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## Course Description

### **Session 3: Seismic Design of Braced Frames** **March 5, 2018**

This live webinar includes presentation of braced-frame configurations, discussion of behavior of braced frames in earthquakes and in testing and detailed treatment of brace behavior in tension and compression. The session provides an overview of configuration-related issues and discussion of the behavior of beam-column-gusset connection assemblies at large drifts and related design approaches. Lastly, treatment of design issues for gusset plates and connection analysis are presented.





## Learning Objectives

- Compare the various braced-frame configurations.
- Describe the behavior of brace members in both tension and compression.
- Describe the behavior of beam-column-gusset connection assemblies that ensure inelastic drift capacity.
- Describe the behavior of a BRBF and how it differs from an SCBF.



There's always a solution in steel.

# Seismic Design in Steel: Concepts and Examples

Session 3: Seismic Design of Braced Frames  
March 5, 2018



Rafael Sabelli, SE



## Course objectives

- Understand the principles of seismic design of steel structures.
- Understand the application of those principles to two common systems:
  - Special Moment Frames
  - Buckling-Restrained Braced Frames.
- Understand the application of design requirements for those systems.



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## Resources

- *AISC Seismic Design Manual*
- *Ductile Design of Steel Structures*, Bruneau, Uang, and Sabelli, McGraw Hill.
- *Earthquakes and Seismic Design*, Facts for Steel Buildings #3. Ronald O. Hamburger, AISC.
- Other publications suggested in each session



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## Other resources

- AISC Solutions Center
  - 866.ASK.AISC (866-275-2472)
  - Solutions@AISC.org
- AISC Night School
  - Nightschool@AISC.org



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## Course outline

### **Part I: Concepts**

1. Introduction to effective seismic design
2. Seismic design of moment frames
3. **Seismic design of braced frames**
4. Seismic design of buildings



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## Course outline

### **Part II: Application**

- 5.Planning the seismic design
- 6.Building analysis and diaphragm design
- 7.Design of the moment frames
- 8.Design of the braced frames



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## **Session 3: Seismic design of braced frames**



## Session topics

- Braced-frame systems
- Special Concentrically Braced Frames
- Buckling Restrained Braced Frames
- Gusset connections
- Additional topics (time permitting)



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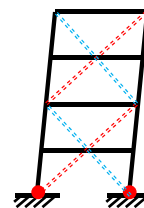
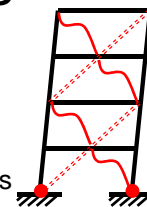
## Braced-frame systems

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## Braced frame systems

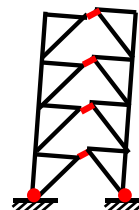
- Concentrically braced frames
  - Special Concentrically Braced Frames
    - Inelastic drift through buckling & yielding of braces
  - Ordinary Concentrically Braced Frames
    - Limit inelastic drift demand through strength
    - Not covered in this course
  - Buckling Restrained Braced Frames
    - Inelastic drift through yielding of brace cores



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## Braced frame systems

- Eccentrically braced frames
  - Inelastic drift from yielding of link beam
  - Not covered in this course



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## Special Concentrically Braced Frames



## SCBF

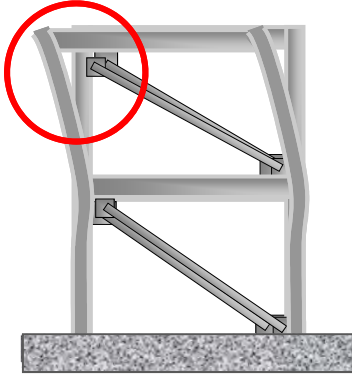
- Inelastic drift through brace axial ductility
  - Tension yield
  - Compression buckling
- Braces sized for compression
  - High overstrength due to tension capacity
- Frame resistance due mostly to brace tension strength
- Braces must survive buckling and maintain tension strength
- Frame members designed for maximum brace forces
  - Prevents unfavorable modes of behavior



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# Post-Elastic Behavior

Unfavorable Modes: Connection Fracture

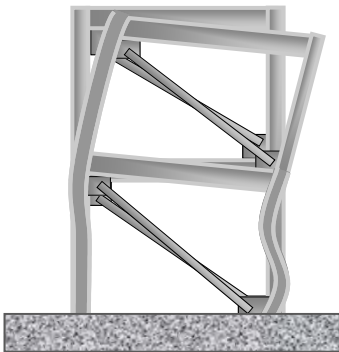


Connection fracture must not be the governing limit state.



# Post-Elastic Behavior

Unfavorable Modes: Column Buckling

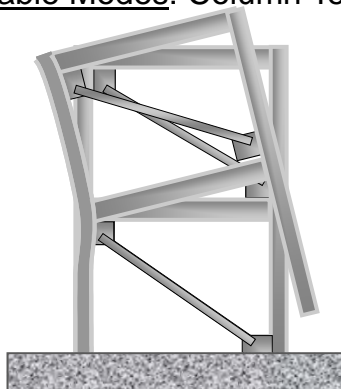


Column buckling must not be the governing limit state.



## Post-Elastic Behavior

### Unfavorable Modes: Column Tension Fracture



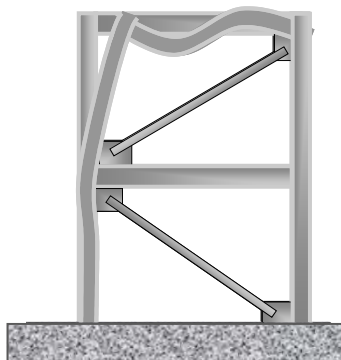
Column tension fracture must not be the governing limit state.



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## Post-Elastic Behavior

### Unfavorable Modes: Beam Failure



Beam failure must not be the governing limit state.

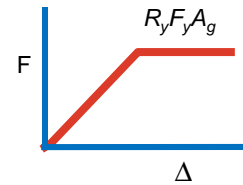
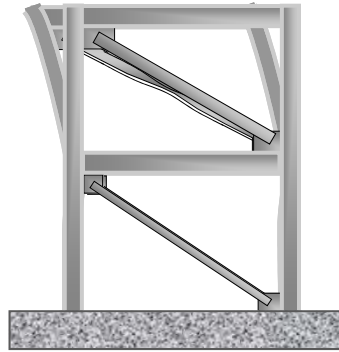


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## Post-Elastic Behavior

### Preferred Modes: Brace Tension Yielding

Brace yielding should be a governing limit state.



Consider maximum effects due to brace force ( $R_y F_y A_g$ )



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## Brace Elongation (Tension Only)



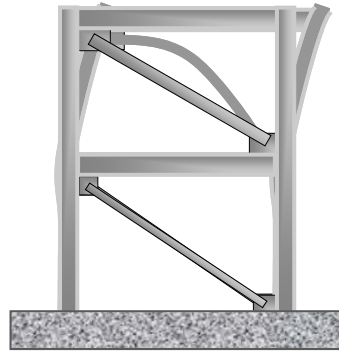
Courtesy of R. Tremblay



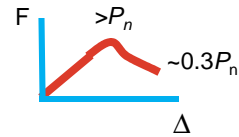
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## Post-Elastic Behavior

### Preferred Modes: Brace Buckling (SCBF)



Brace buckling should be a governing limit state.



Consider maximum effects due to brace force (sometimes  $P \sim R_y P_n$ , sometimes  $P \sim 0.3P_n$ )



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## Brace Buckling



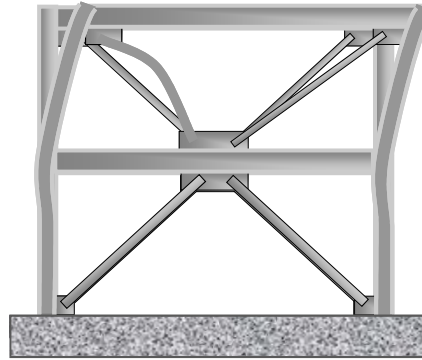
Courtesy of S. Mahin  
U.C. Berkeley, 2004



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## System Behavior with Brace Yielding

### Column Flexure



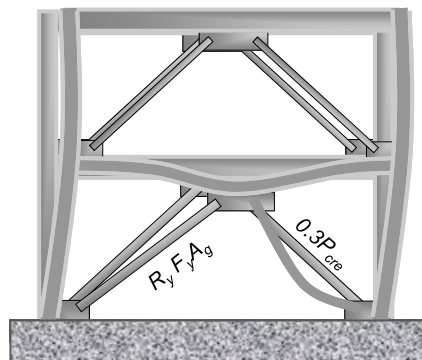
Columns must bend when braces buckle and yield.



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## System Behavior with Brace Yielding

### Beam Flexure



Brace buckling and yielding induce flexural forces in beams in this configuration.



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There's always a solution in steel.

## Design of SCBF



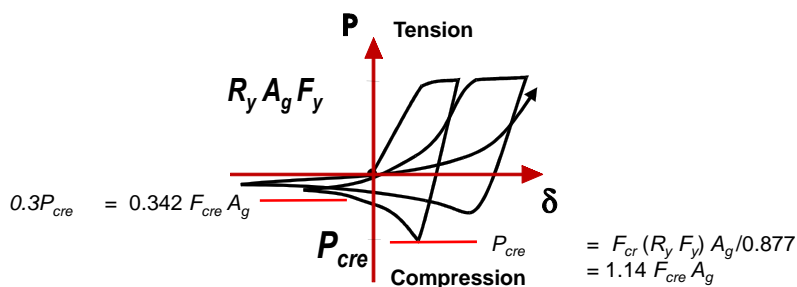
## Design of SCBF

- Force-based design
  - Design for basic load combinations
  - Size braces
- Design beams and columns for maximum forces from braces
  - Consider expected strength
  - Consider buckling behavior
  - Plastic mechanism analysis



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## Brace cyclic behavior (SCBF)



Brace behavior is asymmetric with respect to tension and compression and is subject to strength and stiffness degradation



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## Design of SCBF braces

- Limits
  - Compactness limits
  - Slenderness limits
- Pick/determine plane of buckling
  - End fixity in each plane
  - Brace shape ( $Kl/r$  in each axis)
- Accommodate buckling in plane of buckling
- Provide fixity in orthogonal plane

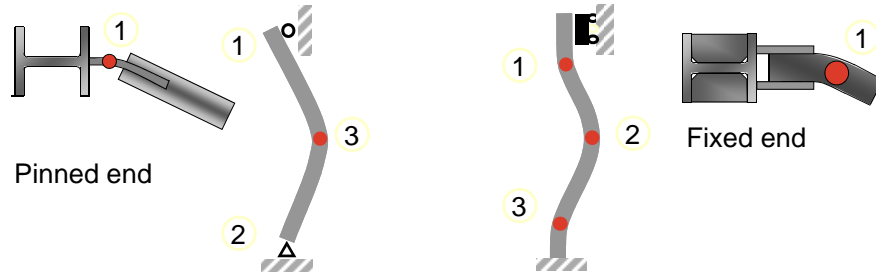


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## Brace Buckling

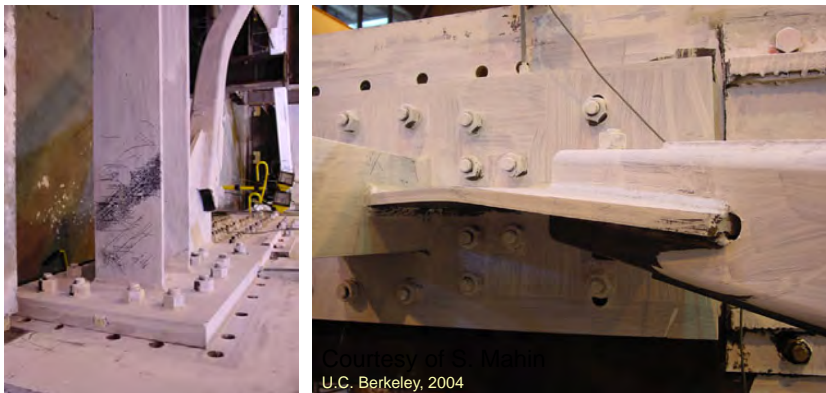
### Flexural buckling (Compression)

Buckling: 3 hinges



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## Pinned-End Gusset Hinging

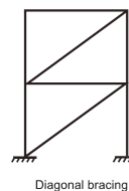


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## Configuration

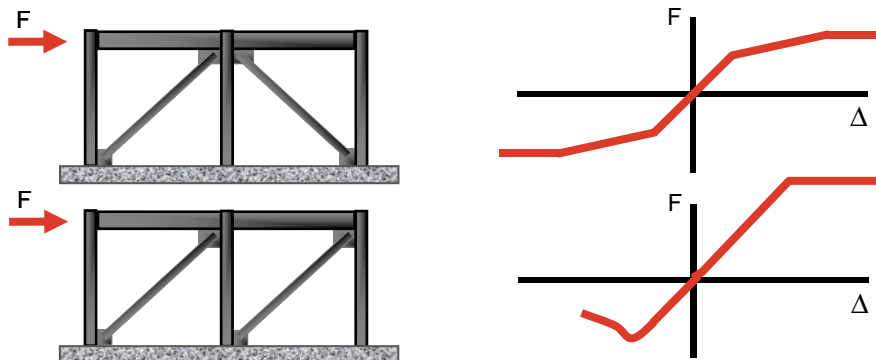
- Single diagonal
  - Unequal response in opposite directions
  - Use in pairs
  - AISC allows single diagonals
    - Design braces for  $\Omega_o E$



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## Bracing Members: Limitations

### Lateral force distribution



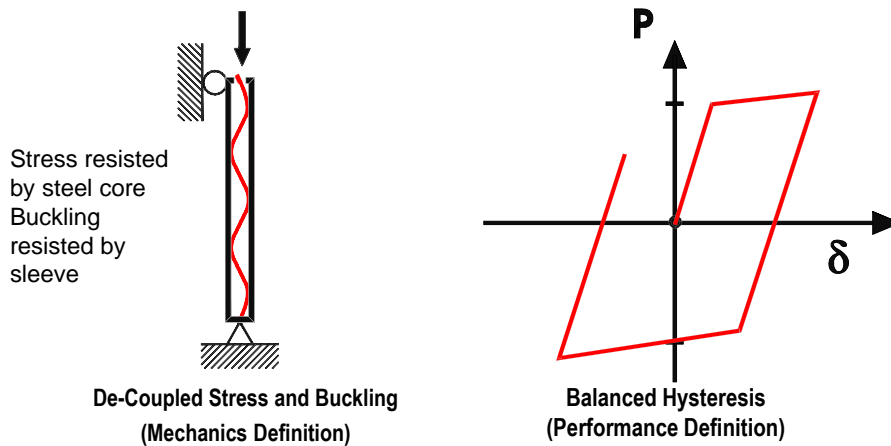
40

There's always a solution in steel.

## Buckling Restrained Braced Frames

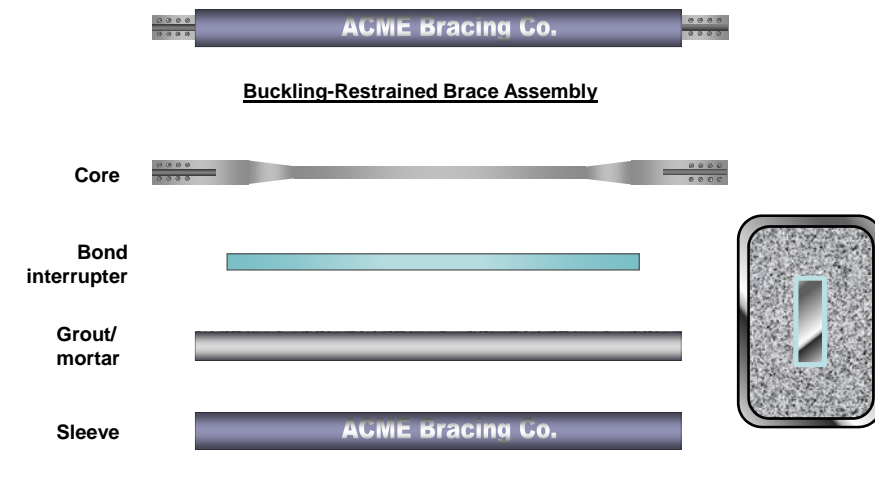


### What is a Buckling-restrained Brace? Two Definitions



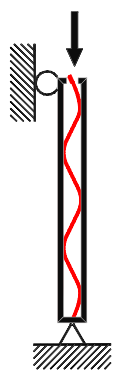
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## Buckling Restrained Braces



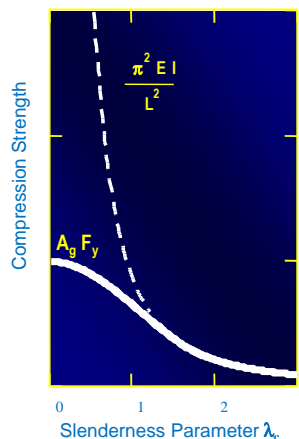
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## BRB Definitions Explained: Sleeved Column



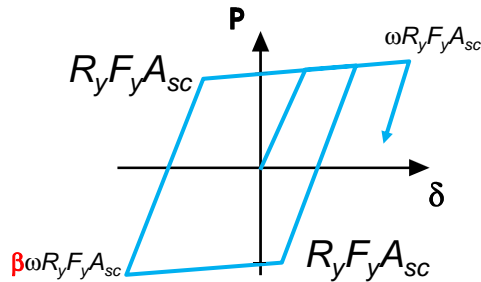
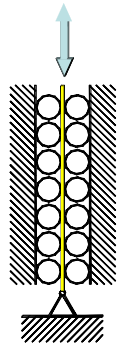
Steel core achieves  $F_y$   
 $kl/r \sim 0$

- Sleeve achieves  $\pi^2 EI/L^2$ 
  - Stress is zero
  - No material stress limit



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## Buckling Restrained Braces

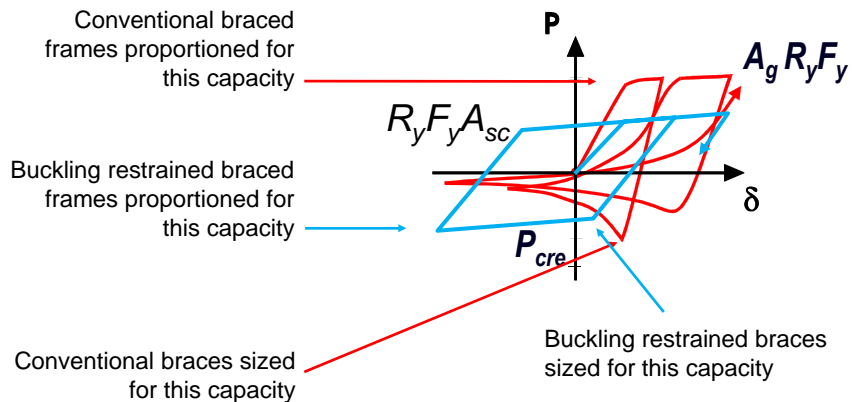


- Balanced Hysteresis
  - Slightly Stronger in Compression ( $\beta$ )
- Hysteretic Energy Dissipation
- Hysteretic Stability
  - Strength
  - Stiffness
- Long Fracture Life



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## Capacity design

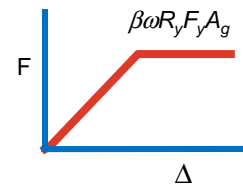
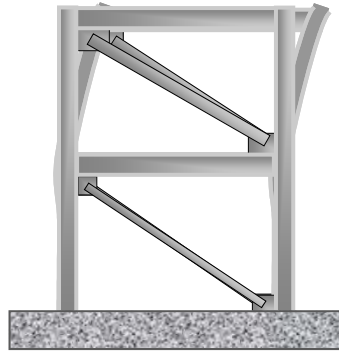


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## Post-Elastic Behavior

### Preferred Modes: Brace Compression Yielding (BRBF)

Brace yielding should be a governing limit state.



Consider maximum effects due to brace force ( $\beta\omega R_y F_y A_g$ )



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## Buckling-Restrained Brace Types



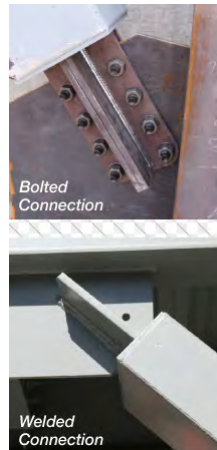
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# Buckling-Restrained Brace Types



Direct bolting of core

Courtesy of  
CoreBrace



Bolted  
Connection

Welded  
Connection

Courtesy of  
STAR Seismic



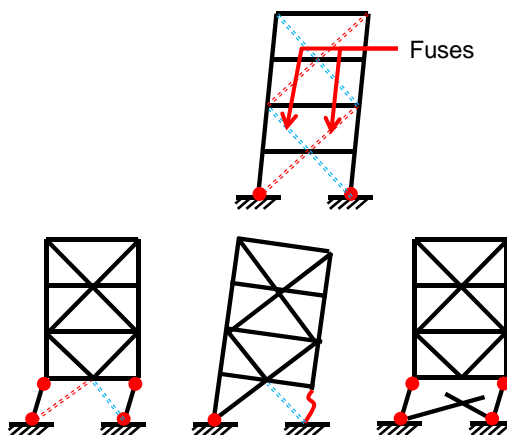
There's always a solution in steel.

## Design of Buckling Restrained Braced Frames



## Design of Buckling Restrained Braced Frames

- Encourage
  - Yielding of braces
- Avoid
  - Flexural hinging in columns (story mechanisms)
  - Buckling of beams or columns
  - Connection failure



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## Fuse concept

- Select appropriate fuses
  - BRBs!
- Size fuses to
  - Provide adequate strength
  - Control drift
- Consider maximum fuse capacity as load on other members
  - Capacity design
  - Precludes undesirable mechanisms

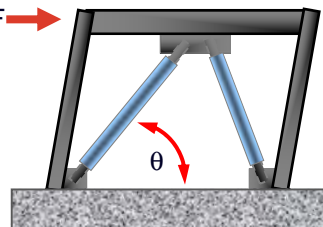


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## Force-based design

$$P_u = \frac{F}{2 \cos \theta}$$

- Assume braces resist 100% of story shear  $F$



$$A_{sc} = \frac{P_u}{\phi F_y}$$

Design braces precisely to calculated capacity  
 ( $P_u = \phi P_n = \phi F_y A_{sc}$ )

Do not include gravity load



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## Brace demands on frame

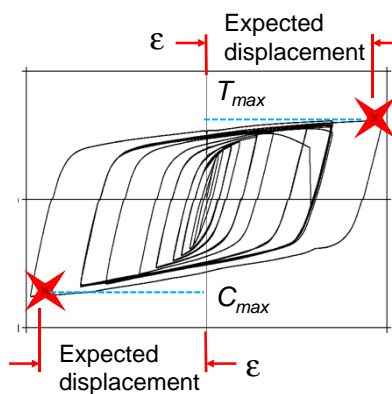
- Estimate fuse capacity
  - Expected material strength
  - Strain hardening
- Based on testing

Calculate deformation

$$\Delta_{bm} = \Delta \cos(\theta)$$

$$\Delta = 2\% h$$

$$\epsilon = \Delta_{bm} / L_y$$



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## Brace demands on frame

- Based on testing

$$\omega = T_{max} / A_g F_y$$

Typical  $1.3 \leq \omega \leq 1.5$

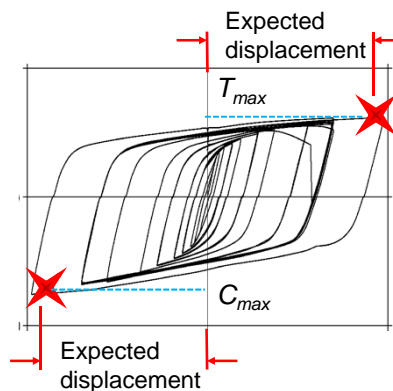
$$\beta\omega = C_{max} / A_g F_y$$

Typical  $1.1 \leq \beta \leq 1.25$

- For design

$$R_u(\text{tension}) = \omega A_g R_y F_y$$

$$R_u(\text{compression}) = \beta\omega A_g R_y F_y$$



AISC 341 F4.3

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## Analysis: brace stiffness

- Braces are non-prismatic
  - Stiffness depends on
    - Core area (proportional to strength)
    - Length of yielding core
      - Connection length required
        - Varies with brace type
        - Varies with brace strength
      - Varies with configuration
        - Shorter for chevron than for single-diagonal




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### Analysis: brace stiffness


$\epsilon \sim (\delta_{br} / L_{wp}) (L_{wp} / L_y)$

$K \sim EA_{sc} / L_y$   
 $= K_F EA_{sc} / L_{wp}$   
 $1.2 \leq K_F \leq 1.8$

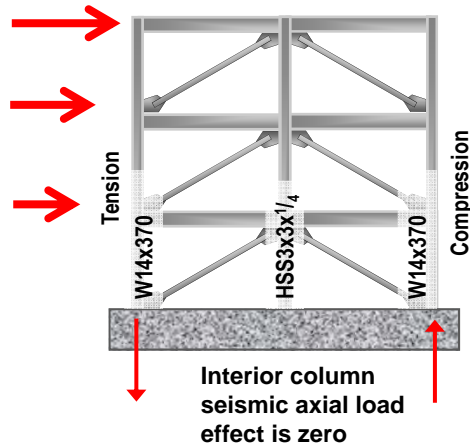

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There's always a solution in steel.

## Plastic mechanism analysis

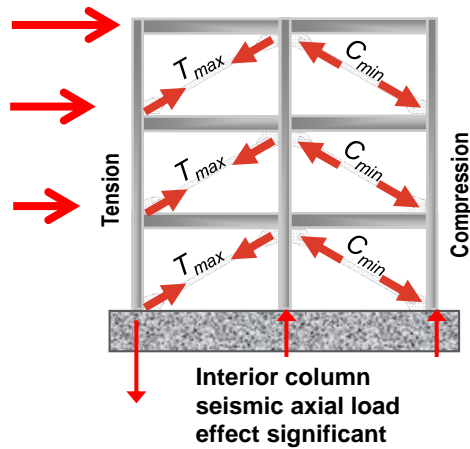


## What elastic analysis misses

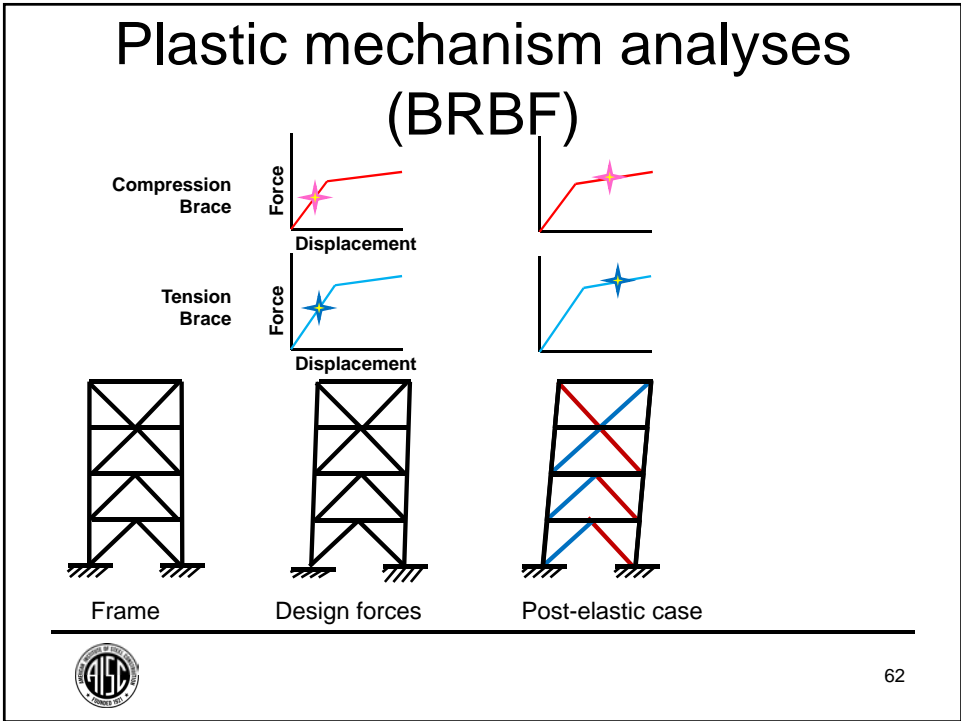
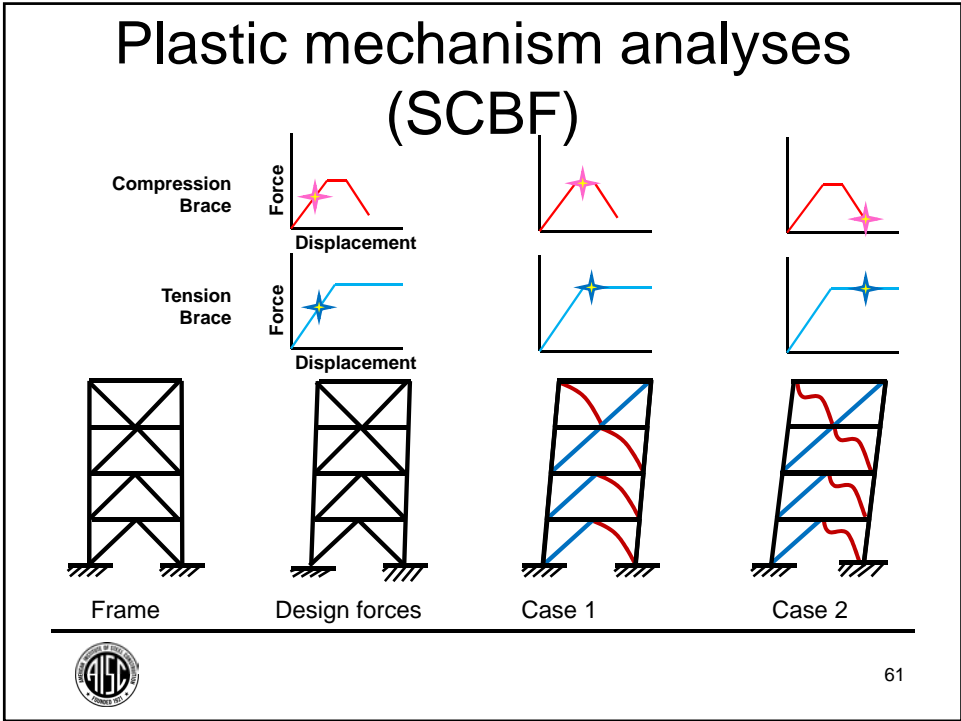


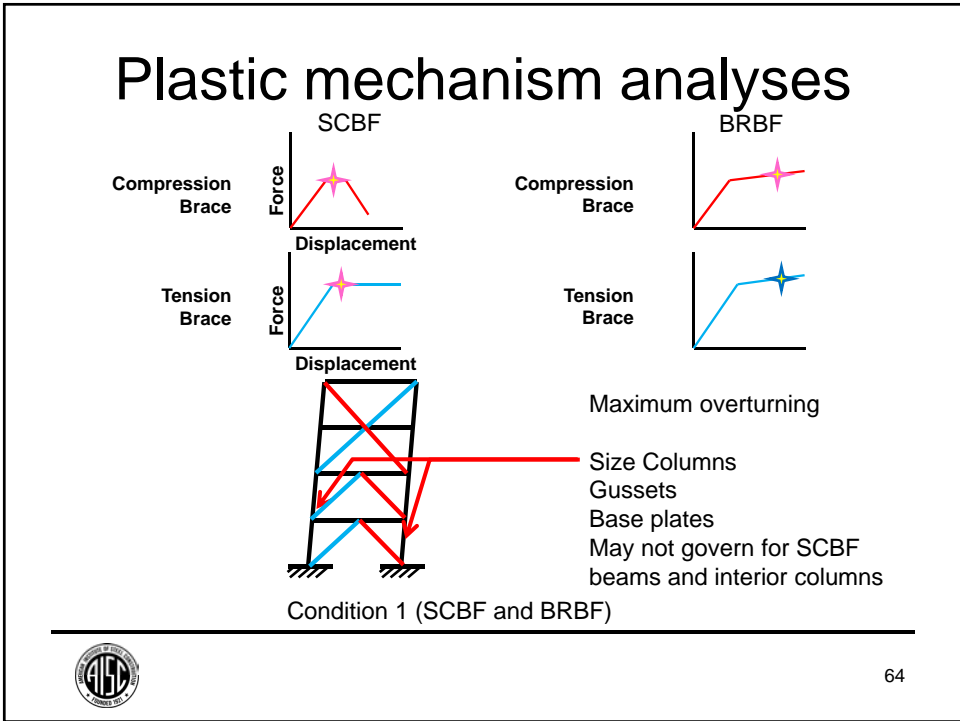
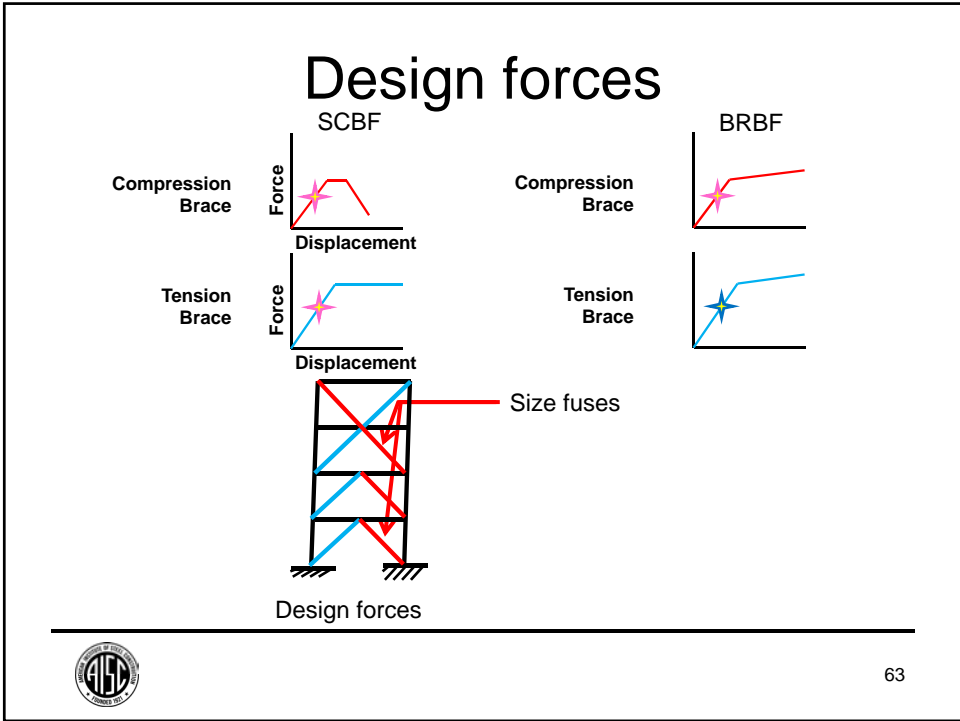
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## What elastic analysis misses

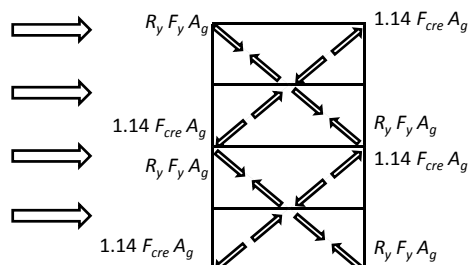


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## Plastic mechanism analyses



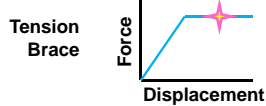
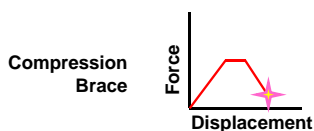
If  $1.14 F_{cre} A_g > R_y F_y A_g$   
 Use  $R_y F_y A_g$

Case 1

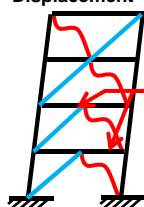


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## Plastic mechanism analyses



Force redistribution:  
 Compression braces  
 participate less  
 Force zig-zags



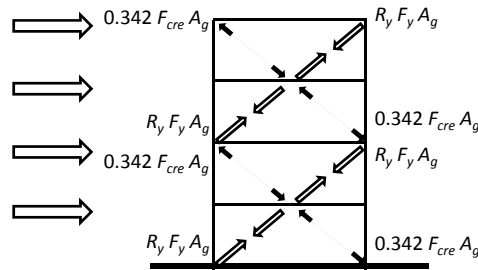
Size beams &  
 interior columns

Condition 2 (SCBF only)



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## Plastic mechanism analyses



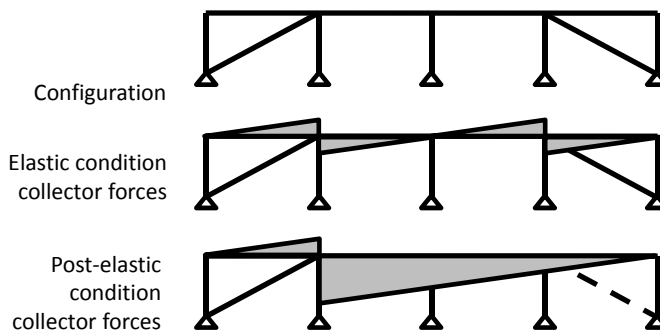
Case 2 (SCBF)



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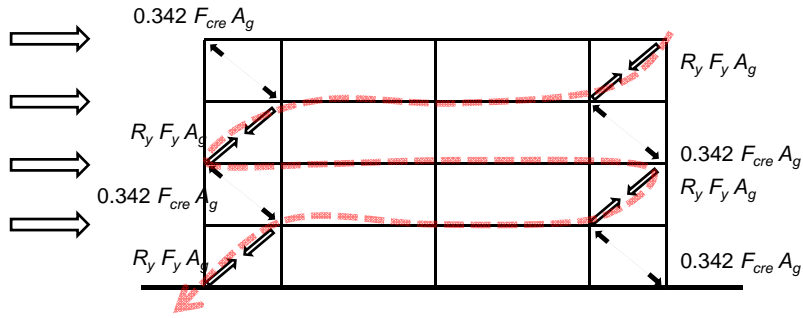
## Layout

- Post-elastic offsets



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## Plastic mechanism analyses



Case 2 Load Path



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## Temperature method of mechanism analysis

Equivalent to imposing strain

Redefine brace material properties

$$\alpha = 1 \text{ in./in.}/8F$$

$$E = 1 \text{ ksi}$$

Apply temperature to braces:

$$T = -\omega R_y F_y 8F/\text{ksi}$$

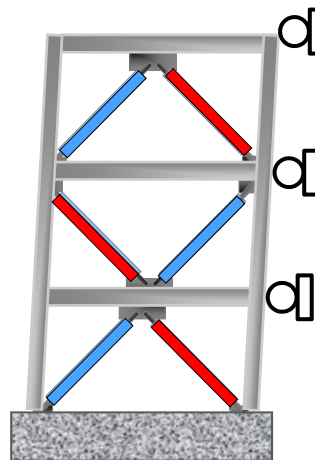
( $R_y F_y 8F/\text{ksi}$  [SCBF])

$$C = \omega \beta R_y F_y 8F/\text{ksi}$$

( $1.14 F_{cre} 8F/\text{ksi}$  [SCBF case 1])  
( $0.342 F_{cre} 8F/\text{ksi}$  [SCBF case 2])

Restrain lateral movement

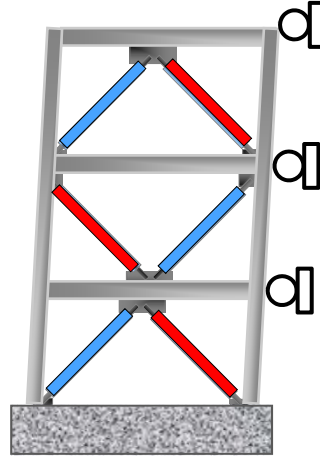
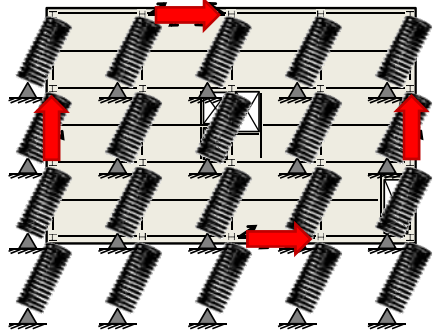
Analyze



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## Temperature method of mechanism analysis

Multiple springs may be used to represent distributed mass



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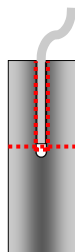
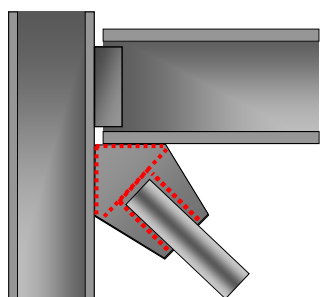
## Connections

There's always a solution in steel.



## Connection limit states

### Connections: Brace End



- Brace net section fracture
- Brace block shear fracture
- Brace-to-gusset weld fracture
- Gusset block shear fracture
- Gusset tension yield or fracture
- Gusset or weld failure at column
- Gusset or weld failure at beam
- Gusset buckling



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## Connection limit states

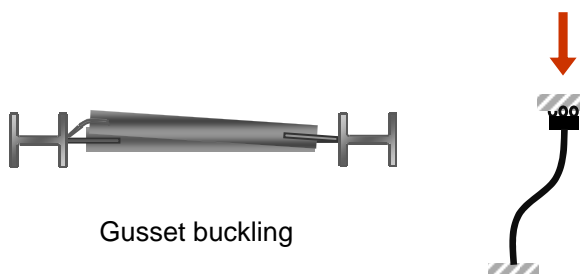
- Web proportioning
  - Where thick gussets are required thin webs may be inadequate
  - Research ongoing
  - Check web local yielding
  - Rule of thumb:
    - $t_w \geq \frac{3}{4} t_g$



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# Connection limit states

## Connections: Brace End



Gusset buckling



Refer to AISC Design Guide 29  
 gusset K factors

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# Gusset design

TECHNICAL NOTE  
**Effective Length Factors for Gusset Plates in Chevron  
 Braced Frames**  
 ENGINEERING JOURNAL / THIRD QUARTER / 2012

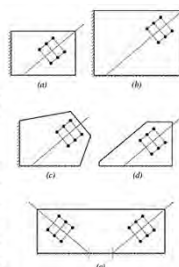


Table 3. Summary of Proposed Effective Length Factors<sup>a</sup>

Gusset Configuration	Effective Length Factor	Buckling Length
Compact corner	$\frac{b}{L}$	$\frac{b}{L}$
Noncompact corner	1.0	$l_{avg}$
Extended corner	0.6	$l_1$
Single brace	0.7	$l_1$
Chevron	0.65	$l_1$

<sup>a</sup> Table 7 from Dowswell (2006) with revisions.  
<sup>b</sup> Yielding is the applicable limit state for compact corner gusset plates; therefore, the effective length factor and the buckling length are not applicable.



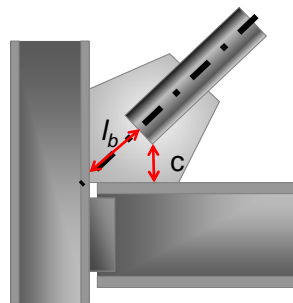
76

## Connection Instability



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## Connections: Compression

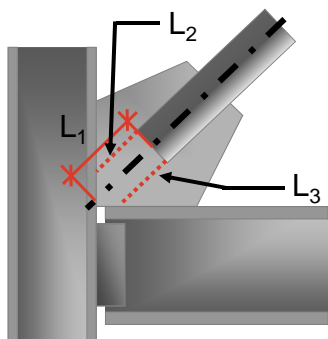


if  $t_\beta < t_g$ , the gusset will yield before it buckle (Dowswell, 2006)

$$t_\beta = 1.5 \sqrt{\frac{F_y c^2}{E l_b}}$$



## Connections: Compression



if  $t_\beta > t_g$ ,  $K = 0.6$  (Dowswell, 2006)  
 for conventional braces

Dowswell (2006)

3 Options (all reasonably reliable)

$L = \text{Ave } (L)?$

$L = \text{Max } (L)?$

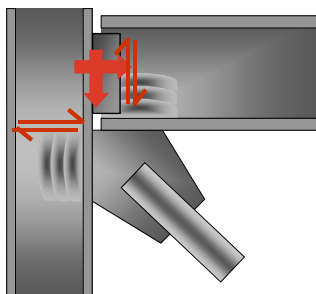
$L = \phi (L)?$



Effective length for BRB gussets is longer; consult with manufacturer

## Connection limit States

### Connections: Brace End



Column web yielding

Column web crippling

Column web shear

Beam web yielding,  
 crippling, shear

Beam-column connection, shear

Beam-column connection, axial



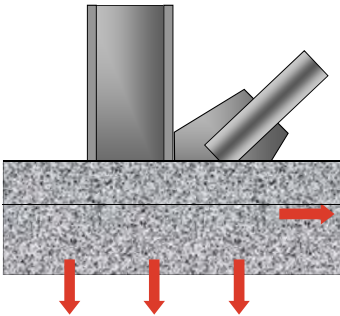
80

# Beam Instability



# Base-plates

## Connections: Base Plate



Shear

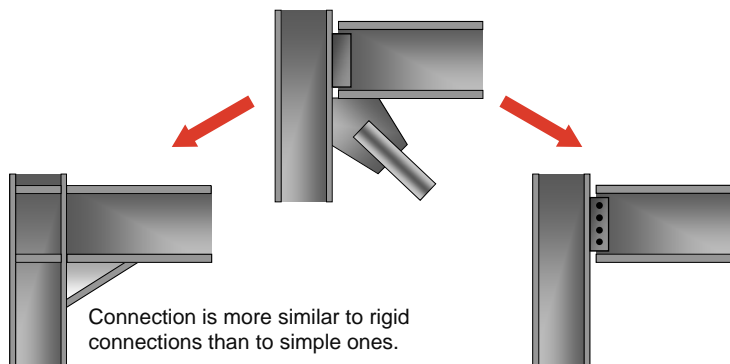
Tension

Resistance to horizontal and vertical force components must be provided. Different mechanisms (with different limit states) can be used.



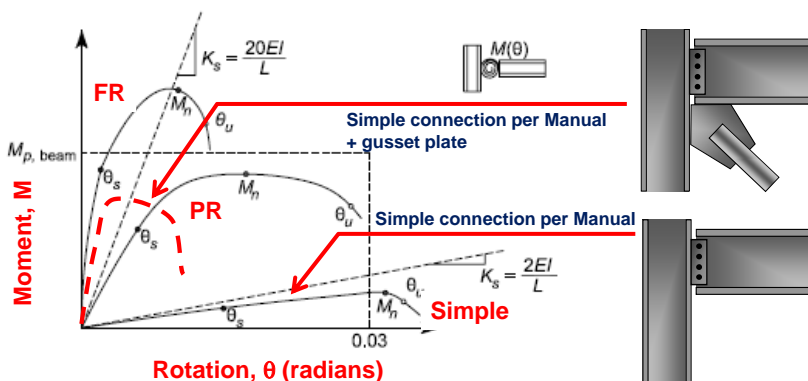
## Fixity of gusset connections

### Flexure: Connection Fixity



83

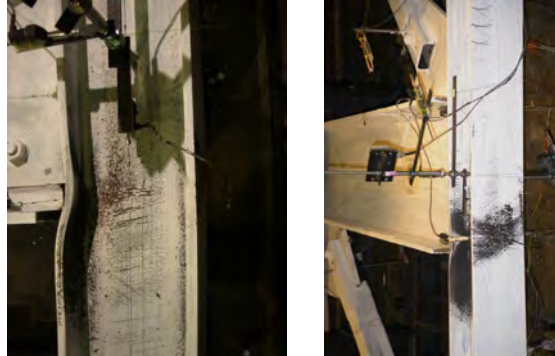
## Rotation in gusseted beam-column connections



84

## Rotation in gusseted beam-column connections

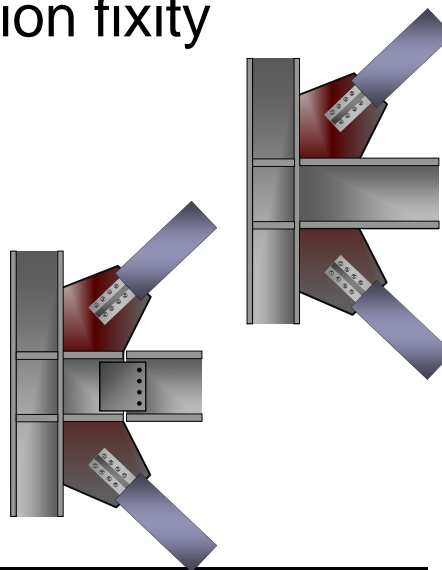
- UC Berkeley testing (and other testing) showed inability of simple+gusset connections to withstand large rotations



85

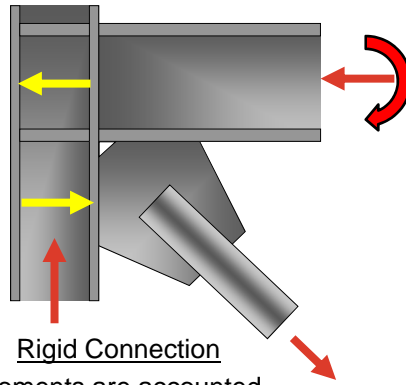
## Connection fixity

- Ductile moment frames provide extra resistance
  - Lateral strength and stiffness
  - Resistance to story mechanisms
- Ductile moment connections difficult to achieve



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## Method of accommodating frame rotations



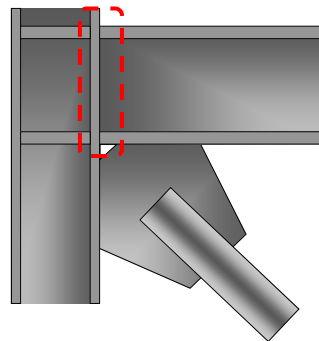
Connection strength exceeds beam strength

Rigid Connection  
Moments are accounted for in design



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## Method of accommodating frame rotations



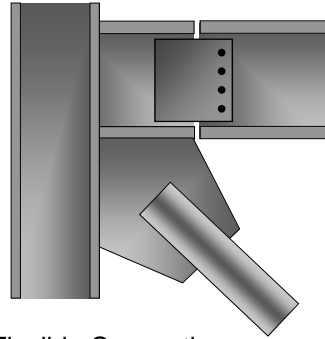
Connection consists of Ordinary Moment Frame (OMF) connection, plus gusset

Rigid Connection  
Moments are implicitly accounted for



88

## Method of accommodating frame rotations



Connection typically provides rotation by means similar to shear connections in AISC manual

2.5% rotation required

Flexible Connection  
Rotations are accommodated



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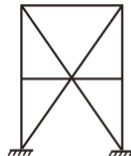
## Additional topics

There's always a solution in steel.

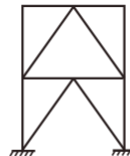


## Configuration

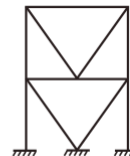
- Chevron
  - V or inverted-V
  - Formerly known as “K”
    - Until 1970s.
  - Two-story X
  - Post-elastic vertical forces on beams



Multistory X-bracing



Inverted V-bracing  
(Chevron)



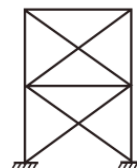
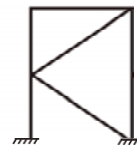
V-bracing



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## Configuration

- K
  - Post-elastic horizontal forces on columns
  - Prohibited
- Tension-only braces
  - Only allowed in OCBF



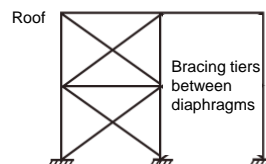
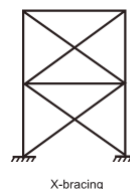
X-bracing



92

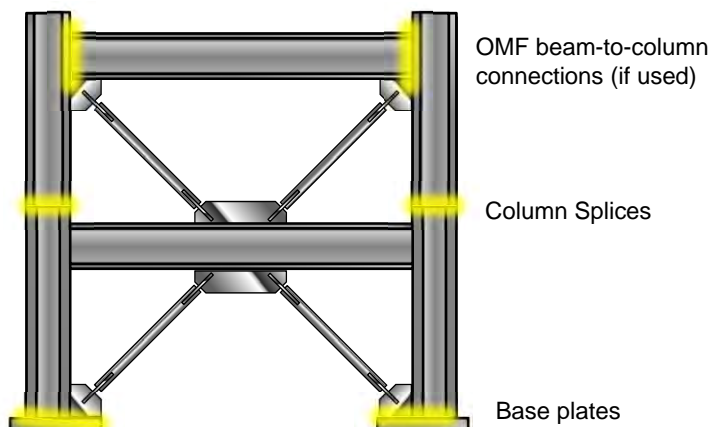
## Configuration

- Cross bracing
  - Tension-compression
  - Increased (concentrated) brace ductility demand
  - Half-length can be used
  - Not possible for BRBF
- Multi-tiered braced frames
  - AISC 341-16 has special provisions



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## Demand critical welds



94

## Detailing & Constructability

- Buckling deformation
- Interaction with architecture
- Protected zones
- Brace connection tolerances
- Direct-welded brace connections

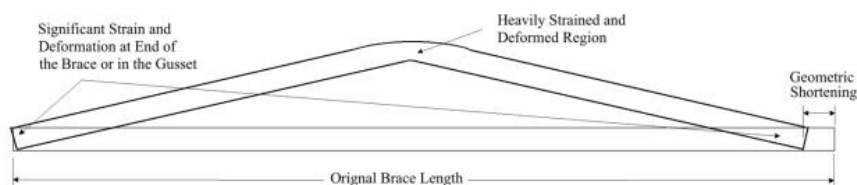


SCBF

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## Buckling deformation (SCBF)

- 10% of brace length should be considered
- Provide clear zone.



SCBF

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## Interaction with architecture (SCBF)

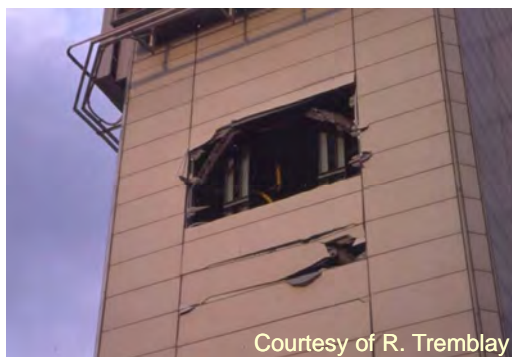
- Braces concealed in walls
  - Allow for brace buckling
    - Double walls for in-plane buckling
  - Allow gussets to flex or fold where required to accommodate brace buckling
    - Composite deck
    - Ground-floor slabs



SCBF

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## Brace Buckling: Effect on Other Elements

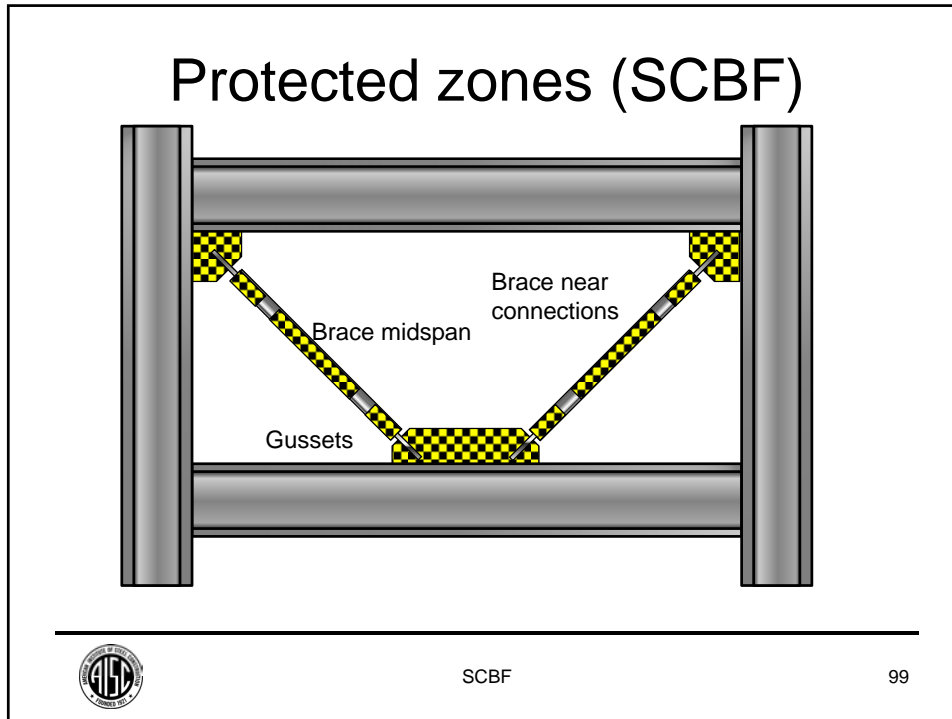


Courtesy of R. Tremblay



SCBF

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### Protected zones

- Areas of anticipated inelastic strain
- Attachments prohibited
  - Assumed to create fracture-initiation points
- Area of ongoing research

SCBF

100

## Brace connection tolerances

- Oversize holes
  - AISC requires design for overstrength factor  $\Omega_o$
- Slots
  - $\frac{1}{8}$ " wider than plate
  - 2" longer than final position
    - Assume erectors may position brace min. 1" off
      - Sufficient lap with gusset for weld, block shear
      - Sufficient reinforcement length in assumed final position



SCBF

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## HSS availability

- A500
  - Material is often dual certified
    - Grade B/Grade C
  - Grade C is preferred
  - Many round shapes published but only available in mill quantities
    - Check AISC website
    - Service centers
- New ASTM A1085
  - $R_y=1.25$



SCBF

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## Configuration

- Overturning

Braced-frame column

Drag forces (case 1 and case 2)

---

SCBF
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## SCBF Connections in the AISC Seismic Design Manual

- F2.6b: Provide a beam-to-column connection which is fixed or allowed to rotate
- F2.6c(3): Accommodate brace buckling

Example	Method of complying with AISC <i>Seismic Provisions</i> Section F2.6b	Method of complying with AISC <i>Seismic Provisions</i> Section F2.6c(3)
5.3.10	Detailed to provide rotation per Section F2.6b(a)	Linear hinge zone
5.3.11	Detailed as FR connection per Section F2.6b(b)(i)	Elliptical hinge zone
5.3.12	Designed to resist moments per Section F2.6b(b)	Hinge plate for in-plane brace buckling Fixed-end brace connection

---

SCBF
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## Direct-welded connections

- Provide full brace strength
- Provide fixity in both planes
  - Provide load path for brace-buckling fixed-end moments
- Investigate all geometrical conditions



SCBF

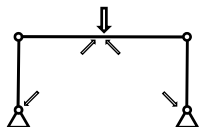
105

## Gravity forces in BRBs

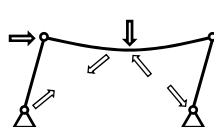
### Gravity Forces in Braces

Neglect

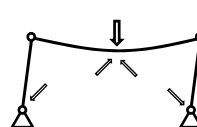
Effective tension and compression strength will be equal for subsequent cycles



Gravity load applied  
 Braces compress



Lateral load applied  
 Braces yield  
 Compression 1<sup>st</sup>?  
 Tension brace pulls down



Lateral load released  
 Beam pulls up and gravity load pushes down  
 Braces compressed  
 $\frac{1}{2} (\beta - 1) \omega R_y A_{sc} F_y$



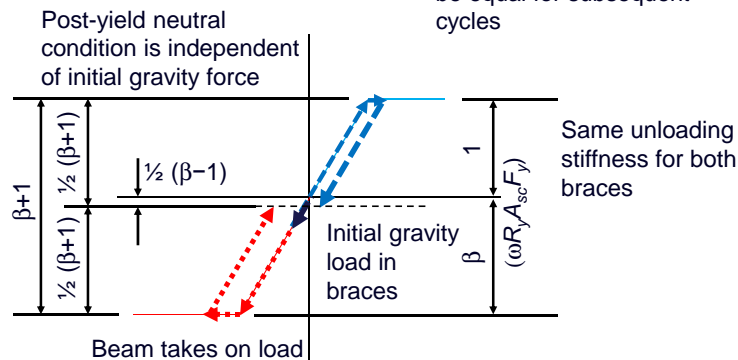
BRBF

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# Gravity forces in BRBs

Gravity Forces in Braces

**Neglect**



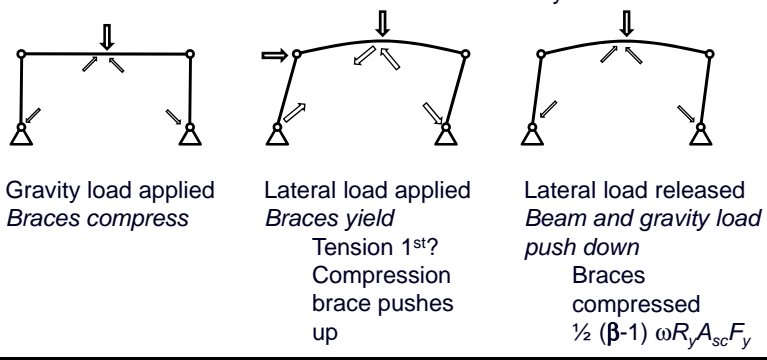
BRBF

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# Gravity forces in BRBs

Gravity Forces in Braces

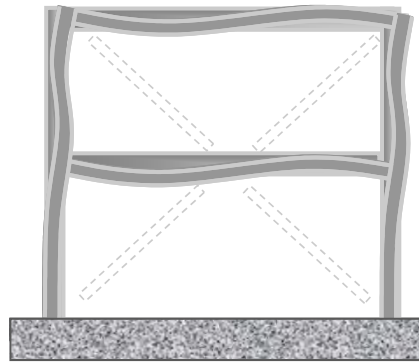
**Neglect**



BRBF

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## Frame Participation

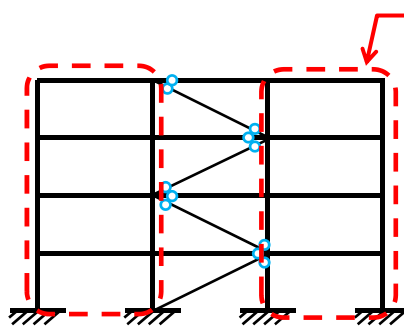


Flexural forces are induced in rigidly-connected columns and beams due to drift.



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## Connection fixity



If moment frames are needed, consider locating them in bays that are free of braces



110

There's always a solution in steel.

## Summary



## Summary

- Braces provide inelastic drift through brace axial ductility
- SCBF braces yield in tension and buckle in compression
- BRBF braces have a core that yields in tension and compression
- OCBF limit inelastic demand through higher strength
- Gusset-plate detailing and proportioning is necessary to ensure inelastic drift capacity



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There's always a solution in steel.

## End of session 2

Next:  
**Seismic design of buildings**



## Additional resources

<p>NIST GCR 13-317-24 NEHRP Seismic Design Technical Brief No. 8 <b>Seismic Design of Steel Special Concentrically Braced Frame Systems</b> A Guide for Practicing Engineers Robert Sabelli Charles W. Roeder James P. Heggie NIST National Institute of Standards and Technology</p>	<p>Steel Design Guide <b>29</b> <b>Vertical Bracing Connections— Analysis and Design</b></p>	<p>NIST GCR 13-317-24 NEHRP Seismic Design Technical Brief No. 11 <b>Seismic Design of Steel Buckling-Restrained Braced Frames</b> A Guide for Practicing Engineers Evan A. Hering Larry A. Eitzinger Marko A. Lapan NIST National Institute of Standards and Technology</p>
		

There's always a solution in steel.

## Question time



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- Password: Same as AISC website password.



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One certificate will be issued at the conclusion of  
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Access to the quiz: Information for accessing the quiz will be emailed to you by Wednesday. It will contain a link to access the quiz. EMAIL COMES FROM NIGHTSCHOOL@AISC.ORG

Quiz and Attendance records: Posted Tuesday mornings.  
[www.aisc.org/nightschool](http://www.aisc.org/nightschool) - click on Current Course Details.

Reasons for quiz:

- EEU – must take all quizzes and final to receive EEU
- CEUs/PDHS – If you watch a recorded session you must take quiz for CEUs/PDHS.
- REINFORCEMENT – Reinforce what you learned tonight. Get more out of the course.

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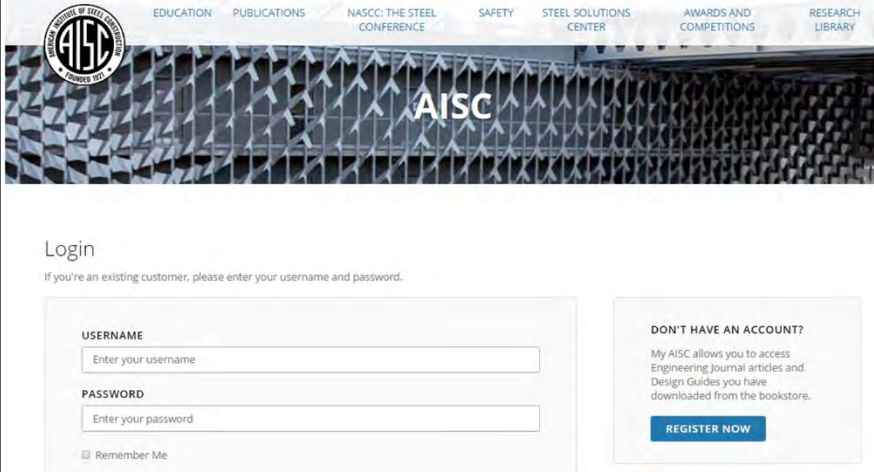
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recording access, and attendance information all in  
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**AISC**

AISC > MYAISC > COURSE RESOURCES

### Course Resources

Event	Start Date
NS 13 8-Session Package-Night School 13 - Design of Industrial Buildings	1/30/2017 7:00:00 PM
NS 14 8-Session Package-Night School 14 - Fundamentals of Stability	6/5/2017 7:00:00 PM

## Night School Resources for 8-session package Registrants



### Night School 13: Design of Industrial Buildings

#### 8-SESSION PACKAGE RESOURCES

Event	Date	Handouts	Video	Quiz	Attendance
NS13 - Design Criteria	1/30/2017 7:00:00 PM	<a href="#">Handouts</a>	<a href="#">View</a> Passcode: NS13DSN	Pass Score: 80	Pending
NS13 - Economic Considerations	2/6/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 02/06/2017 5pm EST	Available 02/06/2017 5pm EST	Pending
NS13 - Lateral Load Systems and Details	2/13/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 02/15/2017 5pm EST	Available 02/15/2017 5pm EST	Pending
NS13 - Preliminary Design Procedures	2/27/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 03/02/2017 5pm EST	Available 03/02/2017 5pm EST	Pending
NS13 - Crane Girder Design and Frame Analysis	3/6/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 03/08/2017 5pm EST	Available 03/08/2017 5pm EST	Pending
NS13 - Frame Member and Connection Design	3/13/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 03/15/2017 5pm EST	Available 03/15/2017 5pm EST	Pending
NS13 - Transfer Crane Girder & Longitudinal Rig Bracing Design	3/27/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 03/29/2017 5pm EST	Available 03/29/2017 5pm EST	Pending
NS13 - Building Envelope and Bracing Design	4/3/2017 7:00:00 PM	<a href="#">Handouts</a>	Available 04/05/2017 5pm EST	Available 04/05/2017 5pm EST	Pending
NS13 - Final Exam	4/10/2017 7:00:00 PM			Available 04/12/2017 5pm EST	

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  - Updated on Tuesday mornings.



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