, L_b (ft), for X-X axis bending

Other Constants and Properties

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Table 6-1

- Interior columns: W24x146 P_r = 29.3 kips, M_r =430 kip- ft
- Laterally braced at top of crane column = 42.5 ft

$$px10^3 = 4.45;\ b_x = 1.88x10^{-3}$$

$$Say\ C_b = 1.75\ \ (from\ evaluation\ of\ moment\ diagram)$$

$$b_x = 1.88x10^{-3}/1.75 = 1.07x10^{-3} > b_{x(min)} = 0.852x10^{-3}$$

$$(.5)(0.00445)(29.3\ kips) + ({}^{9}/_{8})(.00107)(430kip - ft) =$$

$$.59 \leq 1.0\ \ ok$$

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Final Column Sizes

- Exterior Columns: W30x99
  - Braced by struts aligned with longitudinal bracing, L_b = 20 ft. max.
- Interior Columns: W24x146
  - Braced by crane beam / longitudinal crane bracing
- Crane Columns: W14x90 if only one tie provided at top of column; W14x61 if add intermediate tie or brace at mid-height to adjacent building column

There's always a solution in steel!

Design of an Industrial Crane Building

- **Lesson 6**
  - Final Design of the Building Columns
  - Final Design of the Truss
  - Design of the Frame Connections
  - Design of the Anchor Rods

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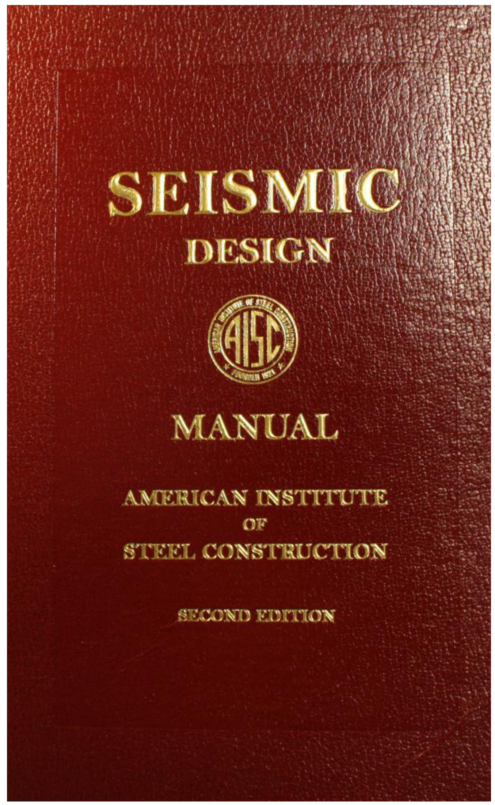
AISC Seismic Manual 2010



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2010 AISC Seismic Provisions E.1 Ordinary Moment Frames

Application of OMF Requirements (E.1 & Commentary):

- Minimal inelastic deformation capacity required, members and connections
- No limits on width to thickness ratios of members beyond the *Specification*.
- Truss and FR moment connection is designed for required flexural strength and required shear strength equal to the maximum moment and corresponding shear that can be transferred to the truss and the connection by the system including the effects of overstrength and strain hardening.

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2010 AISC Seismic Provisions E.1 Ordinary Moment Frames

Application of OMF Requirements (E.1 & Commentary):

The maximum force transferred by the system is determined based on flexural yielding (hinging) of the moment frame columns.

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Design of the OMF Truss

- Determine end moments and axial forces acting on the truss for the seismic load cases

- E based on $1.1R_yM_p$ of the columns LRFD
- ($1.1R_yM_p/1.5$ for ASD)

There's always a solution in steel!

Design of the OMF Truss

Determine Chord forces acting on the end of the truss due to column yielding.

- W30x99 column at the left end of the truss

M_{eleft}=1.1*1.1*50*312/1.5=12,584”$^{-k}$

P_{eleft}=12584”$^{-k}$/(60”-3”)=221^{k}

- W24x146 column at the right end of the truss

M_{eright}=1.1*1.1*50*418/1.5/2=8430”$^{-k}$

P_{eright}=8430”$^{-k}$/(60”-3”)=148^{k}

Determine truss Gravity Loads for load case 5a

P_{vert}=(1.+0.14*.77)(.013)(5)(30)=2.1^{k}

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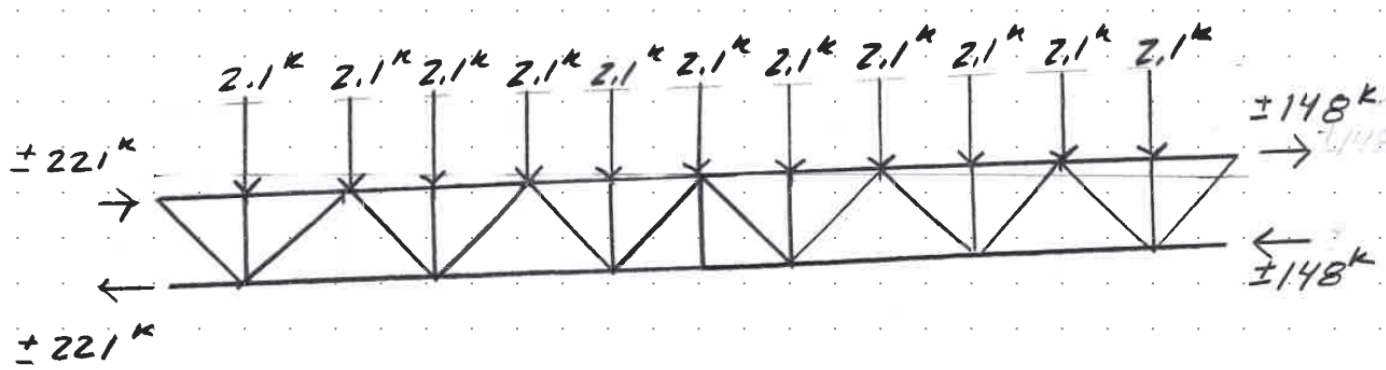
Design of the OMF Truss

Load Diagram Load Case 5a (ASCE 7-10 Section 12.2.2.3)



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Design of the OMF Truss

Model the truss with continuous chords and pinned diagonal members.

Based on analysis of the truss for the load diagram on the previous slide, the top chord forces at the critical location are:

- P_{max}=204.7^{k}
- M_{max}=62.5$^{"\text{-}k}$
- Check WT9x43.0 chord. Based on aligning braces with roof bracing use 10' unbraced length.
- Axial Strength use table 4-7

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Design of the OMF Truss

WT9

Table 4-7 (continued)

Available Strength in Axial Compression, kips

WT-Shapes

F_y = 50 ksi

Shape		WT9×											
lb/ft		48.5		43[c]		38[c]		35.5[c]		32.5[c]		30[c]	
Design		P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD
Effective length, KL (ft), with respect to indicated axis: X-X Axis	0	425	639	356	534	274	412	299	450	250	376	210	315
	10	362	544	306	459	239	360	262	393	221	332	187	281
	12	337	507	286	430	226	339	246	370	209	314	178	267
	14	310	466	264	397	210	316	230	345	196	295	168	252
	16	282	424	241	363	194	292	212	319	182	273	157	235
	18	253	380	218	327	177	266	193	291	167	251	145	218
	20	224	336	194	292	160	240	175	262	152	229	133	200
	22	195	294	171	257	143	215	156	234	137	206	121	182
	24	169	253	149	223	126	190	138	207	122	184	109	164
	26	144	216	128	192	110	166	120	181	108	162	97.1	146
	28	124	186	110	165	95.3	143	104	156	94.1	141	85.9	129
	30	108	162	95.8	144	83.1	125	90.6	136	81.9	123	75.1	113
	32	94.9	143	84.2	127	73.0	110	79.6	120	72.0	108	66.0	99.2
	34	84.0	126	74.6	112	64.7	97.2	70.5	106	63.8	95.9	58.5	87.9
	36	75.0	113	66.5	100	57.7	86.7	62.9	94.5	56.9	85.5	52.2	78.4
	40	60.7	91.2	53.9	81.0	46.7	70.2	50.9	76.6	46.1	69.3	42.3	63.5
Y-Y Axis	0	425	639	356	534	274	412	299	450	250	376	210	315
	10	[illegible]	[illegible]	287	431	219	330	200	301	171	258	147	221
	12	[illegible]	[illegible]	274	412	212	319	173	259	150	225	130	195
	14	303	456	258	387	202	304	144	217	127	191	112	168
	16	279	419	238	358	189	284	117	176	105	158	93.7	141
	18	253	380	217	326	174	262	93.5	140	84.4	127	76.6	115
	20	226	340	195	293	159	238	76.3	115	68.9	104	62.6	94.1
	22	200	301	173	260	143	215	63.3	95.2	57.3	86.1	52.1	78.3
	24	175	263	152	229	127	191	53.4	80.3	48.4	72.7	44.0	66.1
	26	151	227	132	198	112	169	45.7	68.6	41.3	62.1	37.6	56.6
	28	131	196	114	172	97.7	147	39.5	59.3	35.7	53.7	32.6	48.9
	30	114	171	99.8	150	85.4	128						
	32	100	151	88.0	132	75.4	113						
	34	89.1	134	78.1	117	66.9	101						
	36	79.6	120	69.8	105	59.9	90.0						
	40	64.6	97.0	56.7	85.2	48.7	73.1						
Properties													
A_g, in.^{2}		14.2		12.7		11.1		10.4		9.55		8.82	
r_x, in.		2.56		2.55		2.54		2.74		2.72		2.71	
r_y, in.		2.65		2.63		2.61		1.70		1.69		1.68	

ASD	LRFD
$\Omega_c = 1.67$	$\phi_c = 0.90$

[c] Shape is slender for compression with F_y = 50 ksi.
Note: Heavy line indicates KL/r equal to or greater than 200.

$P_n/\Omega = 287^k$

Table 4-7 considers torsional and flexural torsional buckling per Specification Section E4

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Design of the OMF Truss

- Calculate Flexural Strength per Section F9.
- Applicable limit states are yielding, Lateral torsional buckling, and local buckling.
- Yielding per F9.1(b) stem in compression

$$M_p = F_y Z_x \leq M_y \text{ where } M_y = F_y S_x$$

$$M_p = (50\ ksi)(19.90 in^3) \leq (50\ ksi)(11.2 in^3)$$

$$M_p = 560\ in.-kip$$

There's always a solution in steel!

Design of the OMF Truss

- Lateral Torsional Buckling per F9.2 with stem in compression

$$M_{cr} = (\frac{\pi\sqrt{EI_y GJ}}{L_b})(B + \sqrt{1 + B^2})$$

Where: $B = \pm 2.3(d/L_b)\sqrt{\frac{I_y}{J}}$

+ B applies for stem in tension
– B applies for stem in comp.

There's always a solution in steel!

Design of the OMF Truss

- Lateral Torsional Buckling per F9.2 with stem in compression

$$B = -2.3\left(\frac{9.2}{120}\right)\sqrt{\frac{87.6}{2.04}} = -1.15$$

$$Mcr =$$

$$\left(\frac{3.14\sqrt{(29000)(87.6)(11200)(2.04)}}{120}\right)(-1.15 + \sqrt{1 + (-1.15)^2})$$

$$M_{cr} = 2{,}347\ in.-kip > Mp$$

Lateral torsional buckling does not control

There's always a solution in steel!

Design of the OMF Truss

- Local Buckling of the Tee stem F9.4
  stem in compression

$M_n = F_{cr} S_x$ when $\frac{d}{t_w} \leq .84\sqrt{\frac{E}{F_y}}$ $F_{cr} = F_y$

$$\frac{d}{t_w} = 19.2 \leq .84\sqrt{\frac{29000ksi}{50ksi}} = 20.2 \quad Mn = (50ksi)(11.2\ in^3)$$

$$M_n = 560\ in.-kip \qquad M_n/\Omega = \frac{560\ in.-kip}{1.67} = 335\ in-kip$$

There's always a solution in steel!

Design of the OMF Truss

- Check Combined Axial and Bending of the Tee stem

P_r=204.7 kips P_n/Ω =287 kips

M_r=62.5 in-kip $M_n/\Omega = 335\ in - kip$

$$\frac{204.7}{287} + \frac{8}{9}\left(\frac{62.5}{335}\right) = .88 \leq 1.0\ \ OK$$

There's always a solution in steel!

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Design of the OMF Truss

Verify the diagonal members:

Based on analysis:

Max. P_r=- 60.2^k

Based on truss geometry:
L=83" =6.9 ft.

2L3 ½ x3 ½ x 5/16

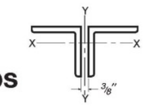
X axis controls

$P_n/\Omega = 65.8^k$

3 equally spaced connectors required.

F_y = 36 ksi

Table 4-8 (continued)
Available Strength in Axial Compression, kips
Double Angles—Equal Legs



2L3½

Shape		2L3½×3½×										
		½		7/16		3/8		5/16		¼[c]		No. of connectors[a]
lb/ft		22.2		19.6		17.0		14.4		11.6		
Design		P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	P_n/Ω_c ASD	$\phi_c P_n$ LRFD	
Effective length, KL (ft), with respect to indicated axis: X-X Axis	0	140	211	125	187	108	162	90.5	136	70.7	106	
	1	139	209	124	186	107	161	90.0	135	70.3	106	
	2	136	205	121	182	105	158	88.2	133	69.0	104	
	3	132	198	117	176	102	153	85.4	128	66.9	101	
	4	126	189	112	168	96.9	146	81.6	123	64.1	96.3	
	5	118	177	105	158	91.3	137	77.0	116	60.6	91.1	
	6	109	164	97.7	147	84.9	128	71.7	108	56.7	85.2	
	7	100	150	89.5	135	77.9	[illegible]	65.8	99.0	52.3	78.6	
	8	90.2	136	80.9	122	70.6	106	59.7	89.8	47.7	71.7	
	9	80.3	121	72.1	108	63.0	94.8	53.5	80.4	43.0	64.6	b
	10	70.4	106	63.5	95.4	55.6	83.6	47.3	71.0	38.2	57.4	
	11	61.0	91.6	55.1	82.8	48.4	72.7	41.2	62.0	33.6	50.5	
	12	51.9	78.1	47.1	70.8	41.5	62.4	35.5	53.4	29.1	43.8	
	13	44.3	66.5	40.1	60.3	35.4	53.1	30.3	45.5	24.9	37.5	
	14	38.2	57.4	34.6	52.0	30.5	45.8	26.1	39.2	21.5	32.3	
	15	33.2	50.0	30.1	45.3	26.6	39.9	22.7	34.2	18.7	28.2	
	16	29.2	43.9	26.5	39.8	23.3	35.1	20.0	30.0	16.5	24.8	
	17	25.9	38.9	23.5	35.3	20.7	31.1	17.7	26.6	14.6	21.9	
	18							15.8	23.7	13.0	19.6	
Y-Y Axis	0	140	211	125	187	108	162	90.5	136	70.7	106	
	2	135	203	119	178	101	152	82.1	123	55.1	82.8	
	4	130	196	115	172	97.6	147	79.5	120	54.7	82.3	
	6	123	185	109	163	92.3	[illegible]	75.4	113	53.9	80.9	
	8	114	172	100	151	85.4	[illegible]	69.8	105	51.9	78.0	
	10	101	151	88.3	133	75.3	113	61.8	92.8	47.3	71.1	
	12	88.1	132	77.1	116	65.7	98.8	54.0	81.2	41.8	62.8	3
	14	75.1	113	65.6	98.6	55.9	84.0	46.0	69.2	35.6	53.6	
	16	62.5	93.9	54.4	81.7	46.3	69.6	38.2	57.4	29.5	44.4	
	18	50.6	76.0	43.9	65.9	37.4	56.1	30.8	46.3	23.9	35.9	
	20	41.0	61.7	35.6	53.5	30.4	45.6	25.1	37.7	19.5	29.3	
	22	34.0	51.0	29.5	44.3	25.2	37.8	20.8	31.3	16.2	24.4	
	24	28.6	42.9	24.8	37.3	21.2	31.8	17.5	26.3	13.7	20.6	
	26	24.4	36.6	21.2	31.8	18.1	27.2	15.0	22.5	11.7	17.6	

Properties of 2 angles—3/8 in. back to back

	½	7/16	3/8	5/16	¼
A_g, in.^{2}	6.50	5.78	5.00	4.20	3.40
r_x, in.	1.05	1.06	1.07	1.08	1.09
r_y, in.	1.63	1.61	1.60	1.59	1.57

Properties of single angle

	½	7/16	3/8	5/16	¼
r_z, in.	0.679	0.681	0.683	0.685	0.688

ASD	LRFD
$\Omega_c = 1.67$	$\phi_c = 0.90$

[a] For Y-Y axis, welded or pretensioned bolted intermediate connectors must be used.
[b] For required number of intermediate connectors, see the discussion of Table 4-8.
[c] Shape is slender for compression with F_y = 36 ksi.
Note: Heavy line indicates KL/r equal to or greater than 200.

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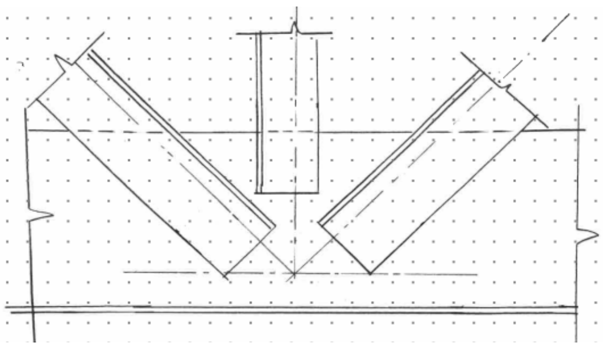
Design of the OMF Truss

Design the typical truss connections:

Must check for limit states of:

- Weld shear rupture (dbl. angle to tee weld)
- Base metal shear rupture (dbl. angle to tee weld)
- Tensile rupture (dbl. angle)
- Whitmore yielding and buckling (tee web)
- Block shear strength (tee web)
- Vertical shear (tee)



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OMF Truss Panel Connection

Connection Force : P_{max}=- 60.2^k

Weld Shear Rupture (Table J2.5)

$$\frac{R_n}{\Omega} = .6F_{exx} * t_{eff} / \ \Omega \qquad \frac{R_n}{\Omega} = .6(70).25 * \frac{.7071}{2} = 3.71 \ ^{k/"}$$

Base Metal Shear Rupture – Tee (J4.2)

$$\frac{R_n}{\Omega} = .6F_u * A_{nw} / \ \Omega \qquad \frac{R_n}{\Omega} = .6(65)(\frac{.48}{2})/2 = 4.68 \ ^{k/"}$$

Base Metal Shear Rupture – Angle (J4.2)

$$\frac{R_n}{\Omega} = .6Fu * A_{nw} / \ \Omega \qquad \frac{R_n}{\Omega} = .6(58)(.3125)/2 = 5.44 \ ^{k/"}$$

L_{req}= 60.2/3.71 = 16.2 " Use (4) 5" long 1/4 *fillet welds*

There's always a solution in steel!

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OMF Truss Panel Connection

Connection Force: P_r = 60.2 kips (+/- Max T&C)

Double angle tensile rupture (d2(b))

$\frac{R_n}{\Omega} = F_u A_n / \Omega$ $\quad A_e = A_n U$ $\quad U = 1 - x/L$

$$U = 1 - \frac{.797}{5} = .804$$

$$\frac{R_n}{\Omega} = (58)(3.9)(.804)/2.00 = 90.9\ kips > 60.2\ kips \text{ OK}$$

There's always a solution in steel!

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OMF Truss Panel Connection

Connection Force : P_{max}=- 60.2^{k} (+/- Max T & C)

Whitmore Yielding (tension)

$$\frac{R_n}{\Omega} = F_y A_w / \Omega \qquad A_w = W_{wh} t_w$$

$$\mathrm{W_{wh}} = \mathrm{L}_{angle} + 2L_{weld} tan(30) = 3.5 + (2)(5)\tan(30)$$

$$W_{wh} = 9.27"$$

$$\frac{R_n}{\Omega} = (50)(9.27 * .48)/1.67 = 133^{\,k} > 60.2^{\mathrm{k}}$$

Whitmore Buckling (Comp.)

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OMF Truss Panel Connection

Whitmore Buckling (Comp.)

$$r_{pl} = \sqrt{\frac{t^2}{12}} = \sqrt{\frac{.48^2}{12}} = .138\text{“}$$

Kl/r=1.5*4/.138=43.5

From table 4-22 $\frac{Fcr}{\Omega}$=26.1 ksi

$\frac{Rn}{\Omega}$=(26.1 ksi)(9.27*.48)=116.1 k > 60.2 k OK

There's always a solution in steel!

OMF Truss Panel Connection

Connection Force: P_r = 60.2 kips (+/- Max T&C)

Block Shear Strength Section J4.3 Equation J4-5

$$R_n = .6F_uA_{nv} + U_{bs}F_uA_{nt} \leq .6F_yA_{gv} + U_{bs}F_uA_{nt}$$

$$\Omega = 2.00$$

Welded connection, therefore $A_{nv}=A_{gv}$

Conservatively $A_{gv}=(.48\ in.)(2x5\ in.)=4.8\ in^2$

$A_{nt}=(.48\ in.)(3.5\ in.)=1.68\ in^2$

$$R_n/\Omega = (.6(50)(4.8) + (1.0)(65)(1.68))/2 = 126.6\ kips > 60.2\ kips\ OK$$

There's always a solution in steel!

OMF Truss Panel Connection

Connection Force: P_{max}=- 60.2^k (+/- Max T & C)

Chord Shear Strength   Chapter G

$V_n = .6F_yA_wC_v$ Ω=1.67   *Section G2*

When $h/t_w \le 1.1\sqrt{kvE/Fy}$ C_v=1.0

C_v=1.51$k_v E/((h/tw)^2 F_y)$

$h/t_w = 19.2 < 1.1\sqrt{\dfrac{5(29000)}{50}} = 59.2$ C_v=1.0

$V_n = .6(50)(.48 * 9.2)1.0 = 132.5\ k$

$\frac{R_n}{\Omega} = 132.5\ ^k/1.67 = 79.3^k > 60.2^k(57/83) = 41.3^k$ OK

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OMF Truss Panel Connection

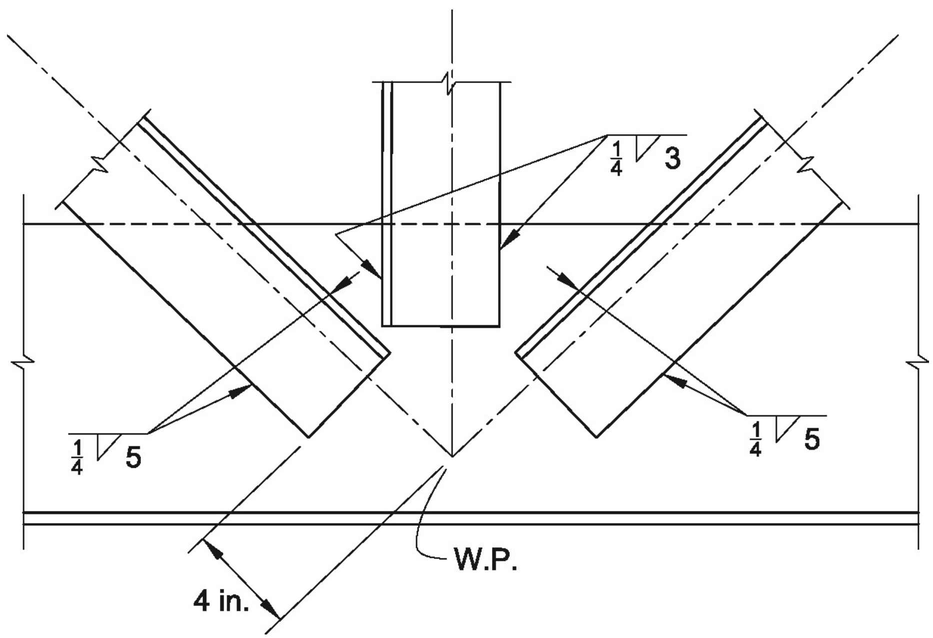
Check shear rupture per J4.2

R_n=.60F_uA_{nv} Ω=2.00

R_n/Ω=.60(65)(.48)(9.2)/2.0=86.1 kips > 41.3 kips ok

There's always a solution in steel!

OMF Truss Panel Connection



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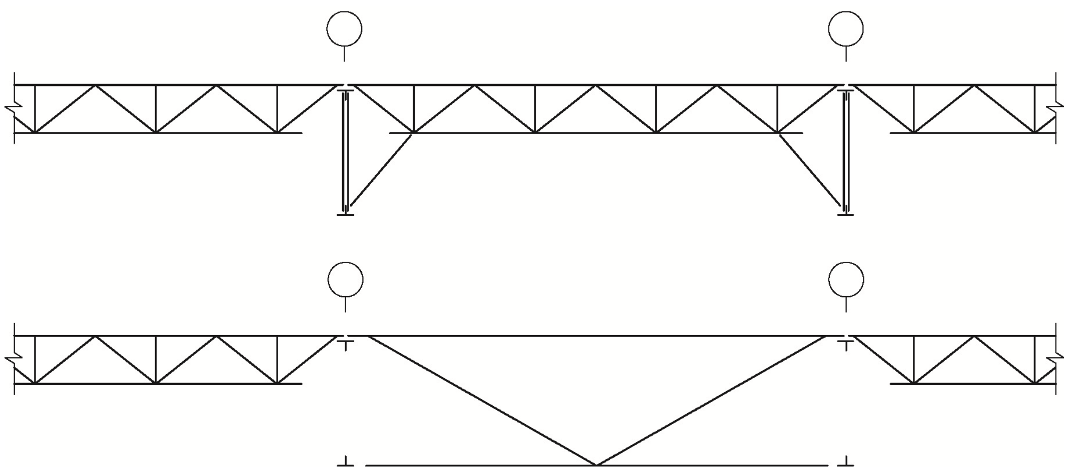
Truss Chord Bracing

2 options:

1. Model the frame including the truss and the chord bracing system into a second order analysis.
2. Design the braces per Appendix 6 Stability Bracing for Columns and Beams



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Design of an Industrial Crane Building

- **Lesson 6**
  - Final Design of the Building Columns
  - Final Design of the Crane Columns
  - Final Design of the Truss
  - Design of the Frame Connections
  - Design of the Anchor Rods

There's always a solution in steel!

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2010 AISC Seismic Provisions Section A4

Section A4 of the Seismic Provisions requires the following information to be on the structural drawings (partial list):

- Designation of the *seismic load resisting system* (SFRS)
- Identification of the members and connections that are a part of the SFRS
- <u>Configuration of the connections</u>
- Connection material specifications and sizes
- Locations of *demand critical welds*
- …

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Design of the OMF Connections

- The design of the OMF connections must meet the AISC 341 Seismic Provisions.
- For Joist Girders, the design procedures can be found in the SJI Technical Digest 11, “Design of Lateral Load Resisting Frames Using Steel Joists and Joist Girders”, November 2007

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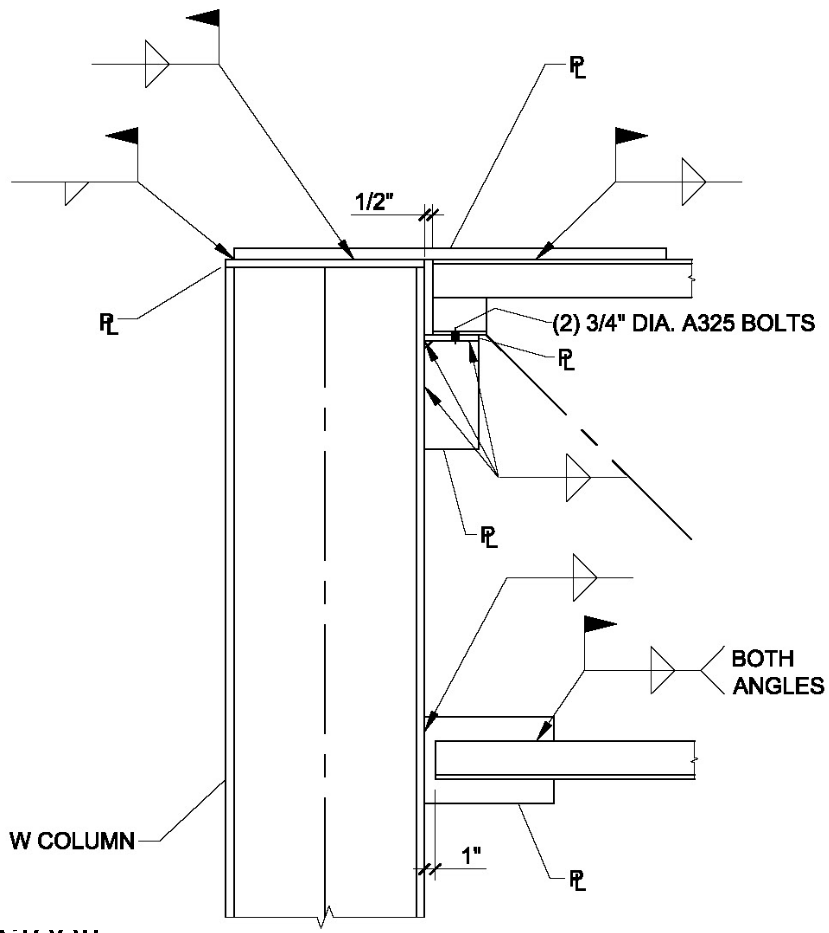
Exterior Moment Connection

This detail provides a direct transfer of the chord forces to the column.

Connection of the truss to the column must be based on developing $1.1R_yM_p$ of the column.

(Same as truss design)



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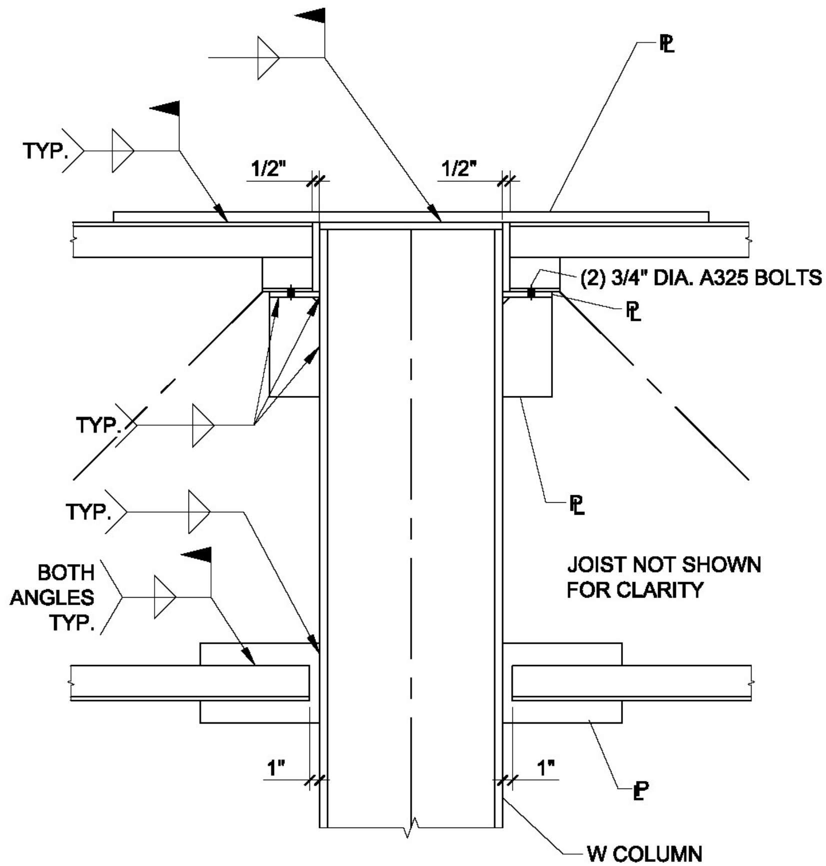
Interior Moment Connection



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OMF Connections

- The top plate and the bottom plate sizes are determined from the maximum chord force (based on $M=1.1R_yM_p$ of column).
- The seat size is determined using Table 10-8, "Bolted/Welded Stiffened Seated Connections" in the AISC Manual

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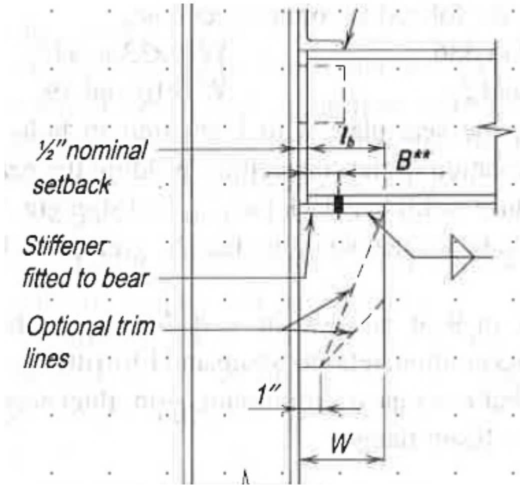
Truss Seat Connection

- Salmon and Johnson (1996) indicates four steps for the design of stiffened seats for beam reactions. These are:
  - Determine the seat width
  - Determine the eccentricity e_s of load
  - Determine the stiffener thickness t_s
  - Determine the angle or plate sizes and arrangement of bolts; or the weld size and length

Truss Seat Connection

- The seat width for beam reactions is based on the required bearing for the beam to prevent local web yielding and web crippling. For the truss same limit states apply to the web of the tee. The vertical reaction is located at the work point of the end diagonal member.



- Based on the limit states of Web Local Yielding (J10.2) and Web Local Crippling (J10.3) a bearing length of 4" is selected.

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Truss Seat Connection

The text by Salmon and Johnson indicates the following limit states for design of stiffened seats.

1. The stiffener thickness, t_s, should be equal to or greater than the thickness, t_w, of the supported beam web. Since the WT web is .48” use a ¾” thick A36 plate.
2. Local buckling of the stiffener must be prevented. Local buckling is prevented provided the stiffener thickness is greater than or equal to w/16 per the 2010 AISC Specification Section J10.8(2). W = width of stiffener.
3. The design bearing strength, R_n, on the contact area of stiffener must satisfy the bearing equation from the 2010 AISC Specification Eqn. J7-1

   ($R_n=1.8F_yA_{pb}$, $\Omega=2.0$, $\varphi=0.75$)

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Truss Seat Connection

- Limit States
  - Eccentric loading on the stiffener and weld
  - Stiffener shear yielding

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Truss Seat Connection

- Eccentric Loading on the stiffener (S&J)

$$t_s = \frac{P(6es - 2W)}{.90FyW^2} = \frac{P(6 * 2.5 - 2 * 4.5)}{.90(36)4.5^2} = .0091P$$

For a ¾" plate: $P_a = .75/.0091 = 82.4\ kips > 43\ kips$ OK

Where, e_s = erection clearance + N/2 or w – N/2.

For A36 plate (F_y =36 ksi):

w = 4 in. +0.5 in. (setback) = 4.5 in

e_s = 4.5 – 4/2 = 2.5 in. $\Omega = 2.0$

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Truss Seat Connection

Stiffener shear yielding:

- $R_n = .6F_y * t_s * L = .6 * 36 * .75 * 12 = 194.4k$
- $R_n / \Omega = 116.4^k > 43^k$

Stiffener to Column Weld:

Refer to manual table 10-8

- For a 12" long seat 5" wide 5/16" weld;
- $R_n / \Omega = 80.2^k$

L = stiffener length, 12 in.
Ω = 1.67

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Truss Seat Connection

Table 10-8
Bolted/Welded Stiffened Seated Connections
Weld Available Strength, kips

L, in.	Width of Seat, W, in.											
	4								5			
	70-ksi Weld Size, in.								70-ksi Weld Size, in.			
	1/4		5/16		3/8		7/16		5/16		3/8	
	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
6	22.7	34.0	28.4	42.5	34.0	51.1	39.7	59.6	23.5	35.2	28.2	42.2
7	29.9	44.9	37.4	56.1	44.9	67.3	52.4	78.6	31.2	46.9	37.5	56.2
8	37.8	56.7	47.2	70.8	56.7	85.0	66.1	99.2	39.8	59.8	47.8	71.7
9	46.1	69.2	57.7	86.5	69.2	104	80.7	121	49.1	73.7	59.0	88.5
10	54.9	82.3	68.6	103	82.3	123	96.0	144	59.0	88.5	70.8	106
11	63.9	95.8	79.8	120	95.8	144	112	168	69.4	104	83.3	125
12	73.1	110	91.4	137	110	165	128	192	80.2	120	96.2	144
13	82.5	124	103	155	124	186	144	217	91.3	137	110	164
14	92.1	138	115	173	138	207	161	242	103	154	123	185
15	102	152	127	191	152	229	178	267	114	171	137	206
16	111	167	139	209	167	250	195	292	126	189	151	227
17	121	181	151	227	181	272	212	318	138	207	165	248
18	131	196	163	245	196	294	229	343	150	225	180	270
19	140	211	175	263	211	316	246	369	162	243	194	291
20	150	225	188	281	225	338	263	394	174	261	209	313
21	160	240	200	300	240	359	280	419	186	279	223	335
22	169	254	212	318	254	381	296	445	198	297	238	357
23	179	269	224	336	269	403	313	470	210	315	252	378
24	189	283	236	354	283	425	330	495	222	334	267	400
25	198	297	248	372	297	446	347	520	235	352	281	422
26	208	312	260	390	312	468	364	546	247	370	296	444
27	217	326	272	408	326	489	380	571	259	388	310	466
Limitations for Connections to Column Webs												
	$B = 2^5/_8$ in. max								$B = 2^5/_8$ in. max			
	W12×40, W14×43 for $L \geq 9$ in. limit weld $\leq 1/4$ in.								None			

Notes:
1. Values shown assume 70-ksi electrodes. For 60-ksi electrodes, multiply tabular values by 0.857, or enter table with 1.17 times the required strength, R_u or R_a. For 80-ksi electrodes, multiply tabular values by 1.14, or enter table with 0.875 times the required strength.
2. Tabulated values are valid for stiffeners with minimum thickness of

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Truss to Column FR Conn,

- Design top plate for axial chord force:
- $\frac{R_n}{\Omega}=\frac{F_y A_g}{\Omega}=\frac{36(1.25*9)}{1.67}=242.5\text{k} > 221\text{k}$
- Design Bottom plate:
- $\frac{R_n}{\Omega}=\frac{F_y A_g}{\Omega}=\frac{36(1.0*12)}{1.67}=258.7^{\text{k}} > 221^{\text{k}}$
- Design the longitudinal fillet welds to the chord:
- Use 5/16 fillets $\frac{r_n}{\Omega}=4.64\ ^{k}/$“ $L_{requ.}=221/4.64=47.6$”
- Use (2) 24” lines of 5/16 fillet welds

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Truss Connection

- Design the transverse fillet welds from the bottom plate to the column flange:
- See J4, Linear wled group, uniform leg size, loaded through the center of gravity.

$$R_n = F_{nw}A_{we} \quad F_{nw} = .60F_{EXX}(1.0 + .50sin^{1.5}\theta)$$

For ½" fillet welds the capacity per inch:

$r_n/\Omega = .60 * 70(1.0 + .50sin^{1.5}90)(.5*.7071)/2.00=11.1$ k/"

For 20" of weld:

$$\frac{r_n}{\Omega} = 222k > 221k\ ok$$

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Truss Connection

- Check Column for Stiffeners:
- Flange Local Bending per J10.1: $\frac{R_n}{\Omega} = 84k < 221k\ ng$
- Web Local Yielding per J10.2: $\frac{R_n}{\Omega} = 149.1k < 221k\ ng$
- Web Local Crippling per J10.3: $\frac{R_n}{\Omega} = 84k < 221k\ ng$
- Web Comp. Buckling per J10.5 : $\frac{R_n}{\Omega} = 90k < 221k\ ng$

Stiffeners are required. See J10.8

- Size flange welds for diff. between required strength and available strength.
- Size web weld transfer stiffener force to the column web.

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Truss Connection

Check Column for Web Panel Zone Shear J10.6 (a)
Panel zone deformation not considered in the analysis:

$P_r \leq .4P_c$ $\quad R_n = .60F_y d_c t_w$ $\quad \Omega = 1.67$

$R_n/\Omega = .6(50)(.52)(29.7)/1.67 = 277 \text{ kips} > 221 \text{ kips OK}$

Note: The 221 kip demand is used for convenience and is conservative, The panel zone shear demand is actually based on the building code load combinations and does not need to achieve $1.1R_yM_p$

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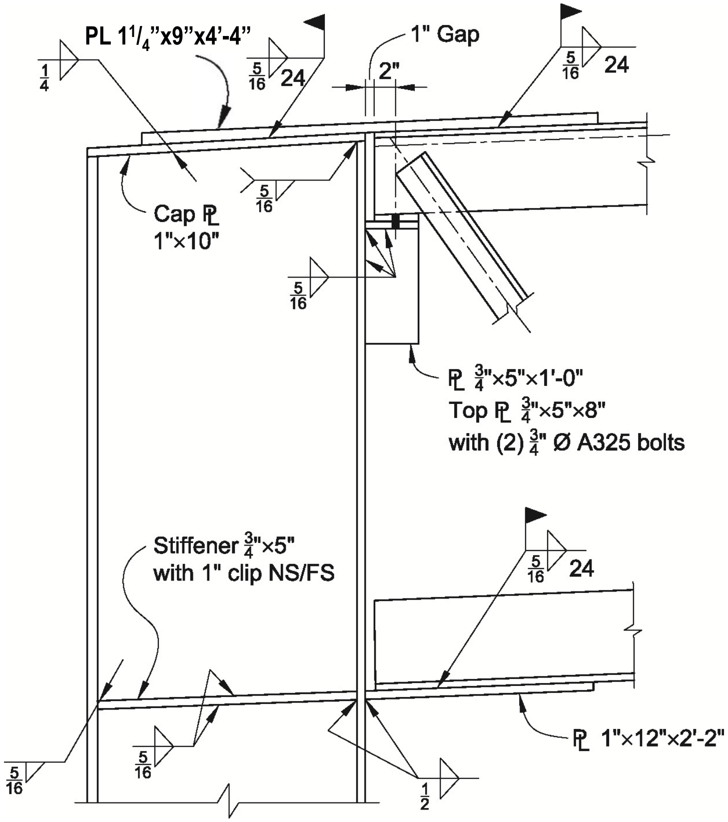
Final Detail at Sidewalls



Additional Design Steps:

1. Provide bearing for joists
2. Review and coordinate with longitudinal bracing

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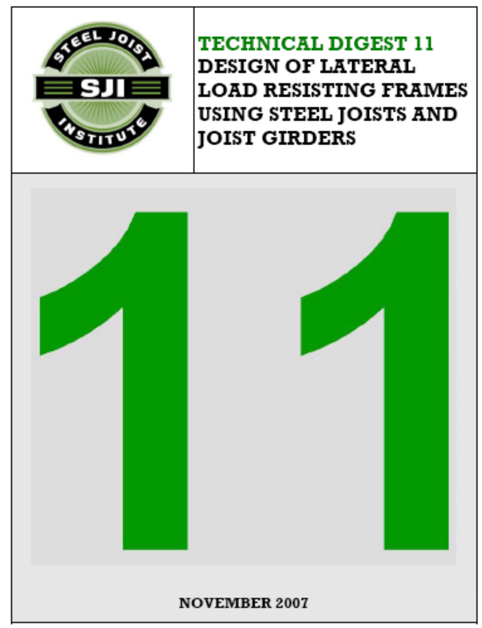
Alternate Joist Girders

As an alternate to the fabricated truss illustrated in this example a joist girder could be specified to act as the truss in the OMF.

SJI has Excel programs available from their website that can be used for the design of the JG to column connection.



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Controlling IBC Load Combinations (ASD)

Mark: G2 **(Note: Left end @ sidewall)**	**Girder Designation:** **60G12NSP**					
LRFD **Load Combination:**	Panel Load (kips)	Left End Moment (kip-ft.)	Right End Moment (kip-ft.)	TC Force (kips)	BC Force (kips)	Remark s
D + S	5.0	73	-487	2		
D + 3/4S + ¾(Crane Lateral)	4.2	-43 120	-359 -515	3		
$(1.0 + 0.14S_{DS})D + M_{pe}/1.5$	2.2	+/-753	-/+703	4		
$[1.0+(3/4)0.14S_{DS}]D+3/4(M_{pe}/1.5)+3/4S$	4.4	+/-565	-/+527	3		
$(0.6 - 0.14S_{DS})D + M_{pe}$	0.9	+/-753	-/+703	4		

M_{pe} in the load combination indicates the AISC OMF requirement, and the SJI requirement of applying $1.1R_yM_p$ to JG ends.

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Controlling IBC Load Combinations (ASD)

Mark: G2 (Note: Right end @ sidewall)	Girder Designation: 60G12NSP					
LRFD Load Combination:	Panel Load (kips)	Left End Moment (kip-ft.)	Right End Moment (kip-ft.)	TC Force (kips)	BC Force (kips)	Remarks
D + S	5.0	487	-73	2		
D + 3/4S + ¾(Crane Lateral)	4.2	359 515	43 -120	3		
$(1.0 + 0.14S_{DS})D + M_{pe}/1.5$	2.2	+/-703	-/+753	4		
$[1.0+(3/4)0.14S_{DS}]D+3/4(M_{pe}/1.5)+3/4S$	4.4	+/-527	-/+565	3		
$(0.6 - 0.14S_{DS})D + M_{pe}$	0.9	+/-703	-/+753	4		

M_{pe} in the load combination indicates the AISC OMF requirement, and the SJI requirement of applying $1.1R_yM_p$ to JG ends.

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Design of an Industrial Crane Building

- **Lesson 6**
  - Final Design of the Building Columns
  - Final Design of the Crane Columns
  - Final Design of the Truss
  - Design of the Frame Connections
  - Design of the Anchor Rods

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Anchor Rod Design

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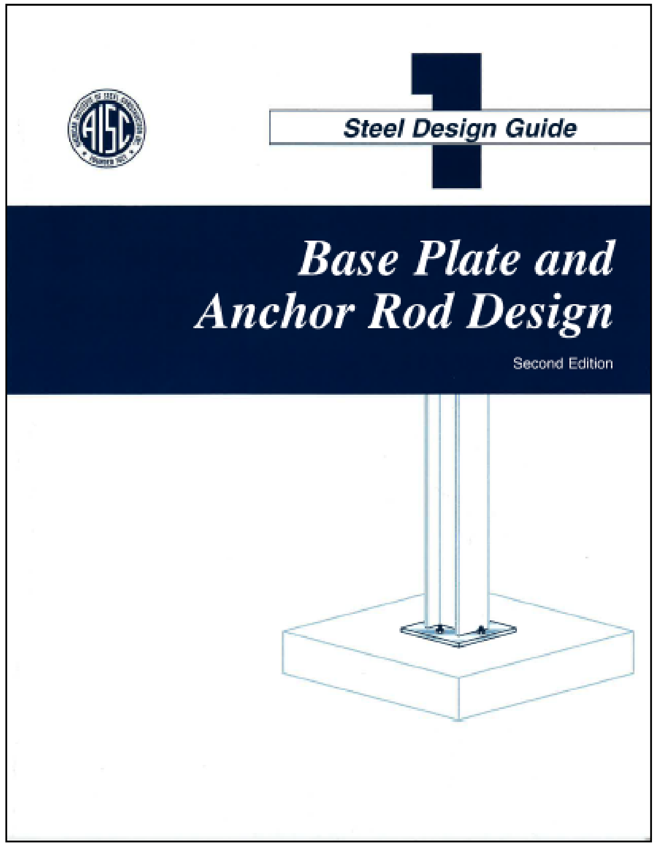
Anchor Rod Design



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Anchor Rod Specifications

ASTM F1554.

Two items of particular interest in 1554 relate to:

- Classification, and
- Product Marking (color coating)

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ASTM 1554 - Classifications

- Anchor rods furnished to the ASTM 1554 Specification can be obtained in three grades which denote three steel yield strengths, they are to be color coated as shown:
- **36 ksi - Blue**
- **55 ksi – Yellow** *
- **105 ksi - Red**

The 36 ksi rods, and the 55 ksi rods, can be obtained in diameters up to 4 in. The 105 ksi rods can be obtained up to 3 in. diameters.

*Supplement S1 for weldable material.

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Anchor Rod Erection Requirements Per OSHA 1926.75

- Minimum of 4 anchor rods
- Designed for a minimum load of 300 lbs at 18-inches eccentric from any column face
- Anchor rods shall not be repaired or replaced or field modified without the approval of SEOR
- Approval must state if repair/modification shall require guying or bracing of the column
- Contractor shall provide written notification to erector of any repair or modification

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Hole Sizes

AISC Anchor Rod Hole Sizes:

The recommended anchor rod hole diameters and minimum washer diameters and thicknesses can be found on page 14-21 of the AISC 14th edition Steel Construction Manual. The sizes are shown below:

Anchor Rod Diameter, in.	Hole Diameter, In.	Min. Washer Diameter, in.
3/4	1- 5/16	1- 7/8
7/8	1- 9/16	2- 1/4
1	1- 13/16	2- 5/8
1- 1/4	2- 1/16	2- 7/8
1- 1/2	2- 5/16	3- 1/8
1- 3/4	2- 3/4	3- 3/4
2	3-1/4	4- 1/2
2- 1/2	3-3/4	5

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Anchor Rod Available Strength, kips

Table 3.1. ASTM F1554 Anchor Rod (rod only) Available Tensile Strength, kips

Rod Diameter, in.	Rod Area, A_b, in.^{2}	LRFD ϕR_n $\phi = 0.75$			ASD R_n/Ω $\Omega = 2.00$		
		Grade 36 kips	Grade 55 kips	Grade 105 kips	Grade 36 kips	Grade 55 kips	Grade 105 kips
⅝	0.307	10.0	12.9	21.6	6.68	8.63	14.4
¾	0.442	14.4	18.6	31.1	9.60	12.4	20.7
⅞	0.601	19.6	25.4	42.3	13.1	16.9	28.2
1	0.785	25.6	33.1	55.2	17.1	22.1	36.8
1⅛	0.994	32.4	41.9	69.9	21.6	28.0	46.6
1¼	1.23	40.0	51.8	86.3	26.7	34.5	57.5
1½	1.77	57.7	74.6	124	38.4	49.7	82.8
1¾	2.41	78.5	102	169	52.3	67.6	113
2	3.14	103	133	221	68.3	88.4	147
2¼	3.98	130	168	280	86.5	112	186
2½	4.91	160	207	345	107	138	230
2¾	5.94	194	251	418	129	167	278
3	7.07	231	298	497	154	199	331
3¼	8.30	271	350	583	180	233	389
3½	9.62	314	406	677	209	271	451
3¾	11.0	360	466	777	240	311	518
4	12.6	410	530	884	273	353	589

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Design of Anchor Rods in Tension:

- Determine the anchor rod tension.
- Select the anchor rod material and the number of anchor rods.
- Determine the base plate size and weld size.
- *Determine the required development length for the anchor rods.*

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AISC 341 REQUIREMENTS

AISC 341 Seismic Provisions, D2.6 Column **Bases**

- D2.6a Required **Axial** Strength – the greater of

  (a)…calculated using the load combinations…including the amplified seismic load

  (b)…required axial strength for column splices (D2.5b)

    (a) …*load combinations*…including the *amplified seismic load* <u>or</u>

    (b) maximum force that can be delivered by the system

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AISC 341 REQUIREMENTS

AISC 341 Seismic Provisions, D2.6 Column **Bases**

- D2.6b Required **Shear** Strength
  - For Columns…required shear strength for column splices(D2.5c) which requires the greater of

    (a) M_{pc}/h (LRFD) or $M_{pc}/(1.5h)$ (ASD)

    (b)AISC 360 requirements and …calculated using the *load combinations*…including the *amplified seismic load*

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AISC 341 REQUIREMENTS

AISC 341 Seismic Provisions, D2.6 Column **Bases**

- D2.6c Required **Flexural** Strength For Columns the lesser of

  (a)$1.1R_yF_yZ$ (LRFD) $(1.1/1.5)R_yF_yZ$ (ASD)

  or

  (b)…moment calculated using the load combinations…including the amplified seismic load

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AISC 341 REQUIREMENTS

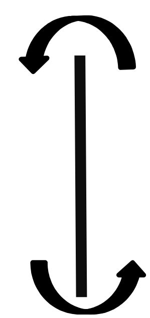
AISC 341 Seismic Provisions, D2.6 Column **Bases**

Based on these rules, we calculate (for the critical load combination):

P_r = 48 k (Ω load combination)

M_r = 1006 k-ft (Ω load combination)

V_r = 49 k (column flexure)



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Large Moment Base Plate Design

Refer to AISC Design Guide 1
Base Plate and Anchor Rod Design
Second Edition

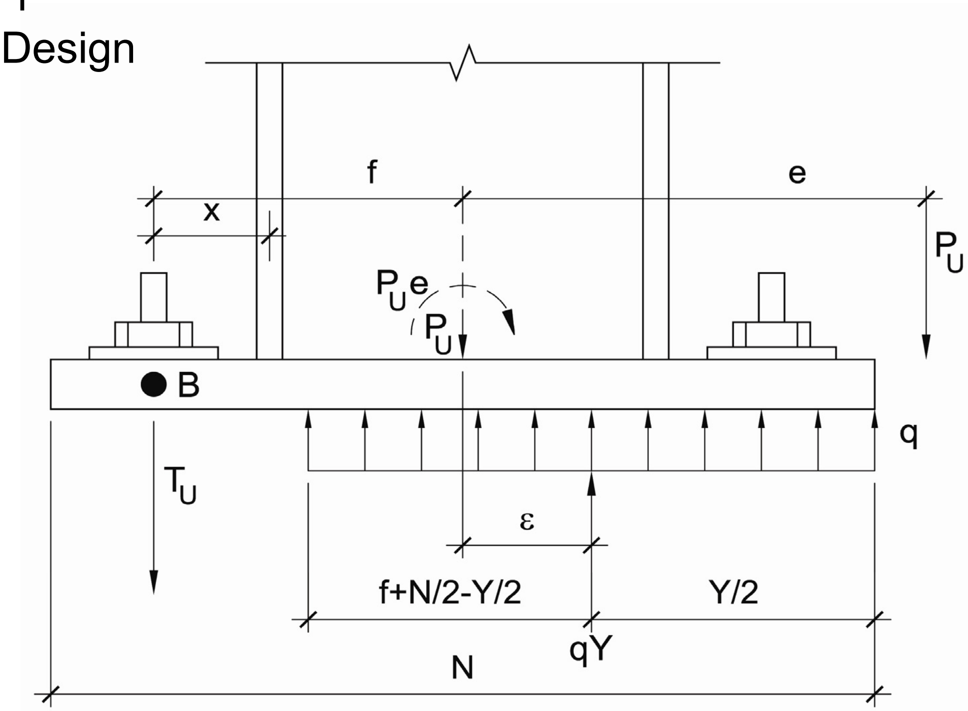

Fig. 3.4.1 Base Plate with Large Moment

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Anchor Rod Tension

For the W24x146: Using amplified forces for axial and the shear force based on hinging the column

P_r = 48.0 kips, M_r = 1006 kip-ft, V_r=49 kips

Try a base plate where N = 40 in. and B = 24 in.

f'_c = 4 ksi, F_y of the base plate = 36 ksi, Ω_c =2.31 (J8)

e = M_r/P_r = (1006 kip-ft)(12)/48 kips = **251.5 in.**

$$f_p(max) = \frac{.85f'_c}{\Omega_c}\sqrt{\frac{A_2}{A_1}} \leq 1.7f'_c = \frac{.85(4\ ksi)}{2.31}(2) = 2.94\text{ ksi}$$

$$q_{\text{max}} = (2.94\text{ ksi})(\text{B}) = (2.94)(24\text{ in.}) = 70.65\text{ kips/in.}$$

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Anchor Rod Tension

Determine from Design Guide 1 equations if the base plate is considered a large moment base plate. If:

$$e > e_{crit} = \frac{N}{2} - \frac{P_a}{2q_{max}} = \frac{40\ in.}{2} - \frac{48\ k}{2(70.65k/")} = 19.66\ \text{in.}$$

$e > e_{crit}$ 251.5 in. > 17.66 in.: Large moment base plate.

where:

e = the eccentricity of load, in.

N = the base plate length, in.

P_r = the required axial force in the column, kips

q_{max} = the maximum stress on the concrete

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Anchor Rod Tension

Check the inequality:

$$\frac{2P_a(e+f)}{q_{max}} < \left(f + \frac{N}{2}\right)^2 \quad or\ a\ larger\ base\ plate\ is\ required$$

$$\frac{2(48)(251.5+16)}{70.65} = 363.5 < \left(16 + \frac{40}{2}\right)^2 = 1296$$

OK, Base Plate Size is adequate to proceed.

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Anchor Rod Tension

Y= Length of the compression block

$$Y = (f + \frac{N}{2}) \pm \sqrt{(f + \frac{N}{2})^2 - \frac{2P_a(e + f)}{q_{max}}}$$

$$Y = (16 + \frac{40}{2}) \pm \sqrt{(16 + \frac{40}{2})^2 - \frac{2 * 48(251.5 + 16)}{70.65}}$$

$$Y = 5.46''$$

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Anchor Rod Tension

Bolt tension ($\Sigma f_{vert}=0$)

$T=q_{max}Y-P_a=(70.65)(5.46)-48=338$ kips

$T_{bolt}=84.4$ kips

Select (4) 2 1/2 in. dia. 36 ksi rods

$R_n/\Omega=107$ kips / bolt

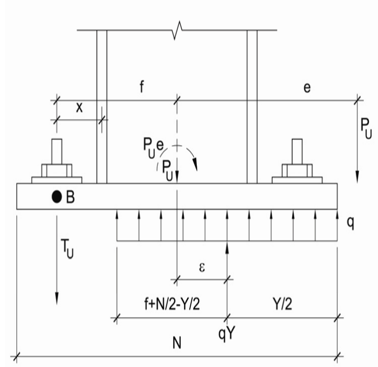

Fig. 3.4.1 Base Plate with Large Moment

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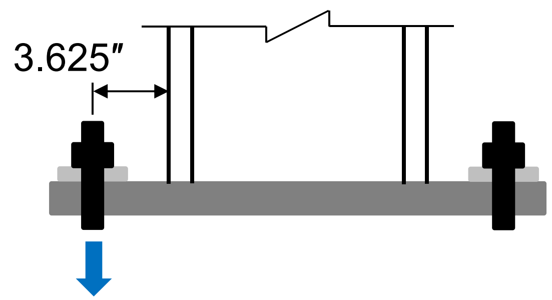
Base Plate Thickness

Washer size for 2-1/2 in. rod = 5 1/2 in. x 7/8 in.
Hole size = 3 3/4 in.
Check plate length beyond flange:
Washer/2 + edge distance + tolerance:
2.75 in. + 0.5 in. + 0.5 = 3.75 in.
Min. Plate length ≈ (2)16 in + (2)(3.75 in.) =39.5 in.
base plate 40 in. x 24 in. OK!

Based on current configuration
Clearance for bolts



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Base Plate Thickness

Lever arm to flange = 3.625 in.

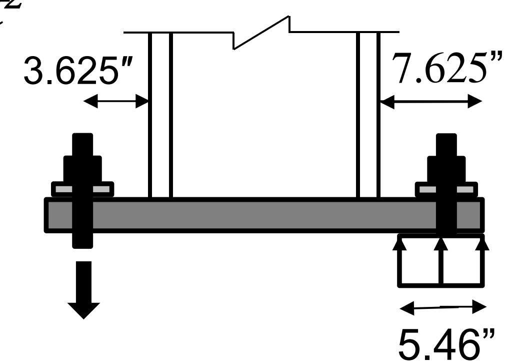
M_t = (338 kips)(3.625 in.) = 1225 kip-in.

M_c=(5.46")(70.65 k/")(7.625-5.46/2)=1888"$^{-k}$

Plate plastic modulus, $Z = Bt^2/4 = 24t^2/4 = 6t^2$

Plate strength $= \dfrac{F_y Z}{\Omega} = \dfrac{(36)(6t^2)}{1.67} = 129.34t^2$

$t = \sqrt{\dfrac{1888}{129.34}} = 3.82"$ Use 4" thick base pl.



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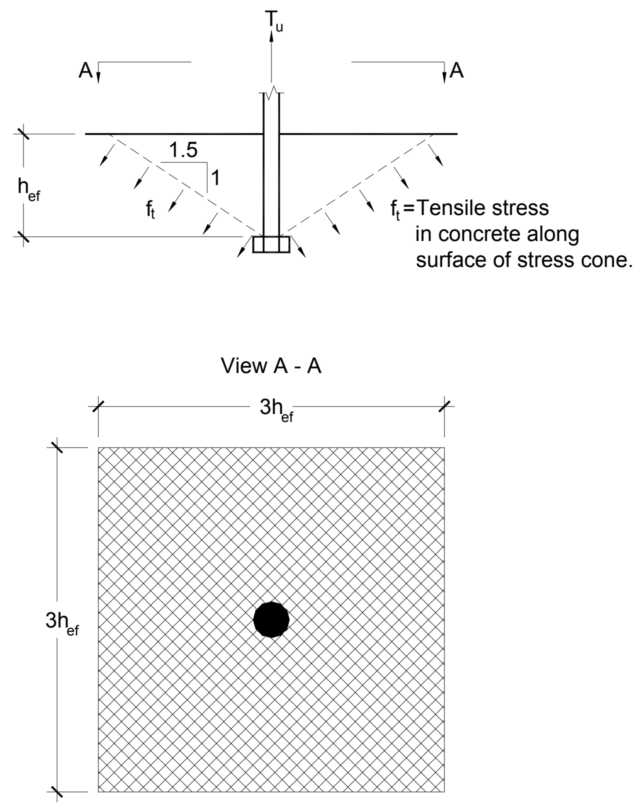
Anchor Rods- Shear

- See AISC Design Guide 1 for suggestions and design procedures to transfer the shear load.
  - Bearing
  - Shear Lugs
  - Shear in Anchor Rods.

Anchor Rod Development

- Refer to ACI 318- 14.



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End of Lesson 6

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- You will receive an email on how to report attendance from: registration@aisc.org.
- Be on the lookout: Check your spam filter! Check your junk folder!
- Completely fill out online form. Don't forget to check the boxes next to each attendee's name!

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Individual Webinar Registrants

PDH Certificates

Within 2 business days…

- New reporting site (URL will be provided in the forthcoming email).
- Username: Same as AISC website username.
- Password: Same as AISC website password.

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8-Session Registrants

PDH Certificates

One certificate will be issued at the conclusion of all 8 sessions.

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8-Session Registrants

QUIZZES

Access to the quiz: Information for accessing the quiz will be emailed to you by Wednesday. It will contain a link to access the quiz. EMAIL COMES FROM NIGHTSCHOOL@AISC.ORG

Quiz and Attendance records: Posted Tuesday mornings. www.aisc.org/nightschool - scroll down to Quiz and Attendance Records.

Reasons for quiz:

EEU – must take all quizzes and final to receive EEU
PDHS – If you watch a recorded session you must take quiz for PDHs.
REINFORCEMENT – Reinforce what you learned tonight. Get more out of the course.

NOTE: If you attend the live presentation, you do not have to take the quizzes to receive PDHs.

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8-Session Registrants

RECORDINGS

Access to the recording: Information for accessing the recording will be emailed to you by this Wednesday. The recording will be available for two weeks. For 8-session registrants only. EMAIL COMES FROM NIGHTSCHOOL@AISC.ORG.

PDHS – If you watch a recorded session you must take AND PASS the quiz for PDHs.

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Night School Resources for 8-session package Registrants

Find all your handouts, quizzes and quiz scores, recording access, and attendance information all in one place!

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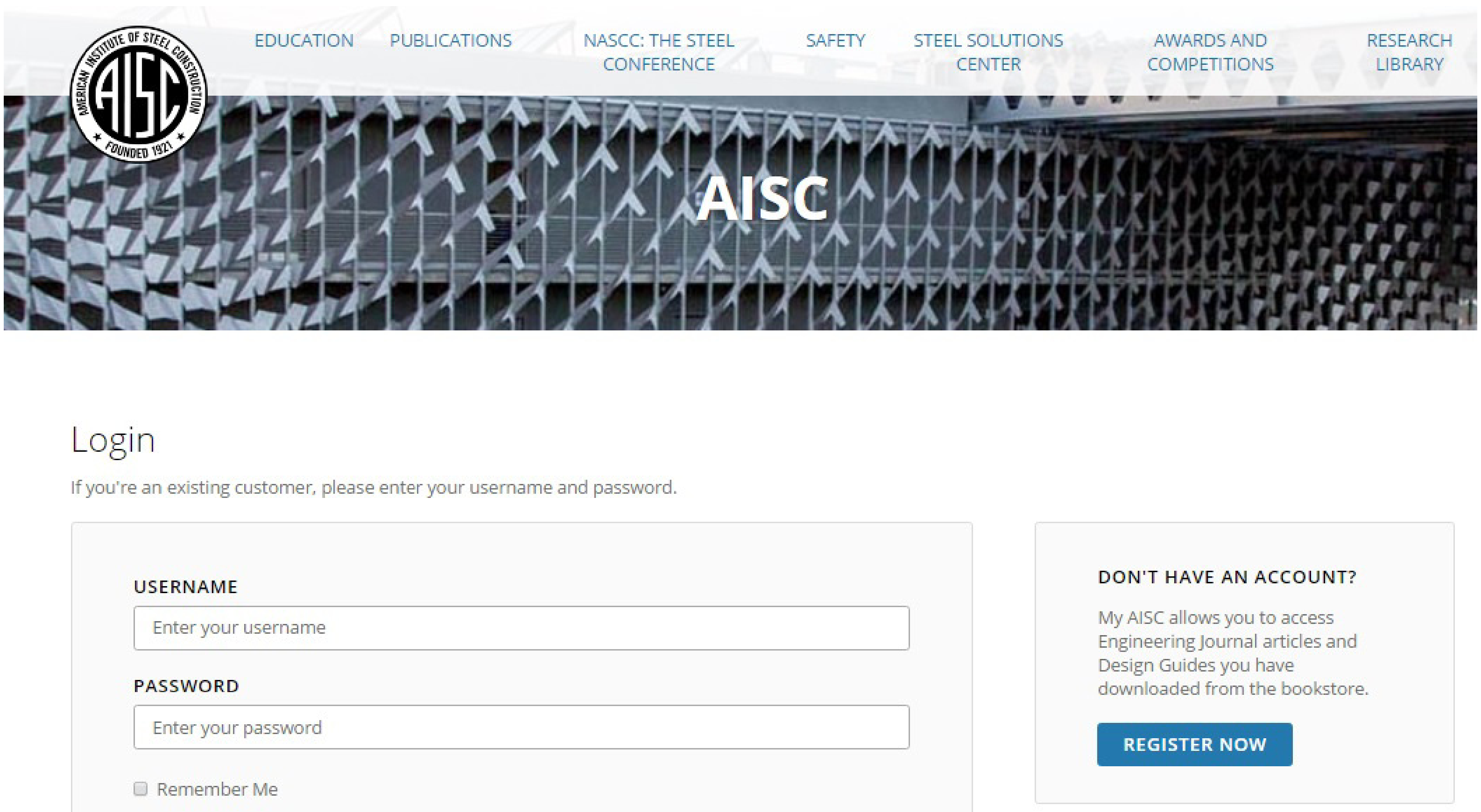
Night School Resources for 8-session package Registrants

Go to www.aisc.org and sign in.



Night School Resources for 8-session package Registrants

IN THIS SECTION

- Edit Profile
- My Downloads
- My Pending Quizzes
- My Events
- Order History
- Course History
- Night School Resources

MyAISC

MY PROFILE

Update your contact and address information.

EDIT PROFILE

MY PURCHASED DOWNLOADS

Access articles and documents that you have purchased.

MY ORDER HISTORY

View your past orders.

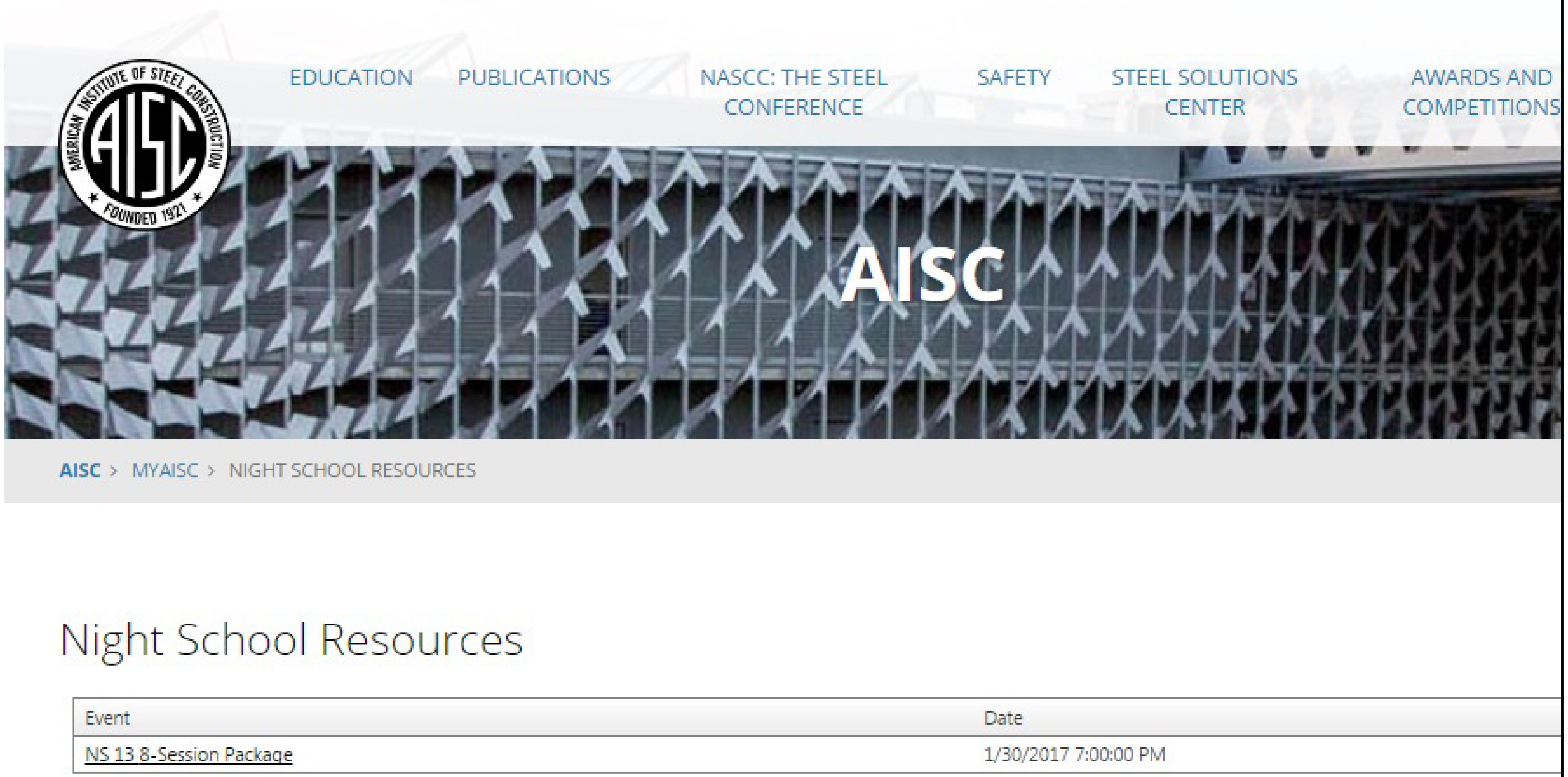
VIEW ORDERS

MY NIGHT SCHOOL RESOURCES

View online resources for Night School courses, available for 8-Session Package registrants. See www.aisc.org/nightschool f information on Night School including registration.

VIEW RESOURCES

Night School Resources for 8-session package Registrants



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Night School Resources for 8-session package Registrants

EDUCATION PUBLICATIONS NASCC: THE STEEL CONFERENCE SAFETY STEEL SOLUTIONS CENTER AWARDS AND COMPETITIONS RESEARCH LIBRARY

AISC > MYAISC > NIGHT SCHOOL RESOURCES > NS13 8-SESSION PACKAGE RESOURCES

Night School 13: Design of Industrial Buildings

8-SESSION PACKAGE RESOURCES

Event	Date	Handouts	Video	Quiz	Attendance
NS13 - Design Criteria	1/30/2017 7:00:00 PM	Handouts	View Passcode: NS13DSN	Pass Score: 80	Pending
NS13 - Economic Considerations	2/6/2017 7:00:00 PM	Handouts	Available 02/08/2017 5pm EST	Available 02/08/2017 5pm EST	Pending
NS13 - Lateral Load Systems and Details	2/13/2017 7:00:00 PM	Handouts	Available 02/15/2017 5pm EST	Available 02/15/2017 5pm EST	Pending
NS13 - Preliminary Design Procedures	2/27/2017 7:00:00 PM	Handouts	Available 03/01/2017 5pm EST	Available 03/01/2017 5pm EST	Pending
NS13 - Crane Girder Design and Frame Analysis	3/6/2017 7:00:00 PM	Handouts	Available 03/08/2017 5pm EST	Available 03/08/2017 5pm EST	Pending
NS13 - Frame Member and Connection Design	3/13/2017 7:00:00 PM	Handouts	Available 03/15/2017 5pm EST	Available 03/15/2017 5pm EST	Pending
NS13 - Transfer Crane Girder & Longitudinal Bldg Bracing Dsn	3/27/2017 7:00:00 PM	Handouts	Available 03/29/2017 5pm EST	Available 03/29/2017 5pm EST	Pending
NS13 - Building Envelope and Bracing Design	4/3/2017 7:00:00 PM	Handouts	Available 04/05/2017 5pm EST	Available 04/05/2017 5pm EST	Pending
NS13 - Final Exam	4/10/2017 7:00:00 PM			Available 04/12/2017 5pm EST	

Night School Resources for 8-session package Registrants

- Weekly “quiz and recording” email.
- Weekly updates of the master Quiz and Attendance record found at www.aisc.org/nightschool. Scroll down to Quiz and Attendance records.
    - Updated on Tuesday mornings.

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Night School Resources for 8-session package Registrants

- Webinar connection information:
  - Found in your registration confirmation/receipt.
  - Reminder email sent out Monday mornings.
- Link to handouts also found here.

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There's always a solution in steel.

Thank You

Please give us your feedback!
Survey at conclusion of webinar.

structural
STEEL